



# *Evaluation of Effectiveness of Three Types of Highway Alignment Best Management Practices for Sediment and Nutrient Control*

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**Publication No. 41209**

Prepared by:

Nevada Department of Transportation and  
Division of Hydrologic Sciences, Desert Research Institute  
University and Community College System of Nevada

Prepared for:

U.S. Forest Service - Lake Tahoe Basin Management Unit,  
Nevada Division of State Lands, and the Nevada Department  
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## **ABSTRACT**

Lake Tahoe is renowned for its natural beauty. Regrettably, water clarity is declining at a rate of approximately 1 foot per year. This degradation has been attributed in part to nonpoint pollution sources including highway runoff. In response to regulatory requirements of the Tahoe Regional Planning Agency, the Nevada Department of Transportation (NDOT) developed the NDOT Lake Tahoe Master Plan for Erosion Control and Stormwater Management. Retrofitting of 39 miles of NDOT roadways with various types of best management practices is a major portion of \$100 million of improvements.

This research evaluates the efficiency of three types of highway alignment BMPs installed during the first phase of the NDOT Master Plan. A sediment trap, sediment basin and Stormceptor® were evaluated for nutrient and suspended sediment removal efficiency. Problems with flow sensors prevented efficiency calculations for the sediment basin. Concentration values did indicate some level of treatment however. The sediment trap removed 51 percent, 42 percent, and 32 percent of TSS, TP and TN respectively, although statistical analysis showed no difference between inflow and outflow. The Stormceptor® provided 31 percent, 25 percent, and 21 percent nutrient removal rates respectively for TSS, TP and TN with statistically significant differences between inflow and outflow.

## **ACKNOWLEDGEMENTS**

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## CHAPTER 1. INTRODUCTION

The beauty of Lake Tahoe, with its exceptional transparency and deep blue color, is widely acclaimed. In *Roughing It*, Mark Twain wrote, “So singularly clear was the water, that...even eighty feet deep...every pebble was distinct, every speckled trout, every hand’s-breadth of sand...The water was not merely transparent but dazzlingly, brilliantly so.”

Regrettably, the clarity of Lake Tahoe is declining at a rate of approximately 1 foot per year (Goldman 1988; Rueter and Miller, 2000). Many factors, identified in studies from 1962 to 1999, have contributed to eutrophication of Lake Tahoe including land disturbance, habitat destruction, soil erosion and air pollution (Rueter and Miller, 2000). Population growth, increased urbanization and roadways are believed to be the major factors contributing to increased sediment input to Tahoe basin streams and the lake (Rueter and Miller, 2000). Decreasing water clarity can be attributed to increases in primary productivity and suspended sediments (Jassaby *et al.*, 1999). Primary productivity has increased at a rate greater than 5 percent per year, closely tracking population growth within the Tahoe basin (Goldman, 1988). Increased nutrient loading has been identified as the cause of progressive eutrophication (Goldman, 1988). Most of the total nitrogen and dissolved inorganic nitrogen load to Lake Tahoe comes from atmospheric deposition (Jassaby *et al.*, 1994), while the majority of phosphorus comes from watershed contributions (Hatch *et al.*, 2001).

Prior to 1980, algal growth in Lake Tahoe was co-limited by nitrogen (N) and phosphorus (P) but began to shift to consistently P limitation around 1980, indicated by bioassay responses to P enrichment (Goldman *et al.*, 1993). This suggests algal growth is increasingly stimulated and limited by phosphorus. Early on, watershed management focused on exporting all sewage from the basin, restricting development, and controlling erosion. Although these measures were originally put into place for controlling nitrogen loading, they are now important controls for P contributions derived from the watershed (Jassaby *et al.*, 1994).

Over the decades, efforts for reducing nutrients and sediment loading to the lake have included acquisition of environmentally sensitive lands, treating surface runoff and implementing best management practices (BMPs) for controlling erosion. Two recent reports (Hydro Science, 2000; Murphy and Knopp, 2000) identified the lack of information pertaining to the effectiveness of various BMPs being constructed in the Tahoe basin and the need for research and monitoring to assess the efficacy of the various treatments and their potential for reducing nutrient and sediment loading to Lake Tahoe.

The Nevada Department of Transportation (NDOT) is responsible for 39 miles of roadway within the Tahoe basin. This includes 14 miles of State Route 28 (SR 28) and 12 miles of U.S. Highway 50 (US 50); both run adjacent to Lake Tahoe’s east shore for much of its length. Typically, roadway runoff from stormwater and snowmelt is channelized in roadside ditches or curb and gutter, ultimately discharged through culvert crossings. In many instances, these culverts discharge at locations within close proximity to Lake Tahoe, e.g., in some cases with direct hydrologic connection to the lake. Effectively treating stormwater runoff prior to discharge to the lake is a difficult challenge. Limited right-of-way, steep topography, highly erosive soils, large rock outcrops, shallow bedrock and lack of precipitation during spring and summer growing seasons are among the challenges that limit the types of BMPs available for use by NDOT.

In March 1997, NDOT implemented the first phase of the NDOT Lake Tahoe Master Plan for Erosion Control and Stormwater Management (MPECSWM) along 5.5 miles of SR 28 and 2 miles of US 50 from Spooner Summit to Glenbrook. This master plan identified needed improvements to meet the Tahoe Regional Planning Agency's (TRPA) 208 Water Quality Plan thresholds (Harding Lawson Associates, 1998). Collaborators, in implementing the MPECSWM, included over 15 different agencies including TRPA, Nevada State Lands, Nevada State Parks, Nevada Division of Environmental Protection, Federal Highway Administration (FHWA), U.S. Fish and Wildlife Service, Washoe County and Carson City. This effort would evolve into NDOT's Environmental Improvement Program (EIP), a component of the TRPA Environmental Improvement Program.

TRPA's EIP is a strategy for restoring, maintaining and/or attaining the nine environmental thresholds (including water quality) developed by TRPA for the Tahoe basin (TRPA, 2001). This is accomplished through the partnership of local, state and government agencies as well as private interests. The EIP serves as the framework for implementing regional projects and programs.

Since Lake Tahoe has become phosphorus limited, with the major sources of P coming from within the watershed, erosion control strategies for sediment reduction are considered appropriate courses of action (Goldman *et al.*, 1993). The Nevada Department of Transportation uses both source and treatment control strategies for sediment control and reduction. Primary source control strategies include roadside shoulder paving, riprap placement and revegetation of cut and fill slopes. Treatment controls include sediment/infiltration basins, sediment traps and ultra-urban BMPs such as sand/oil separators for treatment of roadway runoff. The Nevada Department of Transportation will spend over \$100 million by 2010 on erosion control and water quality improvements within the basin.

To date, 11 miles of NDOT roadways have been retrofitted with typical highway or ultra-urban BMPs. These include sediment traps, sand/oil separators, drop inlets modified to allow infiltration and sediment storage, infiltration basins and sediment basins. Although numerous studies have evaluated the effectiveness of various types of urban BMPs, appropriate mitigation measures for treating urban runoff within the Tahoe basin are unknown. Additionally, the effectiveness of various ultra-urban BMPs, now on the market, in reducing fine-grained sediment is debatable.

Responding to research needs, NDOT along with the Desert Research Institute (DRI), sought funding for monitoring typical treatment control structures installed along NDOT's roadways. This project is specific to three types of BMPs used in highway applications for the reduction of sediment and nutrients contained in highway stormwater runoff. The primary objective of this study is to determine the effectiveness of sediment traps, sediment basins and Stormceptor® units in removing nutrients and suspended sediments from stormwater runoff along NDOT roadways within the Tahoe basin. A second objective is to evaluate the cost benefit of these three types of structures.

Data and information gathered in this study will assist NDOT in adapting erosion control and water quality treatment strategies for future projects. Additionally, these data will be added to the Tahoe Interagency Information Management System (TIIMS) providing scientists, managers, implementers and others with data and information to assist in decision making.

The three BMP study sites are in rural settings surrounded by U.S. Forest Service property. However, although the majority of NDOT's roadways in the Tahoe basin are essentially rural settings, the terrain, exorbitant private property values, limited right-of-way, numerous underground utilities and the unique environment of the Tahoe basin dictate that ultra-urban BMPs be used.

The FHWA defines ultra-urban settings using the following factors to distinguish between studies addressing ultra-urban BMPs (USDA, 2000):

- Limited space available for BMP implementation (less than 1 acre).
- Drainage area imperviousness greater than 50 percent.
- Property value of land over \$30 per square foot.
- Location of BMP in right-of-way (only available space).
- Existence of build-out conditions at the site (lot-line to lot-line development).

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## CHAPTER 2. LITERATURE REVIEW

### Highway Water Quality Control

The Clean Water Act (PL 95-217) requires cooperation between federal, state and local agencies for the development of comprehensive solutions to prevent, reduce and eliminate pollution of U.S. waters. The FHWA is responsible for protecting the environment from highway source pollution under the Clean Water Act and other federal laws. A comprehensive program to identify and quantify the effects of highway runoff and develop management practices for the protection of water resources was initiated by the FHWA and summarized in a series of reports from 1981 through 1986 (Dorman *et al.*, 1996). This four-phase research program included the identification and quantification of highway runoff constituents, identification of pollutant sources, the effects to receiving waters, and the development of tools to minimize the effects of highway runoff pollutants. Research began with a comprehensive, systematic literature search to collect information on mitigation practices in treating highway runoff. Practices include vegetation controls, wet detention basins, dry extended detention basins, infiltration systems and wetlands and are considered the state-of-the art in pollutant removal from highway runoff.

Smith and Lord (1990) summarized the first three phases, over 15 years of FHWA sponsored research, which identified and quantified effects from highway runoff, and developed measures for protecting the environment from potential adverse effects. Five management measures were found to be cost effective for pollutant removal from highway runoff. These are vegetation controls, wet detention basins, dry extended detention basins, infiltration systems and wetlands. Effective nonstructural measures include elimination of curbs, reduction in direct discharge and runoff velocities, management of deicing chemicals, and establishment and maintenance of vegetation (Smith and Lord, 1990). Common practices such as street cleaning, installation of catch basins, porous pavements and filtration devices for sediment control and pollutant load reduction were found to be ineffective.

Phase 1 of the program identified and quantified highway runoff constituents. Table 2.1, adapted from USDA (2000), summarizes average concentration values reported in the literature from several studies, in locations throughout the United States, of various constituents of highway stormwater runoff. Data gathered from this NDOT/DRI investigation found results above the ranges listed here for TSS and TP.

Identification of the primary sources of highway pollutants was the program objective of Phase 2. Particulate sources were primarily from pavement wear, vehicles, atmospheric deposition, and maintenance activities. Major nitrogen and phosphorus sources were identified as the atmosphere and application of roadside fertilizer. Wu *et al.* (1998) found that 20 percent of TSS loadings and 70 to 90 percent of nitrogen loadings from stormwater runoff of highways possibly originated from atmospheric deposition.

Table 2.1. Constituents of highway runoff.

Parameter	National Concentration (mg/L)	NDOT <sup>1</sup> Concentration (mg/L)
Total Suspended Solids (TSS)	45 to 798	74 to 2,799 (827)
Volatile Suspended Solids (VSS)	4.3 to 79	Not Sampled
Total Organic Carbon (TOC)	24 to 77	Not Sampled
Chemical Oxygen Demand (COD)	14.7 to 272	Not Sampled
Biochemical Oxygen Demand (BOD)	12.7 to 37	Not Sampled
Nitrate + Nitrite (NO <sub>3</sub> +NO <sub>2</sub> )	0.15 to 1.636	0.016 to 0.980 (0.15)
Total Kjeldahl Nitrogen (TKN)	0.335 to 55.0	0.52 to 13.45 (3.69)
Total Phosphorus as P	0.113 to 0.998	0.210 to 4.297 (1.15)
Copper (Cu)	0.022 to 7.033	Not Sampled
Lead (Pb)	0.073 to 1.78	Not Sampled
Zinc (Zn)	0.056 to 0.929	Not Sampled

<sup>1</sup>NDOT concentrations are maximum and minimum values. Values in parentheses are the average concentrations for the study period.

Phase 3 program objectives were to determine the magnitude and extent of highway stormwater runoff impacts. Results indicated minimal impacts to receiving waters for highways with less than 30,000 vehicles per day or ADT (Average Daily Traffic). It should be noted that in the Tahoe basin, traffic volume is not the main source for nutrients and suspended sediments, but rather nitrogen comes from atmospheric sources and phosphorus from roadway cut slopes. Evaluation of the use of retention, detention, and overland flow systems as potential highway runoff mitigation measures was the final study in Phase 4. The resulting FHWA report (Dorman *et al.*, 1996) developed and updated design guidelines for these state-of-the-art practices representing the best available technology for removal of pollutants from highway runoff. From the five management measures identified as cost effective, vegetative controls were considered the primary pollution management measure for highway stormwater runoff. Vegetative controls including vegetated swales and filter strips are effective, relatively low in cost and have widespread applicability.

### Vegetative Swales

Grass-lined channels and overland flow areas are the most common mitigation measures used for pollutant removal of highway runoff (Dorman *et al.*, 1996). Design flexibility, site adaptability and relatively low costs in comparison to other mitigation measures are key reasons for their widespread use. When properly designed, vegetative measures can be extremely effective in reducing runoff pollution. Flow depth and detention time are key design elements for the effectiveness of vegetative swales. Increasing flow width and flow length and decreasing slope will extend detention times and increase pollutant removal efficiencies. Successful design of swales should include mild slopes, dense vegetation, low flows, low velocities, maximized surface area and check dams to create ponding areas.

The primary function of vegetative channels and flow areas is the removal of pollutants through sedimentation. Effectiveness is dependent on flow depth and detention time. Stability is the overriding design factor with stability of vegetative control systems



dependent on the erodibility of the underlying soils and the maximum shear stress of the soil. Mitigation is achieved by using grass, riprap, etc., but only grass lining provides effective pollutant removal. Grass is the most common vegetation used and nutrients are more effectively removed by grass than by shrubs, trees, or other vegetation.

Vegetative swales have been shown to reduce 23 percent to 80 percent of TSS loadings from roadway runoff (Kaighn and Yu, 1996; Wu *et al.*, 1998). Kaighn and Yu (1996) reported that one study comparing pollutant concentrations in grass lined and paved channels found water quality parameters were 63 percent lower in grass-lined channels than the paved channels. However, Kaighn and Yu (1996) reported that another study found swales were actual sources of pollution.

Yousef *et al.* (1985) found mass removal of heavy metals, nitrogen, and phosphorus was directly related to infiltration losses and on-site storage. Removal efficiencies were dependent upon contact time and infiltration rates. Losses of nitrogen and phosphorus were found to be lower than those for dissolved heavy metals. Retention of pollutants in swale areas is most likely through chemical mechanisms such as sorption, precipitation, co-precipitation and biological uptake processes.

Dorman *et al.* (1996) state minimum design criteria of vegetative controls are as follows:

- Non-erosive slopes, generally less than 8 percent
- Channel lengths of at least 200 feet in length
- Overland minimum length of 40 feet the direction of flow with minimum width of 40 feet

Vegetative controls are not well suited for environmental conditions within the Tahoe basin due to the lack of moisture within the growing season. Precipitation occurs mainly in the winter months in the form of snow when plants are typically dormant.

### **Wet Detention Basins**

Where vegetative control systems are not feasible, wet detention basins can be an acceptable and effective alternative when properly designed (Dorman *et al.*, 1996). Wet detention ponds are designed to have a permanent pool of water. This permanent pool enhances particulate settling by increasing water residence time and also provides conditions for growth of aquatic vegetation, allowing enhanced filtration, and metals and nutrient uptake (USDA, 2000). Basin depth, the ratio of basin storage volume to watershed area, and routine maintenance are important features for ensuring pollutant removal effectiveness.

Highway pollutants (suspended sediments and trace metals) are removed primarily through sedimentation. Ortho-phosphorus, nitrate and nitrite can be effectively removed through plant and algal uptake and denitrification. A number of studies have shown that wet detention basins are moderately to highly effective in reducing suspended solids, nitrogen and phosphorus (e.g., Ferrara and Witkowski; 1983 and Martin, 1988). However, detention basins can be sources of nutrients (Ferrara and Witkowski, 1983).

Detention facilities are commonly used for peak flow reduction of a design storm. Water quality benefits have been claimed for these structures although such basins are not specifically designed for water quality improvements. Ferrara and Witkowski (1983) cite two

studies that demonstrated detention basin design should be different for flood control and pollution control. Considerations for water quality treatment of solids require characterization of solid gradation, mass loading, surface area and specific gravity (Sansalone *et al.*, 1998). Characteristics of rainfall, runoff, settling velocities for suspended solids and particulate and pollutant distributions in each size fraction are needed to design wet detention basins to achieve pollutant removal objectives (Dorman *et al.*, 1996). Wet detention basins can be highly effective provided the systems are properly designed to settle out suspended solids.

### Dry Detention Basins

Dorman *et al.* (1996) recommends the use of dry detention basins in place of wet detention basins where removal of sediments, rather than nutrients, is the major emphasis. The advantage of a dry detention basin is the reduced volume of storage required when compared to a wet detention basin. Pollutant reduction is dependent on the removal of suspended sediments. Typically, it is assumed that infiltration through the underlying soils will remove soluble nutrients from surface runoff. Infiltration rates and depth to groundwater should be considered when opting for retention of stormwater runoff. Stanley (1996) found that in dry detention basins, TSS removal ranged from 3 percent and 87 percent, TP and TN removals from 13 to 40 percent and 10 to 35 percent, respectively. Table 2.2 shows the removal efficiencies of TSS, TP, TKN and NO<sub>3</sub> from a number of studies. This table indicates greater success in removal of pollutant loading from stormwater runoff than Stanley (1996).

Table 2.2 Pollutant removal effectiveness of detention ponds (%), modified from USDA (2000).

Type	TSS	TP	TKN	NO <sub>3</sub>
On-line wet pond <sup>1</sup>	46	37	14	36
Wet retention pond <sup>1</sup>	94	81	44	64
Extended detention wet pond <sup>2</sup>	76	70	65	75
In-line wet detention pond as pretreatment to wetland system. Efficiencies are for pond only <sup>2</sup>	78	20	-	-
Based on water column sampling from various sites in wet detention pond <sup>1</sup>	85	54	26	92
Dry detention pond <sup>2</sup>	67 to 93	75 to 94	-	-
Dry detention pond, study evaluated modifications to outlet <sup>2</sup>	96	81	44	64

<sup>1</sup> Removal efficiencies based on concentration.

<sup>2</sup> Removal efficiencies based on mass loading.

In general, detention basins should detain runoff for a minimum of 6 hours and have one inlet and outlet to facilitate monitoring. If a permanent pool is present, it should be between 2 and 10 feet in depth. Basin configurations should not allow short-circuiting of storm flows through the basin (Dorman *et al.*, 1996). Detention basin use in the Tahoe basin is limited due to the steep and rugged terrain and the lack of suitable right-of-way.

## **Infiltration Systems**

Suitable infiltration facilities for highway runoff treatment applications include infiltration/retention basins, infiltration/retention trenches, and infiltration/retention wells (Dorman *et al.*, 1996). Susceptibility to clogging and the resulting additional maintenance requirements make infiltration trenches and wells impractical for use at some highway sites. Infiltration basin locations are dependent upon site conditions. Adequate infiltration rates are required with a minimum infiltration rate of 0.3 in/hr, recommended by Dorman *et al.* (1996), needed to allow for available storage for subsequent runoff events. Depth to the seasonal high groundwater table, beneath a basin, should be a minimum of 2 to 4 feet. Urbonas and Stahre (1993) recommend more stringent guidelines including minimum depth to groundwater, depth to bedrock, specific surface and underlying soil types, and a minimum infiltration rate of 0.3 in/hr as reported by SCS soil surveys.

Infiltration basins are typically designed to capture flow from first flush stormwater runoff. The Nevada Department of Transportation, where possible, sizes sediment/infiltration basins to retain the 20-year, 1-hour storm, the storm locally defined as one inch of rainfall. This storm is considered to be the first flush storm. Due to local topography and terrain constraints, detention basins constructed to treat runoff from NDOT roadways are frequently undersized. Large runoff events are not contained within these basins and pass on through; only small runoff events are infiltrated. However, the prevailing thought is that infiltration is the preferable stormwater runoff treatment and should be implemented where possible. Discussions regarding first flush issues are provided in a later section.

## **Wetlands**

Wetlands have been identified as a potentially significant treatment for stormwater runoff (Reuter *et al.*, 1992; Mitsch, 1993; Dorman *et al.*, 1996). Nutrient and pollutant removal in wetlands is effected by a complex, interrelated combination of physical, chemical and biological mechanisms (Reuter *et al.*, 1992; Dorman *et al.*, 1996). Figures 2.1 and 2.2 show nitrogen and phosphorus transformations within a wetland system.

Subsurface soils and vegetation stands provide a large surface area, allowing for high levels of physical, chemical and biological removal of the various forms of nitrogen and phosphorus. Physical processes include entrapment, sedimentation, adsorption and filtration. Chemical processes include volatilization, precipitation, and decomposition. Vegetation and algal uptake and bacterial denitrification are the primary biological removal mechanisms of nitrogen and phosphorus. As with other reported BMPs, flow regime, detention time and ratio of surface area to volume treated are important parameters for treatment effectiveness. Despite reported effectiveness, wetlands do export nutrients at various times. Table 2.3 provides examples of nutrient export.

The Nevada Department of Transportation treats roadway runoff at a few locations using wetlands (none within the Tahoe basin). However these opportunities are rare. In most instances, wetlands are not a feasible option for treating NDOT's stormwater runoff. Highway runoff is intermittent, random, and varies with rainfall intensity. Excessive rainfall could cause erosion. Vegetation would not survive too little rainfall, a common occurrence in Nevada.

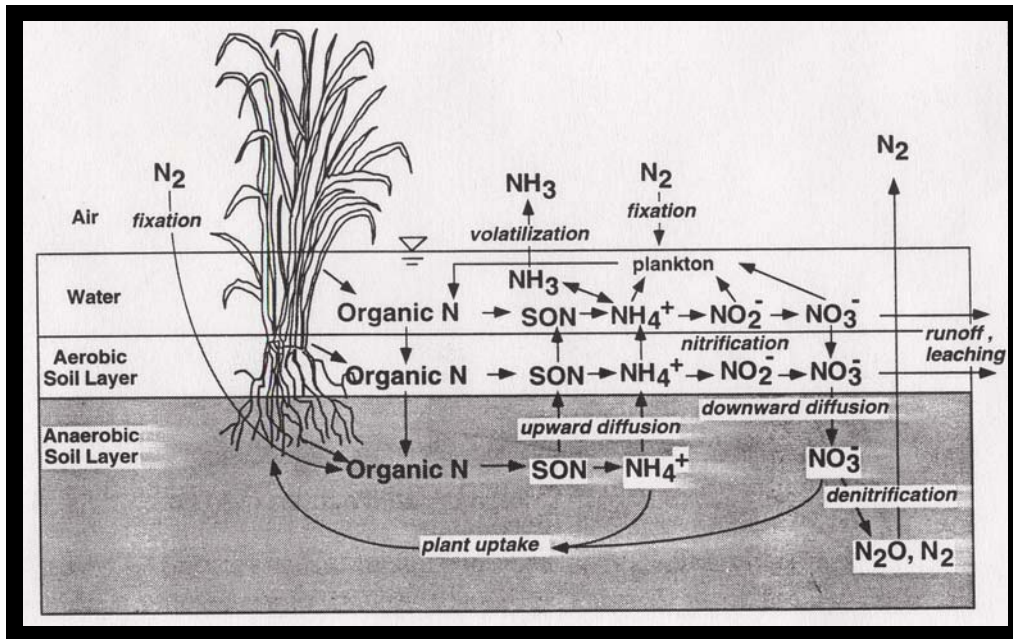


Figure 2.1. Nitrogen transformations (Mitsch, 1993).

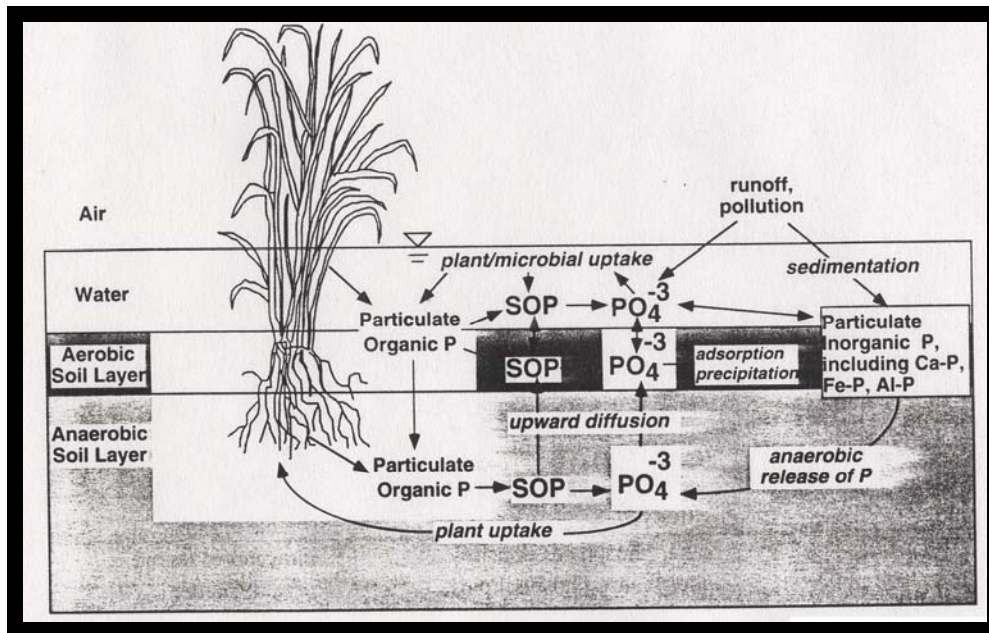


Figure 2.2. Phosphorus transformations (Mitsch, 1993).

Table 2.3. Nutrient and sediment removal comparison for treatment of wastewater and urban runoff expressed as mean annual percent removal. Adapted from Rueter *et al.* (1992).

Wet Land System	TKN	NH <sub>4</sub>	NO <sub>3</sub>	TP	SRP	SS
Wastewater Range	12 to 81	24 to 96	20 to 99	13 to 99	6 to 98	29 to 92
Urban Runoff Minnesota	31	-	97	61	62	80
Urban Runoff Florida	16 to 25	(-73) to (-19)	-	9 to 19	(-18) to 1	44 to 54
Newly Constructed Tahoe Wetland	(-3) to (-14)	(-58) to (-53)	85 to 87	44 to 47	(-28) to (-41)	80 to 88

### First Flush

The first flush is a term commonly used throughout the literature and used as a minimum design parameter for the goal of treating urban runoff. A first flush phenomenon has been defined as the initial period of stormwater runoff where pollutant concentrations are substantially higher than concentrations in the later stages of storm runoff (Lee *et al.*, 2002). First flush runoff in the Tahoe basin is commonly referred as the 20-year, 1-hour storm, approximately equivalent to 1 inch of rainfall over a typical watershed for the Tahoe basin.

Higher nutrient and suspended sediment concentrations of a first flush are assumed to result from the accumulation of pollutants deposited on paved and unpaved surfaces (from various sources such as atmospheric deposition) that will wash off upon the arrival of new storms. The length of time between storms likely increases the amount of loading to receiving waters from stormwater runoff. If the first flush phenomenon is valid for highway runoff in the Lake Tahoe basin, then stormwater treatment systems could be designed to treat only a portion of the storm and not the storm in its entirety. Various studies have reported conflicting results on whether or not a first flush exists and what its characteristics are (Urbonas and Stahre, 1993; Barrett *et al.*, 1998; Deletic, 1998; Lee *et al.*, 2002).

Deletic (1998) provides a number of definitions for first flush calculations reported in the literature. Typically, a comparison is made between the cumulative total pollutant mass versus the total cumulative volume of runoff. Resulting curves with slopes greater than 45 percent are identified as storm runoff affected by a first flush load. A stringent first flush definition is provided, occurring when at least 80 percent of the pollutant load has been conveyed during the first 30 percent of runoff volume. Other common definitions use an approach where a fraction of the total pollutant load is compared with a fraction of the runoff load, typically at the 25 percent to 30 percent storm runoff point (Deletic, 1998). These various definitions contribute to the difficulty and variability in assessing first flush phenomena.

The first flush appears to be highly variable and complex. Lee *et al.* (2002) reported that concentration peaks may vary for different pollutants during the same storm event or for the same watershed during different storm events. Additionally, they found that when analyzing the same storm data using three different first flush analysis methods, the strength of the first flush varied with each calculation method. Deletic (1998) suggests that a first flush effect at the end of a drainage system may be caused by pollutant transformations and transport processes rather than direct pollution input into the drainage system.

The magnitude of the first flush observed in a number of studies varied between types of pollutants, types and sizes of watersheds, percentage of impervious surface, method of first flush calculation and volume of runoff (Cristina and Sansalone, 2003; Deletic, 1998; Lee and Bang, 2000; Lee *et al.*, 2002). Lee and Woong (2000) found that peak pollutant concentration preceded that of the peak flow rate in an area smaller than 100 ha (247 acres) in which impervious area encompassed more than 80 percent of the watershed. Their study found stronger evidence of the first flush for both particulate and dissolved pollutants as the watershed area decreases and the rainfall intensity (*r*) increases (Figure 2.3). Values located above the 45 percent line are indicative of the first flush.

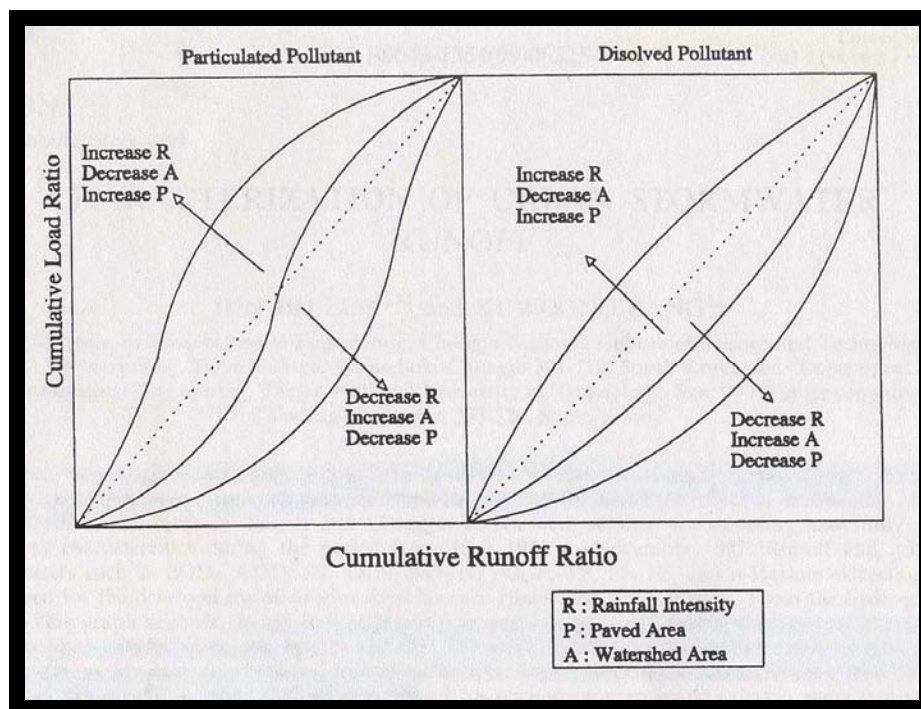


Figure 2.3. Apparent affects of rainfall intensity, paved area, and watershed area on first flush phenomena (Lee and Woong, 2000).

Studies have been contradictory in regard to pollutant build-up between storms. Some research has found no correlation between the first flush phenomenon and the length of antecedent dry weather period (Whipple *et al.*, 1977; Stanley, 1996; Lee *et al.*, 2002), but Brezonik and Stadelmann (2002) found that length of time between storms increased pollutant concentrations in stormwater runoff.

First flush analysis could not be performed for the NDOT sites, as the study was not designed to examine this phenomenon. Detailed analysis is required to determine whether the study areas exhibit first flush characteristics. Data collection must be frequent enough, especially in the first hour of each runoff event, to correctly study the first flush and to capture the short, high-intensity thunderstorms (Delectic, 1998). Analysis of data collected during this study showed little evidence that a first flush existed. Concentrations and loading

values showed no pattern of progressive decreases as storm flows progressed. It is equally important to obtain numerous samples throughout the duration of the event. However, NDOT sites could express first flush phenomena, as these are typically small in size (1 to 2 acres), with impervious surface areas greater than 80 percent.

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## CHAPTER 3. STUDY SITE

### Environmental Setting

Lake Tahoe is an ultra-oligotrophic lake noted for its unusual clarity (Jassaby et al., 1994, 1999). Characteristics causing this high transparency include the small watershed area (314 mi<sup>2</sup>) relative to the lake's size (192 mi<sup>2</sup>), a watershed to lake ratio of only 1.6 (Jassaby *et al.*, 1999) Forty percent of the precipitation in the Tahoe basin falls directly on the lake. The dominant basin soils are relatively sterile decomposed granite soils that allow water to filter through relatively free of nutrients and sediment.

Due to the high altitudes of the surrounding mountain ranges and the prevailing storm systems, precipitation is unevenly distributed throughout the basin. The western side of the Tahoe basin receives more than 80 inches of precipitation per year, on average, compared to the 30 inches per year received on the eastern side (USGS, 1997). Much of the precipitation in the basin falls in January through March in the form of snow. Low annual precipitation, falling mainly in the winter months in the form of snow, along with erosive granite soils pose difficult challenges for implementation of erosion control solutions along Tahoe's east shore. Cagwin-Rock outcrop complex (CaF) is the soil type in the study area on SR 28. The U.S. Highway 50 site contains Umpa (UmE) soils. These soil types have high and moderate erosion hazards, respectively (USDA, 1974).

### Study Sites

Locations of the three monitoring sites are along Tahoe's east shore (Figure 3.1). Two sites, NDOT 2 and NDOT 4, are located on SR 28 in the Secret Harbor Creek watershed. The third site, NDOT 3, is located along US 50 in the Glenbrook Creek watershed. Table 3.1 summarizes site conditions.

A stipulation of one funding source required BMP monitoring take place along SR 28 within Carson City limits. Locations were chosen based on similar contributing areas and on type of runoff each BMP would collect. Each BMP site receives mostly roadway runoff with minimal stormwater runoff contribution from offsite (nonhighway runoff) flows. Sediment contributions to NDOT 2 are a combination of both onsite from road sand applications and offsite contributions from the adjacent 14,585 square foot cut slope. NDOT 3 and NDOT 4 receive sediment mostly from winter sanding operations.

The terrain along much of the 26-mile stretch along SR 28 and US 50 is steep with many of the roadway cut and fill slopes at 1:2 or steeper. Roadway cut slopes generally range from 5 to 100 feet in height. Fill slopes range from 5 to 50 feet in height. Dominant vegetative cover is primarily Jeffery Pine (*Pinus jefferyi*) forest with an understory consisting of shrubs such as manzanita (*Arctostaphylos* spp.), bitterbrush (*Purshia tridentata*) and sagebrush (*Artemisia* spp.). Vegetation cover is typically less than 60 percent (Harding 1997). The average daily traffic is 6,000 and 12,600 vehicles per day for SR 28 and US 50, respectively.

The east shore of Lake Tahoe receives thousands of visitors each year, primarily to enjoy the beaches. Negative impacts of such use include roadside parking and impromptu startup trails created by beach users, which cause increased erosion. Moreover, roadside parking impacts erosion control and water quality improvements implemented by NDOT.



Figure 3.1 NDOT BMP monitoring sites.

Table 3.1 Site characteristics.

Site	Area (Ac)	% Imp Area <sup>1</sup>	Onsite Design Peak Flows (cfs)	Offsite Design Peak Flows (cfs)	Average Daily Traffic (Vehicles/day)	Land Use	Soil Type	Annual Offsite Sed. Vol (ft <sup>3</sup> )	Annual Onsite Sed. Vol (ft <sup>3</sup> )	Tc <sup>2</sup>
NDOT2	0.37	100	1.24	N/A	6,000	Rural Hwy	CaF	56	78	2.5
NDOT3	0.72	100	2.05	N/A	12,600	Rural Hwy	UmE	-	12	10.5
NDOT4	0.24	100	0.64	N/A	6,000	Rural Hwy	CaF	-	23	3.9

1. Impervious surface area. 2. Time of Concentration (time for water to flow from the most remote point of drainage area to BMP) in minutes.

Much of the adjacent land along the roadway corridors is relatively undisturbed U.S. Forest Service land, Nevada State Parks or prime residential real estate. The difficulty in acquiring right-of-way on environmentally sensitive land or expense of prime private property limits NDOT's stormwater treatment options.

To date, 11 miles of roadway have been retrofitted with typical highway BMPs. These include sediment traps, sand/oil separators, modified drop inlets with sediment storage that allow infiltration, sediment and infiltration basins. The Nevada Department of Transportation will spend over \$100 million by 2010 on erosion control and water quality improvements to its roadways in the Lake Tahoe basin.

### General Design Criteria

Development of the NDOT MPECSWM was a partnering effort with input from numerous Lake Tahoe basin stakeholders including the Tahoe Region Planning Agency, Federal Highway Administration, Nevada Division of Environmental Protection, Nevada State Lands, Nevada State Parks, Caltrans and the U.S. Forest Service (Haring, 1998). Erosion control and stormwater quality management are addressed using two strategies, source control and treatment control methods. Source control strategies are efforts to prevent sediment from entering stormwater by protecting roadway cut and fill slopes from the erosive forces of wind and rain. Typical source control methods include stabilizing the toe of slopes, applying rock riprap on slopes 1:1.5 (H:V) and steeper, and revegetating areas where success is most likely. Treatment control methods are designed to remove nutrient and sediment from stormwater runoff. Strategies for treating roadside drainage and sediment interception design criteria were also developed through the partnering process. Agreed-upon design criteria are as follows. Sand/oil separators are installed where paved turnouts, in close proximity to the lake, provide room to park 15 or more cars. Sediment catchment facilities are installed where sediment deposition from upstream cut slopes is substantial.

Sediment and infiltration basins are constructed where favorable topography and adequate area exist along the roadside and where traffic safety standards are not jeopardized. The 20-year, 1-hour storm event, typically assumed as 1 inch of rainfall, is the target criteria used by the TRPA for sizing infiltration and sediment basins (TRPA, 2002). Most basins along NDOT's roadways are not large enough to hold that volume, as the steep topography and lack of right-of-way make this criterion difficult to meet. In areas where favorable site

conditions exist, but runoff exceeds the 20-year, 1-hour volume, sediment basins may still be constructed, allowing for some infiltration of highway runoff. State Route 28 drainage facilities are designed to pass the 10-year storm for onsite and the 25-year storm for offsite (NDOT, 1998). US 50 has a minimum design storm return period of 25 years for onsite drainage systems and 50-year storm for offsite flow conveyance.

The control of erosion is a major goal of the MPECSWM and TRPA. Treatment control facility design along NDOT roadways is influenced by four sources of sediment production (Harding, 1998). Sources include erosion from rainfall and snowfall runoff events, erosion of cut and fill slopes adjacent to the highway, channel degradation from concentrated stormwater, and deicing sand placed during winter months. Sediment that would be generated from cut and fill slopes was estimated using the Revised Universal Soil Loss Equation. Additionally, estimates of average deicing sand applications for SR 28 and US 50 were used for sizing of sediment capture structures. Harding (1998) estimated annual sediment generation along SR 28 at 2,622 ft<sup>3</sup>/yr from cut and fill slopes and 3,007 ft<sup>3</sup>/year from winter maintenance activities. Source control improvement, such as riprap placement and slope revegetation, are expected to yield an approximate 40 percent reduction, estimated at 1573 ft<sup>3</sup>/year (Harding, 1998). Treatment control structures provide 1,573 ft<sup>3</sup> of sediment storage. The Nevada Department of Transportation maintenance crews applied 8721 ft<sup>3</sup> of road sand along SR 28 during the winter of 2002/2003. Records show 15,535 ft<sup>3</sup> of sediment were recovered from sweeping operations along SR 28 during the same time period (Jeffery Dodge, 2004, personal communication, NDOT Maintenance Manager Coordinator).

Estimated annual sediment production along US 50 is 8,147 ft<sup>3</sup>/yr and 3,357 ft<sup>3</sup>/year from adjacent cut and fill slopes and winter sanding operations, respectively (Harding, 1998). Slope-generated sediment is expected to be reduced to 7,518 ft<sup>3</sup>/yr by source control improvements such as riprap. Treatment control facilities are designed to capture sediment not contained by source control improvements. The volume provided by proposed treatment control structures along US 50 is 3,460 ft<sup>3</sup>. Winter maintenance operations applied a total of 6,426 ft<sup>3</sup> of road sand to US 50 in the winter of 2002/2003. A total volume of 7,263 ft<sup>3</sup> was recovered from sweeping operations from June 2002 through July 2003 (Dodge, 2004)

### **Sampling Methodologies**

Runoff samples at all three sites were collected using automated samplers. Flow measurements were taken using Palmer Bowlus flumes at the sediment trap and Stormceptor® sites. Secret Harbor Creek flows were measured with a Parshal flume. Pressure transducers were used to measure and determine continuous flow in Secret Harbor Creek and flow into and out of each site during storm events. Probes recording turbidity, electrical conductivity (EC) and water temperature were installed at each sampling location. Sandbag berms were used to direct flow through sampling devices during storm events. Solar panels provided power for instrumentation.

Sample collection was triggered on the basis of outflow. Samples were taken every half hour, 10 minutes and 1 hour at NDOT 2, NDOT 3 and NDOT 4, respectively. Dataloggers stored data and transmitted real time information back to the DRI via cell phone, allowing for real-time assessment of ongoing storms. Figure 3.2 shows the setup configuration in the sediment trap at NDOT 2. Shown are the three probes and sampling tube for the automated sampler.



Figure 3.2. Sample collection tube, temperature, EC and turbidity sensors within sediment trap at NDOT 2.

Sample bottles were collected within 24 hours after each storm event and taken to the DRI for analyses. Nutrient analyses included total Kjeldahl nitrogen (TKN), dissolved TKN (TKNsol), nitrate, nitrite, ammonium, total phosphorus (TP), TPsol (dissolved TP), orthophosphate ( $\text{OPO}_4$ ), TSS and turbidity. Ammonium and nitrite concentrations were analyzed on two occasions and found to be at very low concentrations and therefore not measured again. The amount of sediment captured in the sediment trap was measured after each storm event.

Outflow samples were taken at the end of the culvert pipes at NDOT 2 and NDOT 4, not accounting for possible bypass flows. Therefore, efficiency calculations were for the entire BMP system that included bypass flows. Field personnel did not observe storm events large enough to cause bypass flows for either NDOT 2 or NDOT 4.

Due to a construction error, stormwater discharge through the sediment basin flowed over a side berm rather than through the overflow section. Hence, outflow data records do not accurately reflect actual discharge from the basin. Repairs were made in July 2003. This error may have affected the results of storm events from November 2002 through August 2003.

BMP efficiencies for each runoff event were calculated by subtracting the nutrient outflow load from the nutrient inflow load and dividing the difference by the inflow load. Total loads (TL), in grams, for each runoff event were calculated using Equation (1)

$$TL = \sum [C_i(Q_i\Delta t_i)] \quad (1)$$

where  $C_i$  = pollutant concentration (mg/L) during sample interval,  $Q_i$  = flow (L/min) during sample interval, and  $\Delta t_i$  = time interval.

Equation (2) is a summation of all inflow and outflow loads used in calculating BMP efficiencies (E) for the entire monitoring period. Due to the small watershed size relative to the BMP flow capacity and lack of precipitation, bypass flows did not occur during any runoff event for the monitoring period.

$$E = \frac{\sum Load_{in} - \sum Load_{out}}{\sum Load_{in}} \quad (2)$$

Event mean concentration (EMC) values were calculated for every storm event using Equation (3). The EMC is defined as the average pollutant concentration (mg/L) present in the total volume of runoff from a storm event and was calculated by the following equation:

$$EMC = \frac{\sum [C_i(Q_i\Delta t_i)]}{\sum (Q_i\Delta t_i)} \quad (3)$$

where  $C_i$  = pollutant concentration (mg/L) of sample interval,  $Q_i$  = (L/min) flow during sample interval, and  $\Delta t_i$  = time interval.

## **CHAPTER 4. NDOT 2 SEDIMENT TRAP**

### **Site Description**

The sediment trap site is located along the lakeside of SR 28 in Carson City at approximately milepost 3.4 and discharges directly into Secret Harbor Creek, approximately 0.7 miles upstream of the confluence with Lake Tahoe (Figure 3.1). This site collects stormwater runoff from two lanes of roadway with an average daily traffic (ADT) volume of 6,000 vehicles per day. Offsite flow contributions are negligible. The total onsite area is 0.37 acres with the 10-year design storm peak flow of 1.24 cfs (Harding, 1998). The roadway longitudinal and transverse slopes are 5.56 percent and 0.5 percent, respectively.

Harding (1998) reports that an estimated 134 ft<sup>3</sup>/yr of sediment would be generated within this catchment basin from slope erosion for post-project conditions and road sand applications. Estimated sediment production from a single 130-ft cut slope is 100 ft<sup>3</sup>/yr for pre-project conditions and 56 ft<sup>3</sup>/yr for post-project conditions (after riprap application). The slope varies from 0 feet to 29 feet in height with a slope angle of 0.5:1 (H:V) and an exposed cut slope area of approximately 14,585 ft<sup>2</sup> (Harding 1998). Vegetation cover varies from 0 to 25 percent. Rock outcroppings are moderately to deeply weathered. The soil type is Cagwin-Rock Outcrop Complex (CaF) with a particle size distribution of greater than 80 percent sand, hydrologic soil group C and a high erosion hazard (USDA Soil Conservation Service, 1974). Road sand applications yield an estimated 78 ft<sup>3</sup>/yr for this catchment basin. Sediment capacity provided by the sediment trap at this location is 170 ft<sup>3</sup>.

### **Best Management Practice – Structures Installed**

A Stormceptor® was originally intended for this location because of the perennial creek crossing. However, a large boulder was encountered during excavation, preventing the Stormceptor® installation. A triple-barrel sediment trap was substituted, as it could fit in the narrow space between the buried boulder and Secret Harbor Creek.

A typical sediment trap is a very simple design typically consisting of two 36 inch by 8 foot corrugated metal pipes (CMP) placed vertically in the ground with 36-inch-diameter grates placed on top (Figure 4.1a and 4.1b).

Each pipe is connected near the top by an 18 inch by 7.5 foot CMP. Low-flow stormwater runoff typically passes into the upstream grate. Stormwater runoff rises within the first pipe, flowing into subsequent pipes, and discharging into a riprap outlet. These traps are designed and sized simply to capture roadway runoff and sediments from adjacent cut slopes and deicing activities. The sediment trap at NDOT 2 consists of three barrels due to the large, highly erosive cut slope immediately upstream of this location (Figure 4.2).

From August 2001 through April 2002, Caltrans monitored similar double-barrel sediment traps at two locations within the Tahoe basin (Caltrans, 2002). One objective of the study was to assess the effectiveness of this type of BMP to reduce nutrient and suspended sediment concentrations in highway runoff.

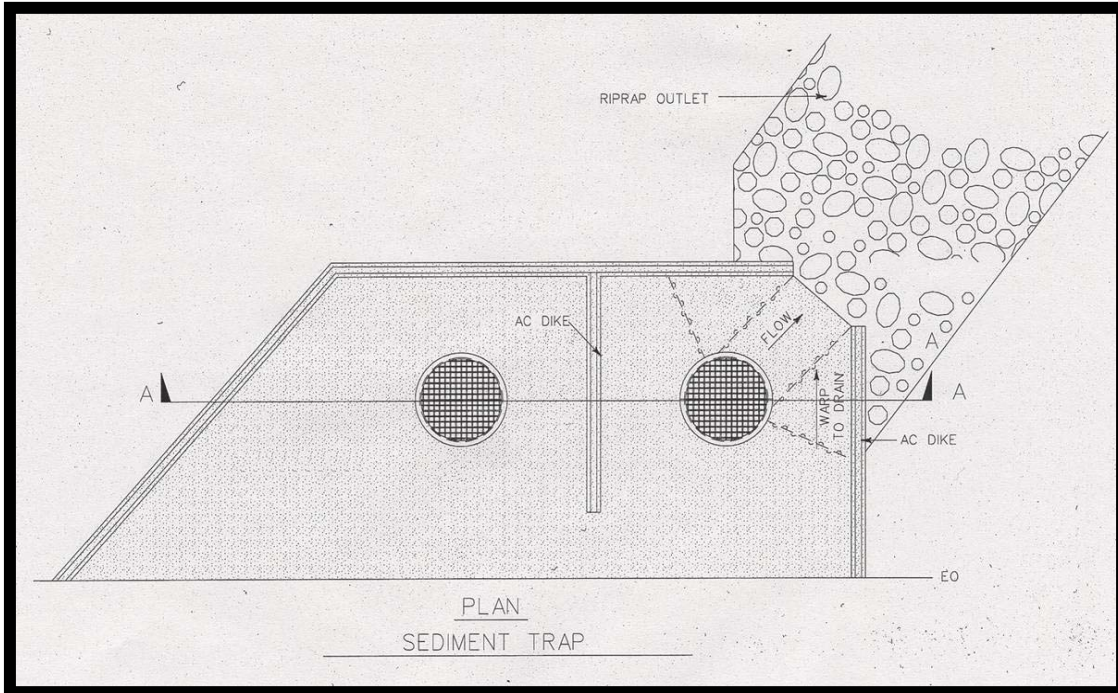


Figure 4.1a. Plan view of typical NDOT double barrel sediment trap BMP (Section A-A shown in Figure 4.1b).

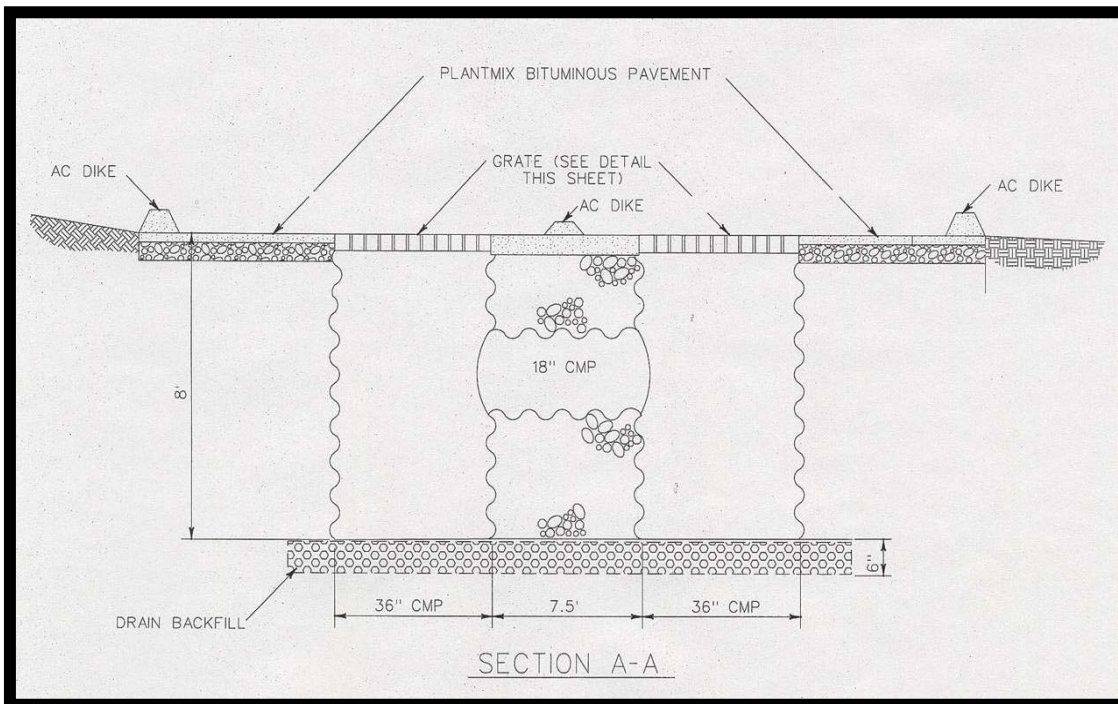


Figure 4.1b. Cross-sectional view of a typical NDOT sediment trap BMP.





Figure 4.2. Triple-barrel sediment trap at Secret Harbor Creek.

For comparison purposes, sediment trap monitoring studies performed by Caltrans at two locations in the Tahoe basin are provided in this report. Table 4.1 lists selected nutrient and suspended sediment EMC values from the Caltrans 2001 to 2002 monitoring season. Listed EMCs are combined influent and effluent data for each site. Caltrans used the paired t-test to determine if runoff through the sediment trap produced statistically different results from inflow values. Statistically significant results are indicated by the word “Yes” in the far-right column of Table 4.1. Insignificant results were indicated by the word “No.” P-values of 0.1 or less were considered significant in the Caltrans report.

Table 4.1. Selected sediment and nutrient ranges of combined influent and effluent data from Caltrans sand trap effectiveness studies of 2001 to 2002 (Caltrans, 2002).

Constituent	No. of Samples	Mean (mg/L)		Mean Standard Deviation		Inf/Eff Difference (%)	Statistically Different (p<0.1)
		Influent	Effluent	Influent	Effluent		
TSS	25	657	422	505	299	36	Yes
Nitrate	25	0.3	0.3	0.3	0.2	-1	No
TKN	25	2.0	1.7	1.8	1.5	12	No
TP	25	0.4	0.4	0.2	0.3	8	No
Dissolved P	25	0.08	0.07	0.03	0.03	15	Yes
Orthophosphate	25	0.08	0.06	0.04	0.04	24	Yes

Results for NDOT 2 are listed in Table 4.2. P-values of 0.05 or less were considered significant for NDOT data. Although percent efficiency ranges from -20 percent to 35 percent depending on the constituent monitored, all p-values indicate that there is no statistical difference between inflow EMC values and outflow EMC values at the NDOT 2 site. EMC values for NDOT 2 are displayed here for comparisons with the two Caltrans sites. The large, highly erosive cut slope directly adjacent to this site may have affected NDOT 2 efficiency. The sediment trap was reported almost full by mid-April 2003. Increased maintenance at this location would most likely improve overall performance of the sediment trap.

Table 4.2. Selected suspended sediment and nutrient EMC ranges (total runoff volume of 181,693 liters through the sediment trap) from NDOT sediment trap effectiveness studies of 2002 to 2004.

Constituent	No. of Samples	Mean EMC (mg/L)		Standard Deviation		Inf/Eff Difference (%)	P-value (p<0.05)
		Influent	Effluent	Influent	Effluent		
TSS	18	784	483	762	414	35	No
Nitrate	18	0.13	0.15	0.21	0.23	-20	No
TKN	18	2.43	2.14	1.92	1.39	11	No
TP	18	1.08	0.80	1.07	0.53	26	No
Dissolved P	18	0.05	0.05	0.03	0.02	-1	No
Orthophosphate	18	0.030	0.021	0.02	0.01	14	No

### Monitoring Results

Total loads entering and leaving each site were used to calculate BMP efficiency. As noted previously, no bypass flow occurred during the monitoring period; therefore efficiency percentages represent the entire system. Table 4.3 shows total influent and effluent loading and percent differences and p-values for 18 runoff events. As with the p-values for EMCs, p-values for total loading show no statistical difference between influent and effluent concentrations using the criteria that p <0.05 is significant.

Table 4.3. Sediment and nutrient total loads for 18 storms from NDOT sediment trap effectiveness studies of 2002 to 2004.

Constituent	Total Load (g)		Mean (g)		Standard Deviation (g)		Inf/Eff Difference (%)	P-value (p<0.05)
	In	Out	In	Out	In	Out		
	TSS	1,043,590	507,059	1,043,590	28,170	122,225		
Nitrate	188	216	10.5	12.0	19.08	20.09	0	No
TKN	3,395	2264	189	126	393.49	207.73	3	No
TKNsol	722	647	40.1	36.0	72.12	59.38	-14	No
TN	3,590	2432	199	135	411.38	226.49	3	No
TP	1,526	880	85	49	184.39	87.39	21	No
Dissolved P	25	22	1.7	1.4	2.68	1.89	-2	No
OPO <sub>4</sub> -P	46	30	2.6	1.7	5.29	2.09	6	No

Figure 4.3 depicts the total influent and effluent loads to NDOT 2 for 13 runoff events (grams are used rather than pounds due to the small values). Percent reductions for TSS, TP, and TN are 35 percent, 26 percent and 9 percent, respectively. Reduction in nutrient loading is indicated in all cases with the exception of TKNsol and NO<sub>3</sub>, showing an export of 9 percent and 20 percent, respectively. However, p-values indicate no significant difference between nutrient loads entering and exiting the sediment trap. The increase in TKNsol represents a decrease in TKN possibly signifying transformation of TKN to TKNsol within the sediment trap.

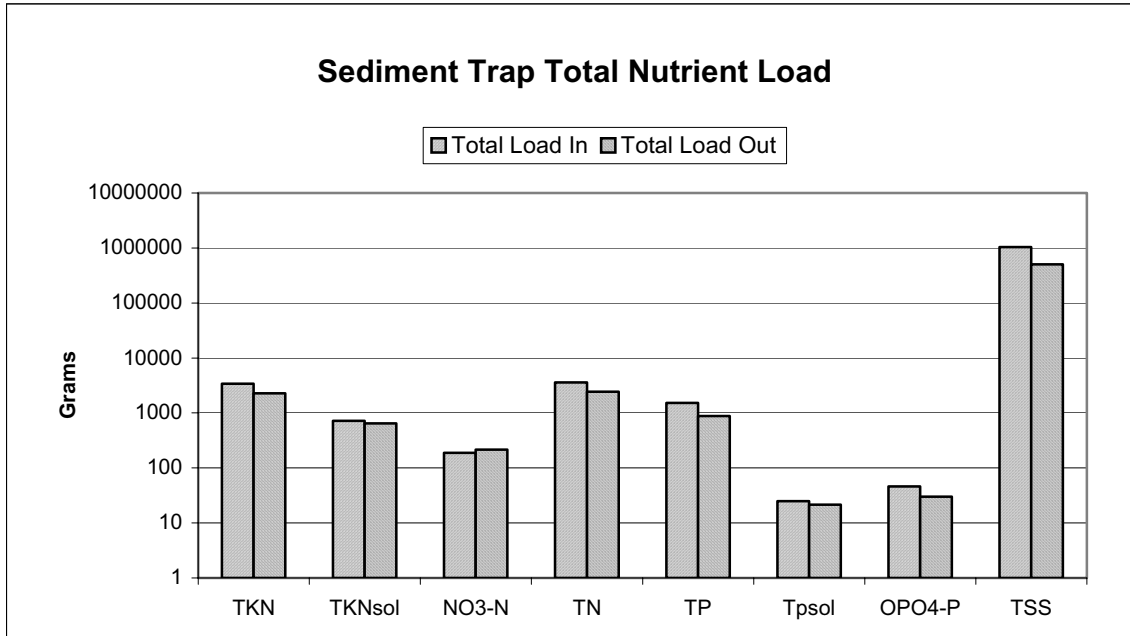


Figure 4.3. Total influent and effluent loads for 18 runoff events from November 2002 through April 2004.

Figures 4.4 and 4.5 show average EMC values and total loads for the study period. Summer EMC values are higher than winter EMC values. Higher EMC values in the summer months may be due to higher rainfall intensity. These values are based on two summer storms and 11 winter storms. In contrast, nutrient loads are greatest in the winter due to greater volume of runoff for winter storms and the application of road which would result in increased TSS and associated TP, Tpsol and OPO<sub>4</sub>-P.

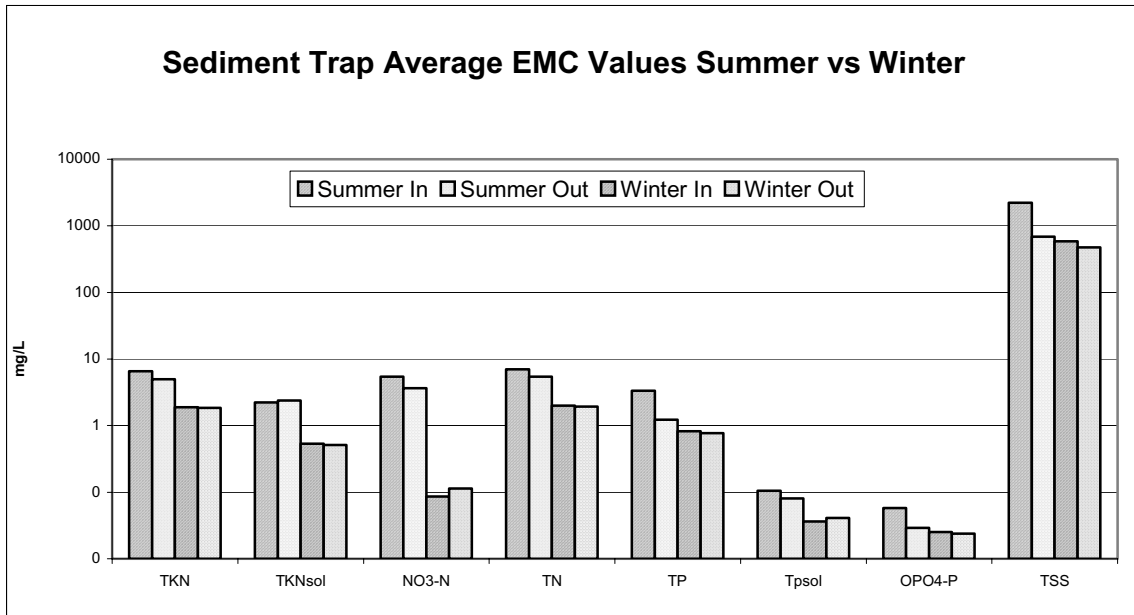


Figure 4.4. Average EMC values summer/winter from November 2002 through April 2004.

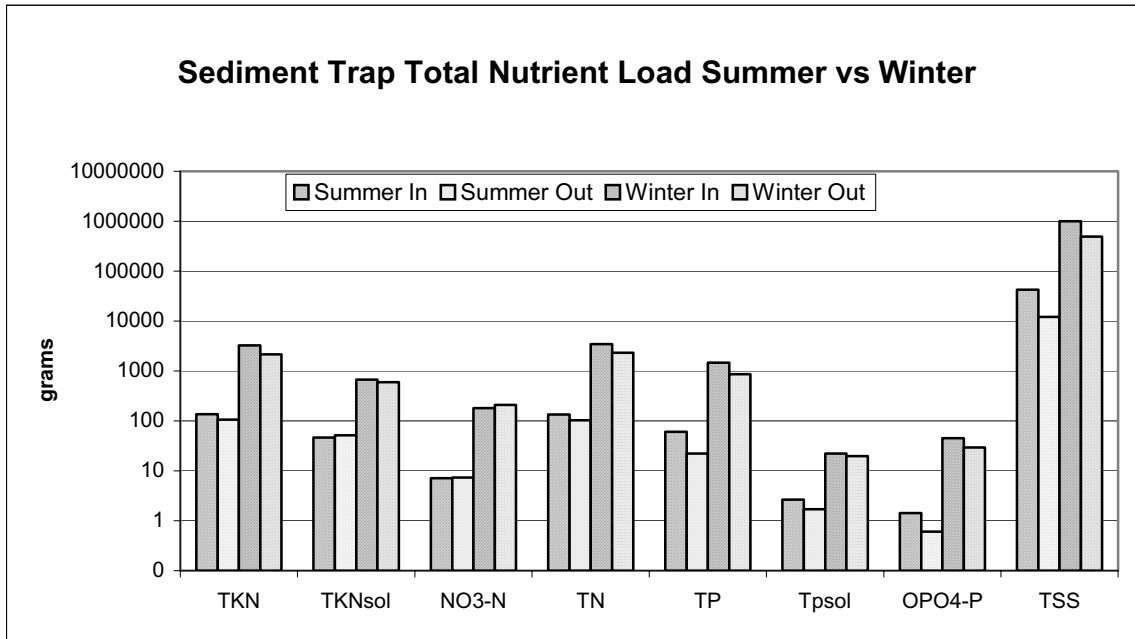


Figure 4.5. Total summer/winter nutrient values from November 2002 through April 2004.

Figures 4.6 through 4.8 show pollutant removal efficiencies as a function of runoff volume. As expected, efficiencies decrease as flows increase, due to re-suspension of sediment within the sediment trap, with negative efficiencies occurring for all pollutants.

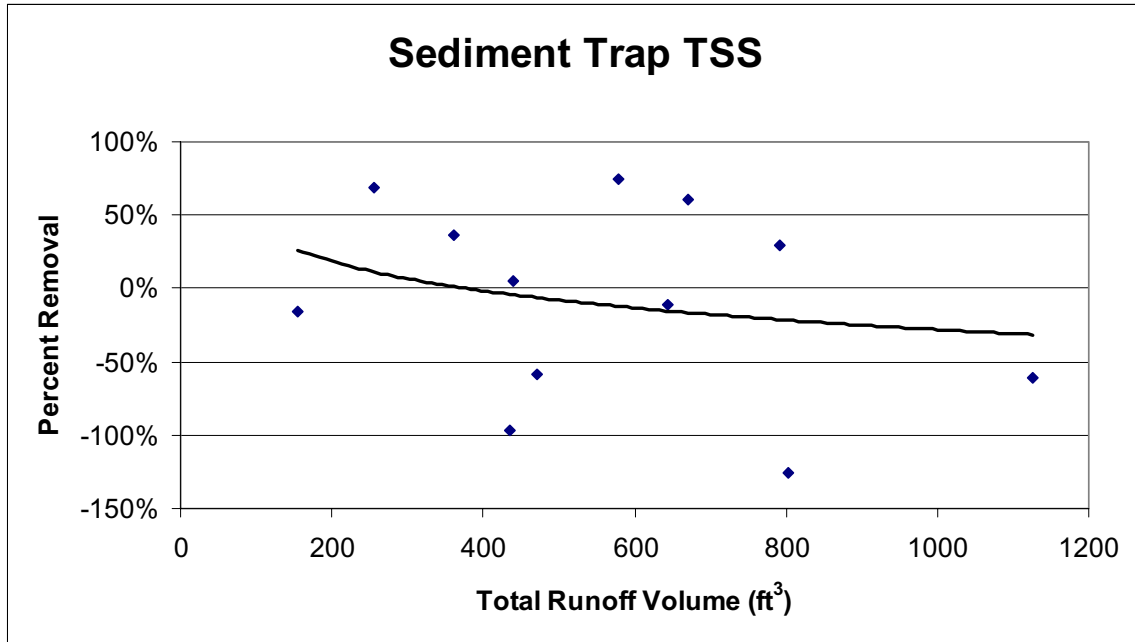


Figure 4.6. Percent removal of TSS as a function of runoff volume for NDOT 2.

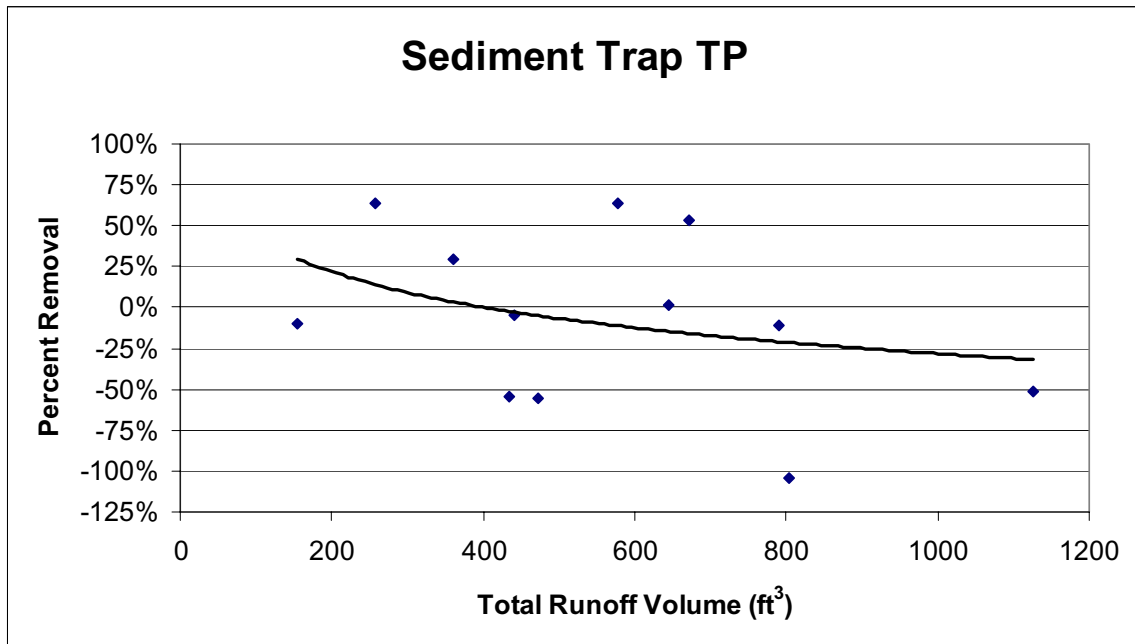


Figure 4.7. Percent removal of TP as a function of runoff volume for NDOT 2.

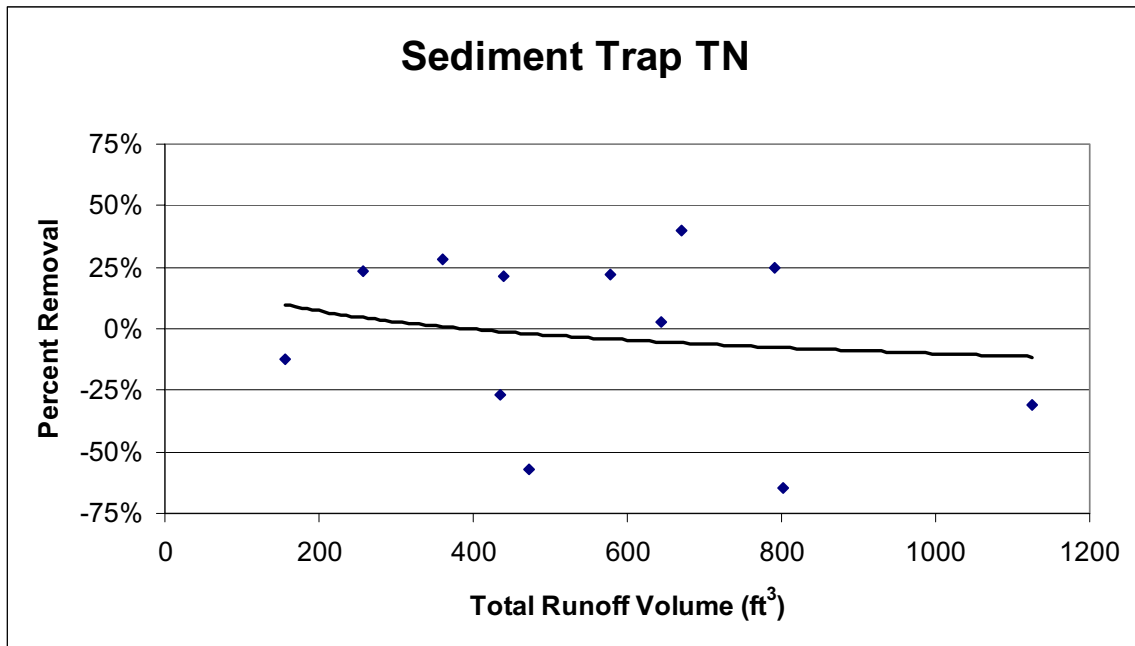


Figure 4.8. Percent removal of TN as a function of runoff volume at NDOT 2.

## CHAPTER 5. NDOT 1 SECRET HARBOR CREEK

### Site Description

Secret Harbor Creek crosses SR 28 at Carson City mile post 3.4 (Figure 3.1). Water quality monitoring was performed upstream and downstream of SR 28 adjacent to the sediment trap (Figure 5.1). Secret Harbor Creek is an ungaged creek of which 1.87 square miles drain to the creek crossing at this location. Soil type is dominated by Cagwin-Rock Outcrop Complex with 30 to 50 percent slopes and the watershed is mostly undeveloped. Vegetation is mainly evergreen forest and with a small percentage of shrub land.



Figure 5.1. Secret Harbor Creek just downstream of sediment trap.

### Monitoring Results

Comparisons of pollutant concentrations upstream and downstream of SR 28 indicate Secret Harbor Creek is, in some instances, impacted by roadway runoff. Figure 5.2 shows TSS upstream and downstream concentrations for three storms on November 8, 2002, April 15, 2003, and June 23, 2003. Only TSS had p-values  $< 0.1$  for all three storms. P-values are 0.006, 0.08, and 0.027 for the November 2002, April 2003, and June 2003 storms, respectively. Figures 5.3 and 5.4 illustrate effects of roadway runoff in Secret Harbor Creek for TP and TN. TP concentrations have p-values of 0.482, 0.12 and 0.05 for the November 2002, April 2003, and June 2003 storms, respectively. Only during the June 2003 storm event did Secret Harbor Creek receive a significant TN contribution from SR 28, a p-value of 0.081. Significant contributions from other nutrients varied from storm to storm.

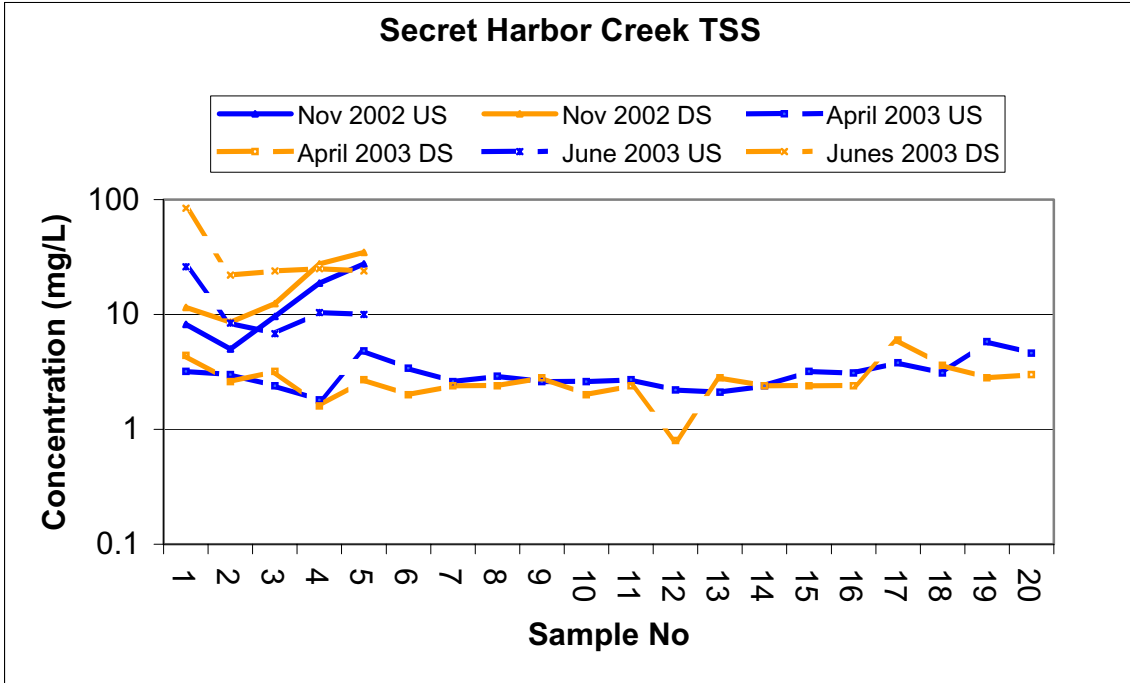


Figure 5.2. Upstream (US) and downstream (DS) TSS concentrations at Secret Harbor Creek.

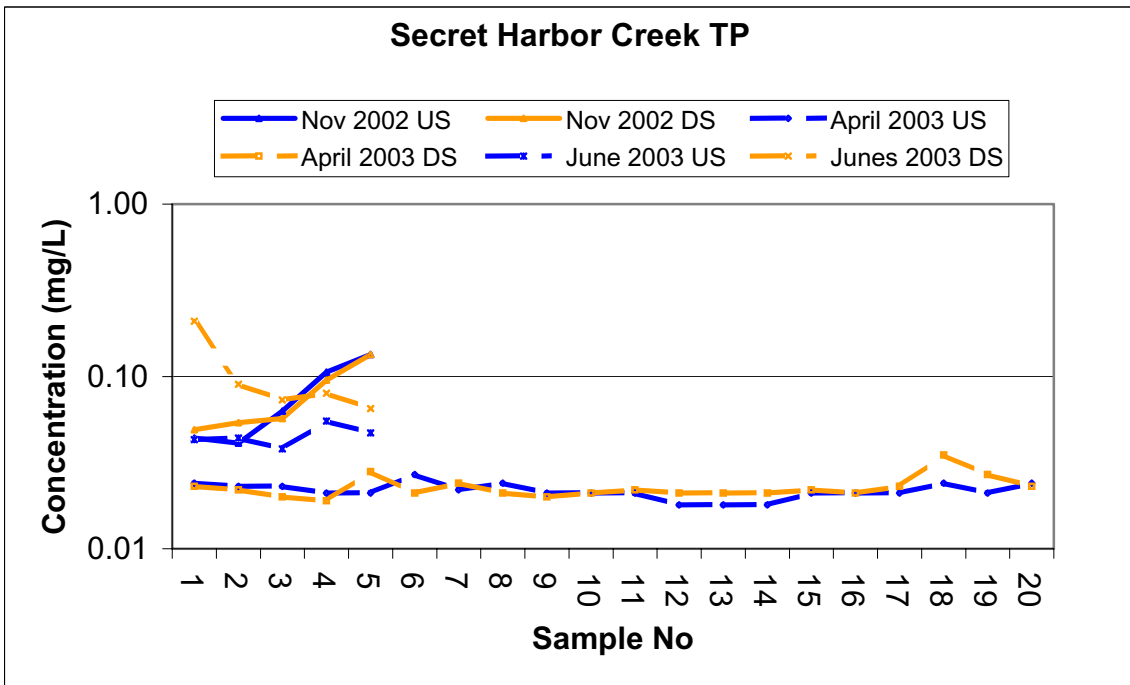


Figure 5.3. Upstream (US) and downstream (DS) TP concentrations at Secret Harbor Creek.



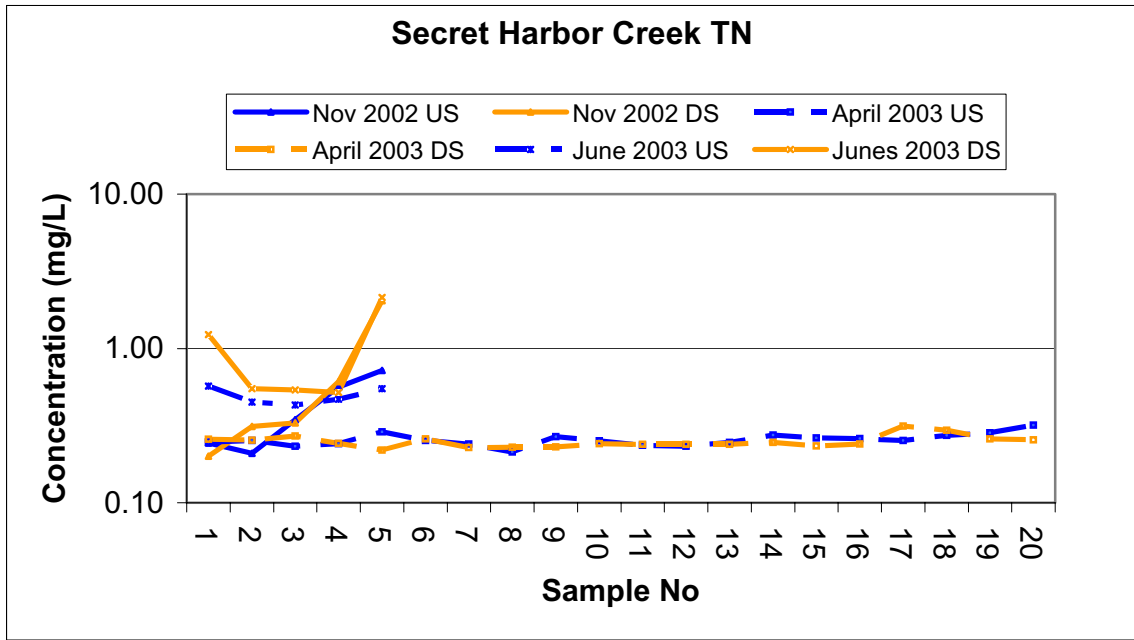


Figure 5.4. Upstream (US) and downstream (DS) TN concentrations at Secret Harbor Creek.

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## CHAPTER 6. NDOT 3 SEDIMENT BASIN

### Site Description

NDOT 3 (sediment basin site) is located along the lakeside of US 50 in Douglas County at approximately milepost 11.5 (Figures 3.1 and 6.1). Stormwater runoff is collected from four lanes of roadway with an ADT volume of 12,600 vehicles per day. Offsite flows (nonhighway runoff) contributions are negligible. The total onsite area is 0.72 acres with the 10-year design peak flow of 2.05 cfs (Harding, 1998). Roadway longitudinal and transverse slopes are 5.5 percent and 3.5 percent, respectively. Basin design storage volume is 413 ft<sup>3</sup> with the total estimated volume of runoff for the 20-year, 1-hour storm at 2,336 ft<sup>3</sup>. Harding (1998) estimates road sand applications during winter months yield an estimated 92 ft<sup>3</sup>/yr for this catch basin.



Figure 6.1. NDOT 3, U.S. Highway 50 sediment basin.

This site is located on Umpa (UmE) soils, classified as a very stony sandy loam found on 15 to 30 percent slopes (USDA Soil Conservation Service, 1974). Umpa soils are in hydrologic soil group C and pose a moderate erosion hazard. Much of the stormwater runoff entering this basin is infiltrated. Overflows discharge into a 60-ft-long riprap channel. The Soil Survey estimates infiltration rates based on UmE soils to be 2.0 to 6.3 in/hr. A percolation test was not performed at this location, therefore the infiltration rate is unknown.

The Tahoe Regional Planning Agency requires treatment of the 20-year, 1-hour storm, which is considered the first flush. Limited right-of-way, steep topography, and

culturally and environmentally sensitive areas limit feasible locations for sediment/infiltration basins. The primary variables for determining viability of different treatment strategies such as sediment basins and infiltration systems are particulate characterization and loading rates (Sansalone *et al.*, 1998). Forebays, settling basins or sinuous flowpaths typically used to settle out and keep suspended solids within the BMP cannot be incorporated into this type of basin, as there simply is no room to do so. Therefore, on the occasions where flow overwhelms the storage capacity of the basin, an export of nutrients and sediment can occur. However, it is thought that some infiltration, notwithstanding the limited volume and poor soils, is better than no infiltration. Dorman *et al.* (1996) reiterate this basic assumption.

### **Best Management Practice - Structure Installed**

Sediment/infiltration basins are typically located in areas where there is a natural depression or where the terrain lends itself to basin construction. Locations that have favorable width, depth, site stability, mild slope and are located outside an archeologically sensitive area or in a stream environment zone are few. Design considerations such as characterization of roadway runoff reaching the structure, soil hydrologic group, soil organic content, soil cation exchange capacity, and settling velocities have not been considered in designs of existing sediment basins. Infiltration rates are determined by percolation tests. The Nevada Department of Transportation sediment basins must be located in areas where maintenance crews can easily access the site for sediment removal. All NDOT sediment basins are lined with interlocking articulated concrete block consisting of 13 inch x 11 ½ inch x 4 ¾ inch open celled blocks tied together with cables. The 20 percent open area allows vegetation establishment and infiltration. The articulated blocks provide a stable hard surface for maintenance crews to remove accumulated sediment without disturbing the underlying soils and with minimal disturbance to established vegetation.

### **Monitoring Results**

Technical difficulties plagued the NDOT 3 sediment basin site. During the original basin construction, the side berm was constructed at an elevation lower than the outlet riprap channel. This error caused stormwater runoff to overflow the side berm rather than flow through the outlet channel. Construction crews corrected the error in August 2003. As a result, accurate outflow loadings could not be calculated for the November 2002 and March 2003 storm events (the only two storms with both inflow, outflow and chemistry data). Problems continued through summer 2003. Automated samplers were originally triggered to take samples upon sensing outflow, however, several storms in April and May did not produce outflow through the basin and therefore chemistry data are not available to calculate inflow loads for several spring storms. One grab sample was taken for the June storm event. Outflow chemistry data are not available for the July storm. Inflow depth sensors failed during the two storms in August 2003.

For small volume storms, the basin has been effective in capturing and infiltrating runoff produced by small storms, as evidenced by the stored storm runoff. As previously stated, an assumed benefit is gained by stormwater infiltration. Although loading data are currently unavailable, concentration values indicate that the basin is effective in retaining and treating nutrients via infiltration. Figures 6.2 through 6.4 show concentration values for TSS, TP and TN from July 2002 through August 2003. Note that November 2002 is a composite

sample. July 2002 and April and June 2003 concentration values are grab samples. Values for all other months are averaged from samples collected during storm events. Inflow concentration values are greater than outflow values, indicating a reduction in pollutant loading through this system.

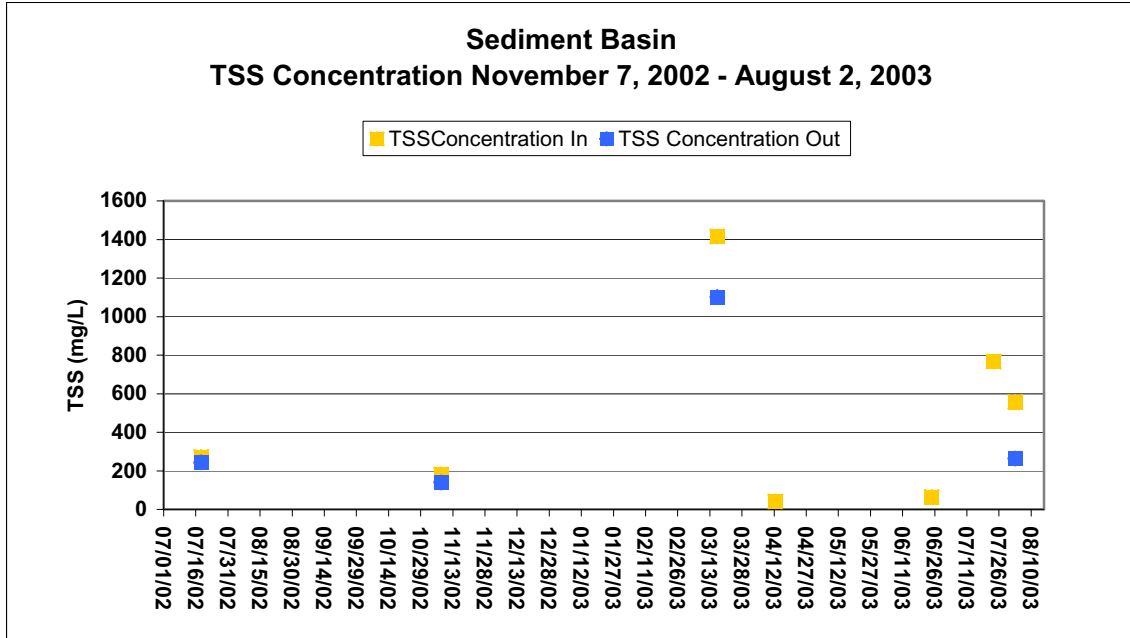


Figure 6.2. NDOT 3 TSS concentrations.

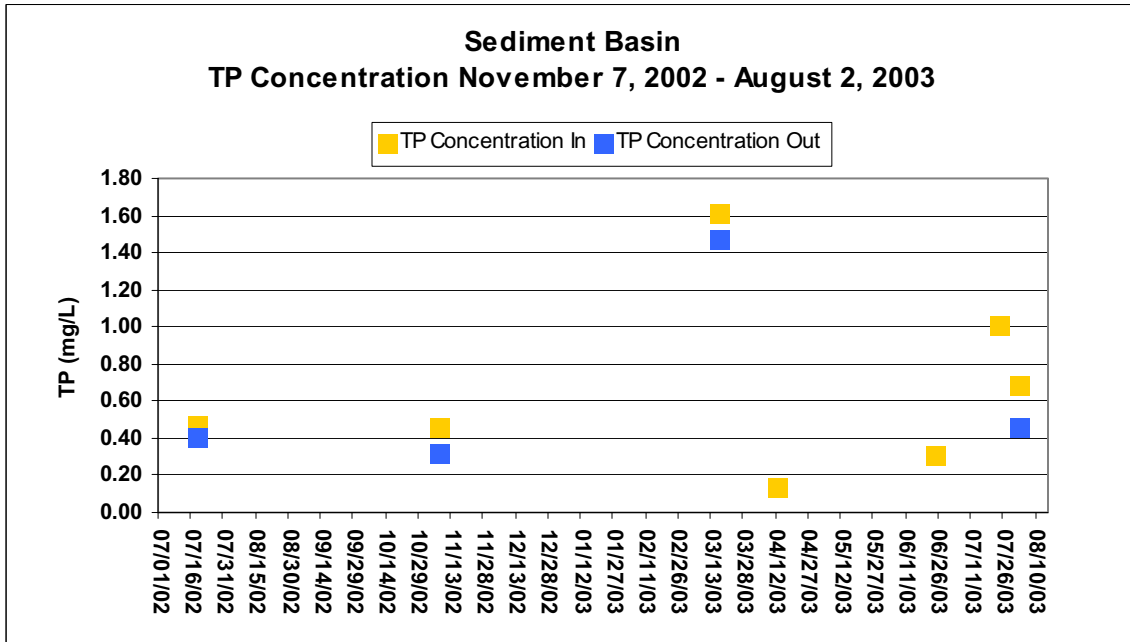


Figure 6.3. NDOT 3 TP concentrations.

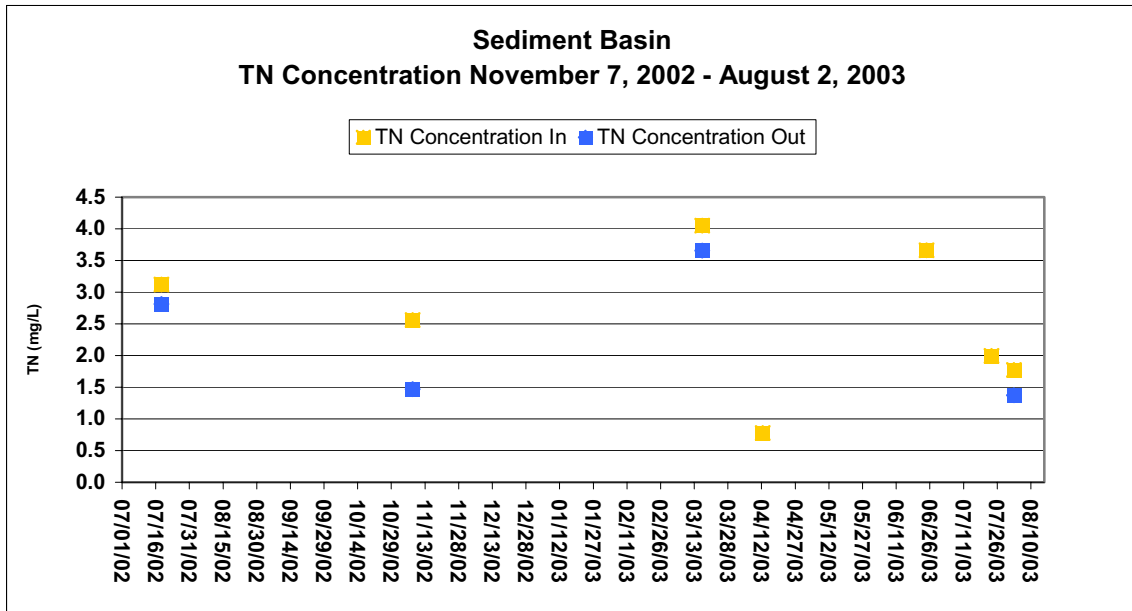


Figure 6.4. NDOT 3 TN concentrations.

## CHAPTER 7. NDOT 4 STUDY SITE

### Site Description

The NDOT 4 study site is located along the lake side of SR 28 in Carson City at CC mile post 3.7 and approximately  $\frac{1}{4}$  mile from the NDOT 2 study site (Figure 3.1). The distance to Lake Tahoe from the discharge point is approximately 0.7 miles. This site collects stormwater runoff from two lanes of roadway with an ADT volume of 6,000 vehicles per day and discharges directly into a stream environment zone (SEZ) (Figure 7.1).



Figure 7.1. NDOT 4 study site.

Offsite flow, nonhighway runoff, contributions are negligible. The total roadway onsite drainage area is 0.25 acre with the 10-year design storm flow of 0.64 cfs (Harding, 1998). The roadway longitudinal and transverse slopes are 4.76 percent and 0.5 percent, respectively.

Harding (1998) reports that 22 ft<sup>3</sup>/yr of sediment are generated within this catchment basin from road sand applications for post-project conditions. The soil type is Cagwin-Rock Outcrop Complex (CaF) with a particle size distribution of over 80 percent sand, hydrologic soil group C, and a high erosion hazard (USDA Soil Conservation Service, 1974).

The NDOT 4 roadway runoff is treated by a Stormceptor® inlet (Figure 7.2). Stormceptor® is a patented stormwater treatment structure that removes oil and sediment from stormwater runoff. It has been on the market for over 10 years. The Stormceptor® unit can be divided into two components, the lower treatment chamber and the upper by-pass chamber separated by a fiberglass insert. Storm flows entering the unit, are diverted by a u-shaped weir downward into the separation/holding chamber. Pipes aligned perpendicular to the inflow pipe direct stormwater around the circular walls of the chamber and horizontally

toward the pipe outlet. Sediment accumulates at the chamber bottom and oil is trapped underneath the fiberglass insert for removal at a later date (Figure 7.3.a.). During high-flow events beyond the Stormceptor® treatment capacity, flows are diverted over the weir and through the bypass chamber directly to the outlet pipe (Figure 7.3.b). Previously-captured sediment and oil are left relatively undisturbed at the bottom of the chamber.



Figure 7.2. NDOT 4 Study Site, Stormceptor® unit.

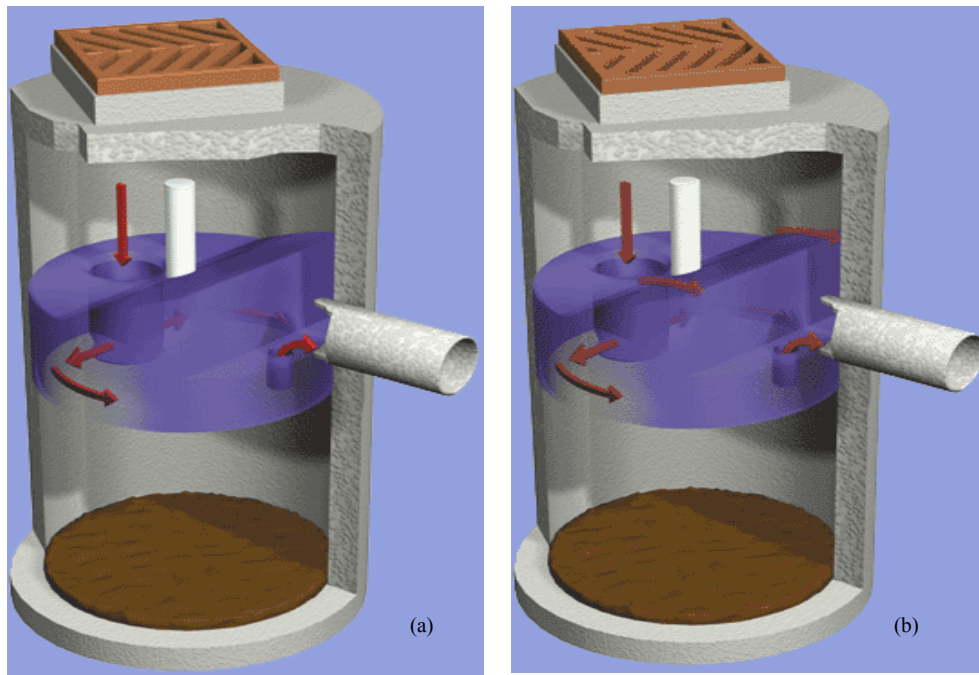


Figure 7.3. (a) Design storm treatment, and (b) high-flow bypass.



## **Best Management Practice Description**

Product literature indicates that up to 80 percent of fine and coarse sediment loads can be captured from storm flows treated by the Stormceptor® (Stormceptor, 2001). Nutrient removal rates for nitrogen and phosphorus are not specifically claimed by the manufacturer. However, several studies (e.g., Yu *et al.*, 200; Waschbush, 1999) have investigated EPA-recommended urban runoff constituents including TSS, TN, TP and oil and grease removal capabilities of the Stormceptor. The Virginia Department of Transportation sponsored a study evaluating the use of several ultra-urban BMPs including the Stormceptor® (Yu *et al.*, 2001). Removal efficiencies were based on EMCs. The study found that removal rates for TSS, TP, and TN were 57 percent, 66 percent and -27 percent, respectively. Cost comparisons between BMPs found that the Stormceptor®-associated cost per percent TSS removed was \$76.92. In comparison, a bioretention area, comprising of a grass buffer strip, ponding area, and planted area, monitored during the same study period, cost \$12.19 per percent TSS removed.

The U.S. Geological Survey performed an extensive study of a Stormceptor® unit treating a 4.3-acre public works maintenance yard (Waschbush, 1999). Removal efficiencies of the treatment chamber were found to be 25 percent, 19 percent and 21 percent for TSS, TP, and dissolved P, respectively. Total efficiencies for the entire unit, which included flows bypassing the treatment chamber, were 21 percent and 17 percent for TSS and TP, respectively. It was noted that the unit was improperly installed, causing bypass flows to occur at a flow rate of 500 gal/min rather than the 800 gal/min published in the product literature. Overall efficiency of the unit was affected by the improper installation but the efficiency of the treatment chamber was not.

A Stormceptor® model STC 900 unit was installed at NDOT Site 4. This model has a total holding capacity of 950 gallons and a sediment holding capacity of 75 ft<sup>3</sup>. At the time of project design, Stormceptor® sizing was based on a flow rate and total acreage treated. The Stormceptor® model STC 900 is recommended to treat a maximum flow rate of 0.635 cfs (287 gal/min) and a maximum impervious area of 0.45 acres for areas designated as sensitive. The NDOT 4 site has 0.25 acres of impervious surface that results in a design storm discharge of 0.64 cfs. The STC 900 is well within the design criteria of this site. Field observations indicate that, throughout the study period, storm flows were never large enough to bypass the treatment chamber. The maximum flow rate recorded at this site was 0.07 cfs (36 gal/min) recorded on January 23, 2003.

It should be noted that Stormceptor® units may now be sized according to sizing software that simulates five different physical models to estimate TSS removal. These include a pollutant buildup model, a pollutant wash-off model, and the EPA SWMM Version 4.3 model.

## **Monitoring Results**

Total loads entering and leaving the treatment chamber were used to calculate BMP efficiency. As noted previously, no bypass flow occurred during the monitoring period; therefore, efficiency percentages represent the entire system. Table 7.1 shows total influent and effluent loads and percent differences and p-values. In contrast to the NDOT 2 site, P-values for total loads show a statistical difference between all influent and effluent loads with the criteria that  $p < 0.05$  is significant.

Table 7.1. Total sediment and nutrient loads for 16 storms from NDOT Stormceptor® effectiveness studies of 2002 to 2004.

Constituent	Total Load (g)		Mean (g)		Standard Deviation (g)		Inf/Eff Difference (%)	P-value (p<0.05)
	In	Out	In	Out	In	Out		
TSS	173,639	119,723	19,293	7,043	1,8045	13,109	31	Yes
Nitrate	29	10	3.44	0.63	3.51	1.19	65	Yes
TKN	618	490	68.68	28.82	46.19	39.23	21	Yes
TKNsol	199	145	22.10	8.56	16.42	9.99	27	No
TN	613	483	68.16	28.41	49.14	40.34	21	Yes
TP	227	170	25.27	9.98	22.19	16.88	25	Yes
Dissolved P	12	7	1.36	0.43	0.94	0.52	40	Yes
OPO <sub>4</sub> -P	7	3	0.79	0.21	0.60	0.30	51	Yes

Figure 7.4 shows the total influent and effluent loads for the NDOT 4 site (grams are used rather than pounds due to the small values). Percent reductions for TSS, TP, and TN are 31 percent, 25 percent and 21 percent, respectively. Reduction in nutrient loads is indicated in all cases including dissolved species. Significant differences exist between flows entering and exiting the Stormceptor® for all nutrients and TSS.

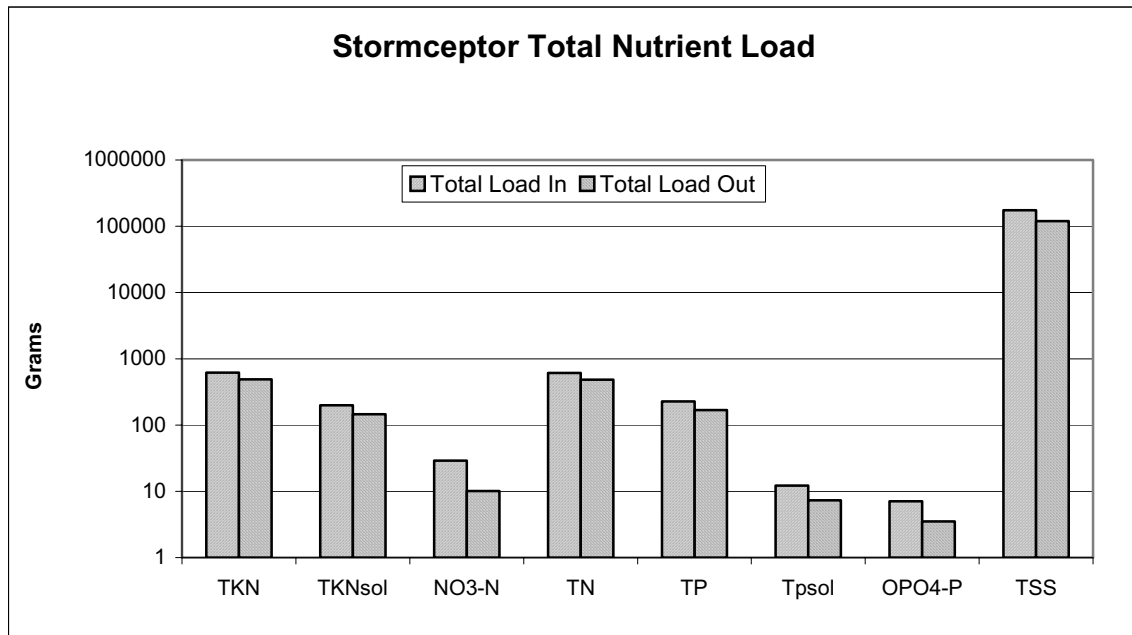


Figure 7.4. Total Nutrient and TSS Loads from November 2002 through November 2003.

Figures 7.5 and 7.6 show average EMC values and total loads for the study period. Most summer EMC values are higher than winter EMC values including TSS. However, these values are based on four summer storms and 13 winter storms. Phosphorus and TSS

loads are greatest in the winter, whereas nitrogen loads are generally similar or less in the winter.

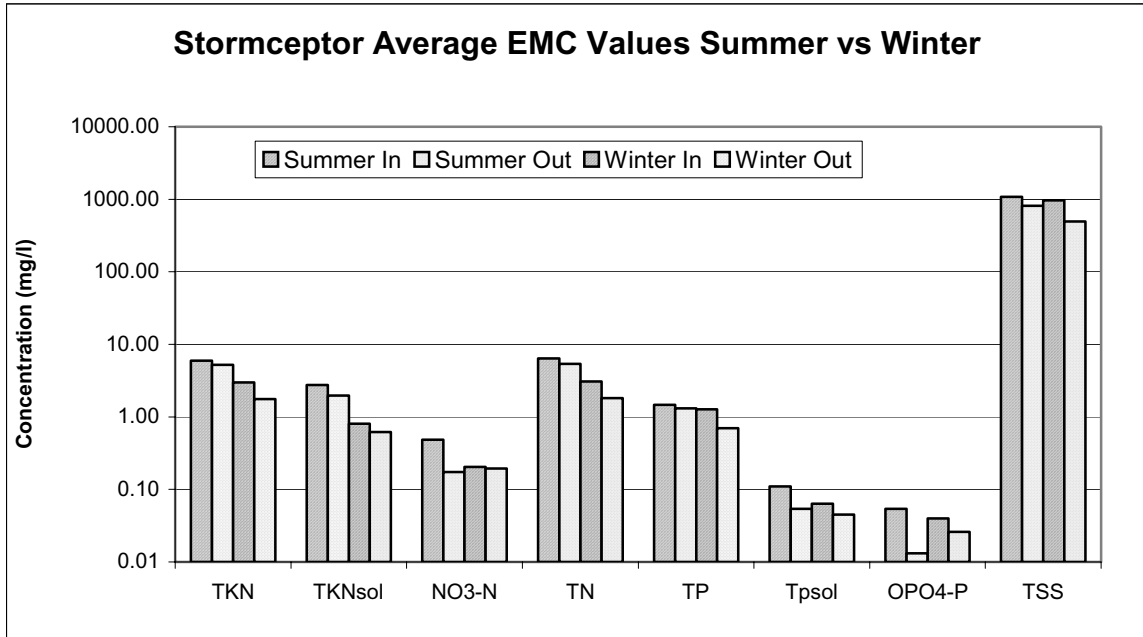


Figure 7.5. Average EMC values summer/winter from November 2002 through November 2003.

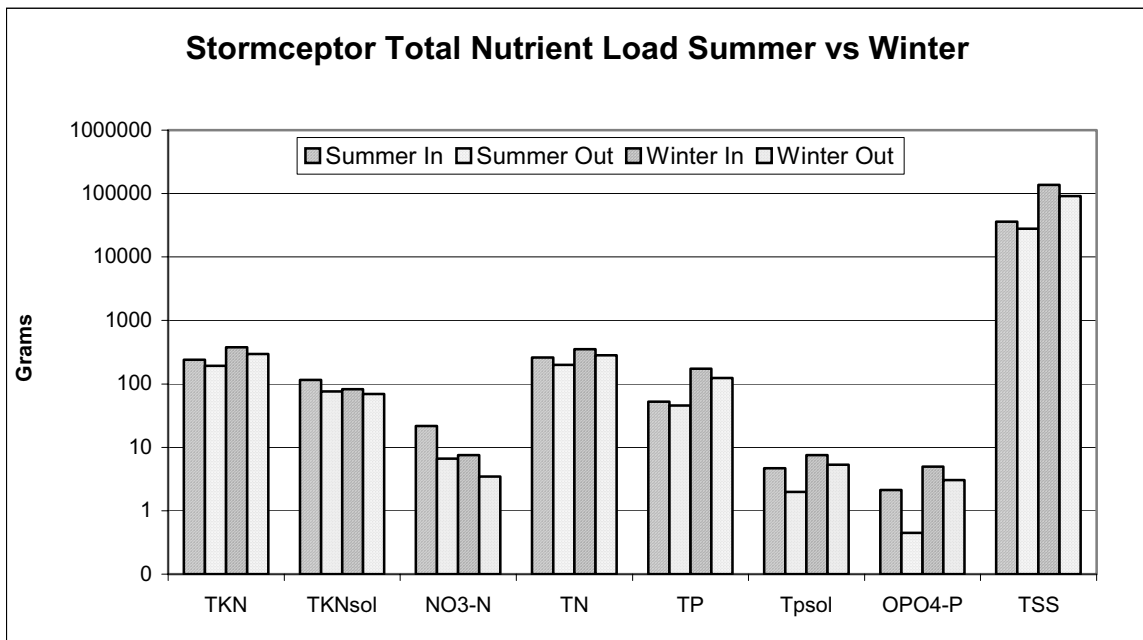


Figure 7.6. Total summer/winter nutrient values from November 2002 through November 2003.

Figures 7.7 through 7.9 show removal efficiencies as a function of runoff volume. As expected, efficiencies decrease as flows increase. However, in contrast to the sediment trap, flow increases do not cause best-fit line for removal efficiencies to fall below zero.

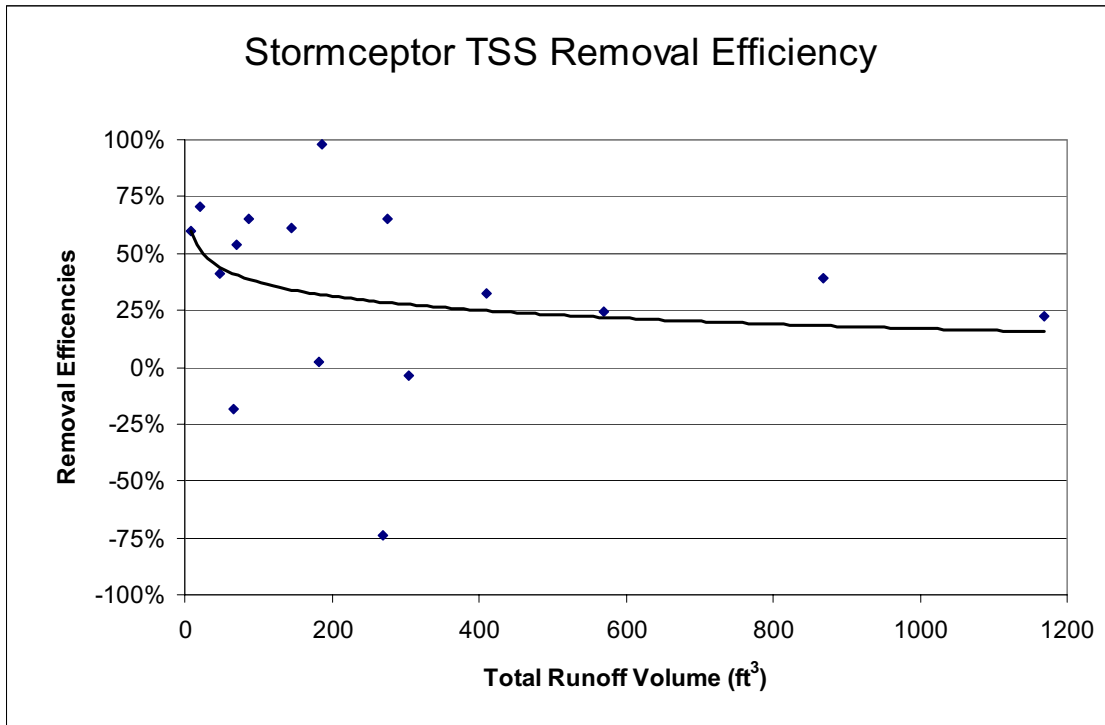


Figure 7.7. TSS as a function of runoff volume for NDOT 4.

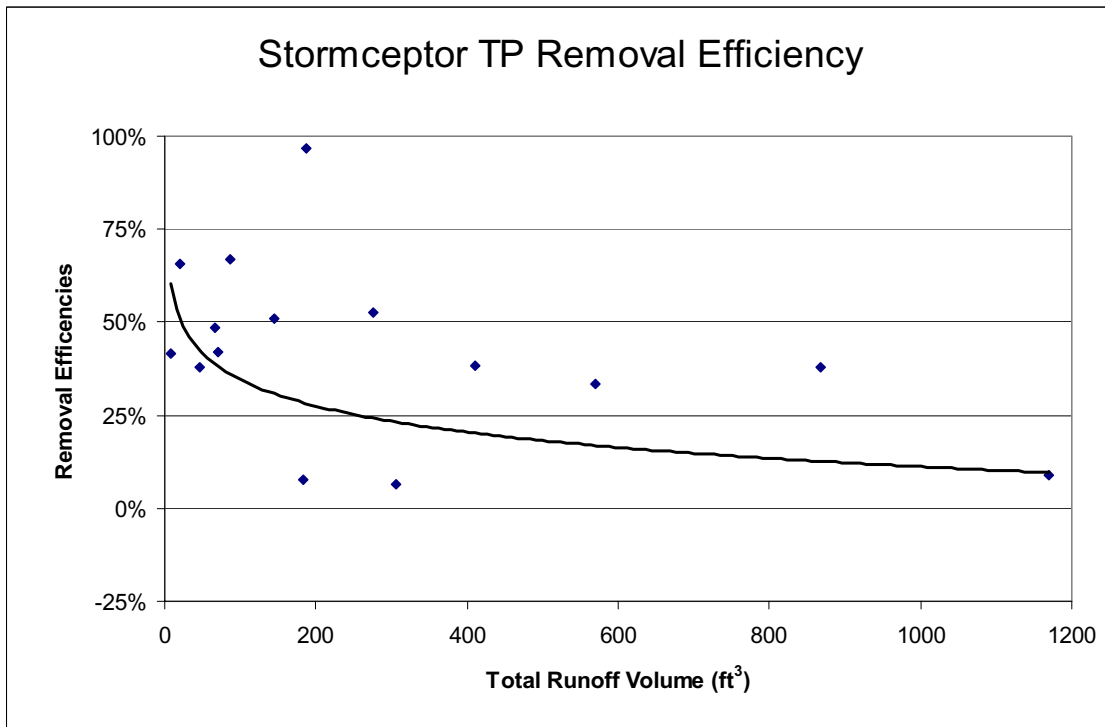


Figure 7.8. TP as a function of runoff volume for NDOT 4.

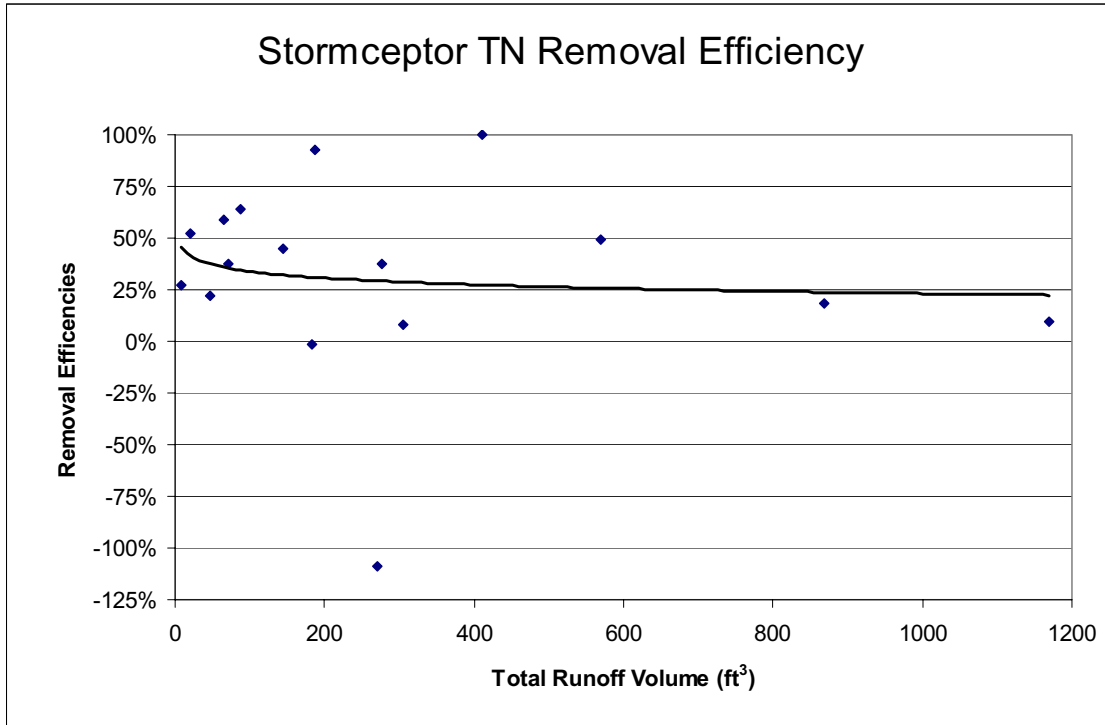


Figure 7.9. TN as a function of runoff volume at NDOT 4.

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## CHAPTER 8. COMPARISONS

During the period July 2002 through April 2004, nutrient data from roadway runoff were collected for a total of 25 storms at NDOT 2, nine storms at NDOT 3, and 21 storms at NDOT 4.

Due to sampling problems, efficiency comparisons were calculated for only 18 out of the 25 storms at NDOT 2. Nutrient loading for the current study period, could not be calculated for NDOT 3 due to faulty construction and difficulties with inflow depth sensors on various occasions. As previously noted, the sediment basin outlet elevation was slightly higher than the west berm, causing a portion of the flows during the November 2002 and March 2003 storms to bypass the outlet, thus prohibiting meaningful load calculations. Seventeen of the 21 storms were used for comparisons at NDOT 4.

During the sampling period, three types of storms were experienced along SR 28 and US 50: frontal storms, winter snowstorms, and summer convective storms. For the purpose of this study, winter storms were classified as those storms where roads required snow plowing and sand/salt treatments. Maintenance records show that sand and salt were applied during and after every frontal and winter storm at all monitoring locations. Winter storms, where road sanding and plowing activities took place, occurred between November and May of each year. Sixteen winter storms were sampled at NDOT 2 and 13 at NDOT 4. Summer thunderstorms accounted for two storms at NDOT 2 and four storms at NDOT 4. Overall, average nutrient loads were higher for summer storms than winter storms (Figures 8.1 and 8.2).

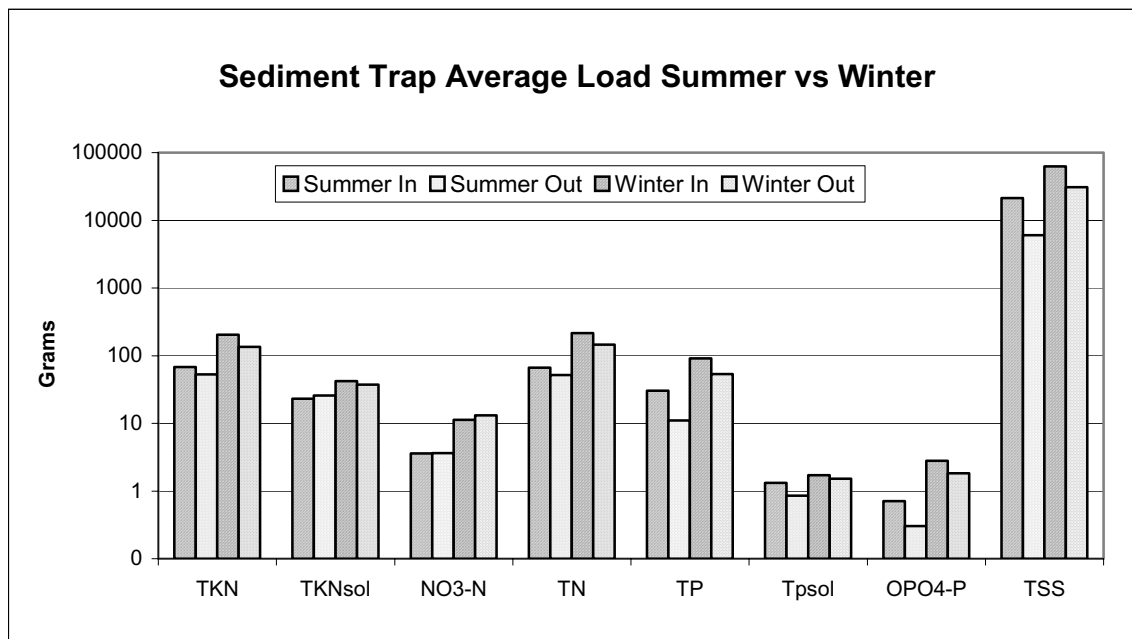


Figure 8.1. Average Nutrient Load per Storm to Sediment Trap (NDOT 2).

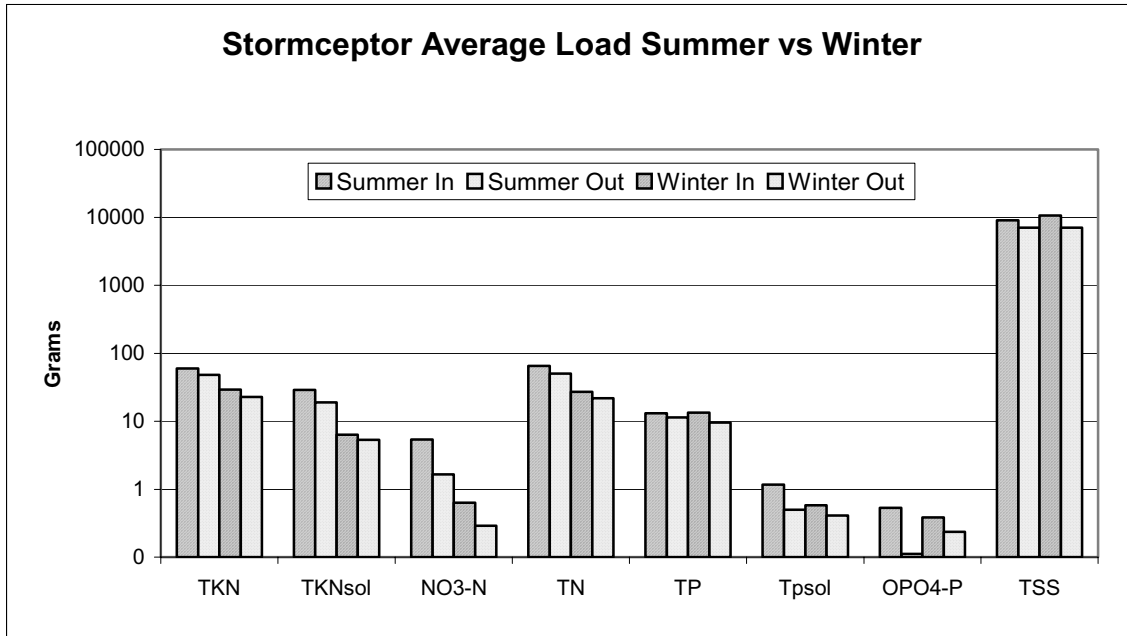


Figure 8.2. Average nutrient load per storm to Stormceptor® (NDOT 4).

Total suspended solids and TP loads to the Stormceptor® were higher for winter storms. This may be due to the fact there are no roadway cut slopes adjacent to this site; therefore, sediment reaching the Stormceptor® would be mostly from winter maintenance activities. The sediment trap site is adjacent to a large cut slope and receives sediment from storm runoff for both summer and winter storm events.

Summer convective thunderstorms occurred during the months of June through August 2003. At each site, winter snowstorms typically produced the most runoff flowing through each BMP and therefore the greatest loading. However, nutrient loading did not appear to depend on the type of storm, e.g., winter or summer storms, during 2003. For example, at NDOT 2, the maximum nutrient loading occurred during the March 2003 storm for TSS, TP, and TN, with summer thunderstorms in June and July 2003 contributing approximately the same loading (see Figures 8.3 through 8.7). Total loading for orthophosphate (OPO<sub>4</sub>) and nitrate (NO<sub>3</sub>) were higher during the summer convective storms of June and July. Loading rates were much greater during the winter of 2004 due to higher flows. Markers shown in red indicate a net export of nutrient during given storm event.

Field personnel reported the sediment trap was nearly full on April 10, 2003. Maintenance crews were unable to clean this site until August 26, 2003. It is reasonable to assume lack of maintenance affected overall BMP performance.



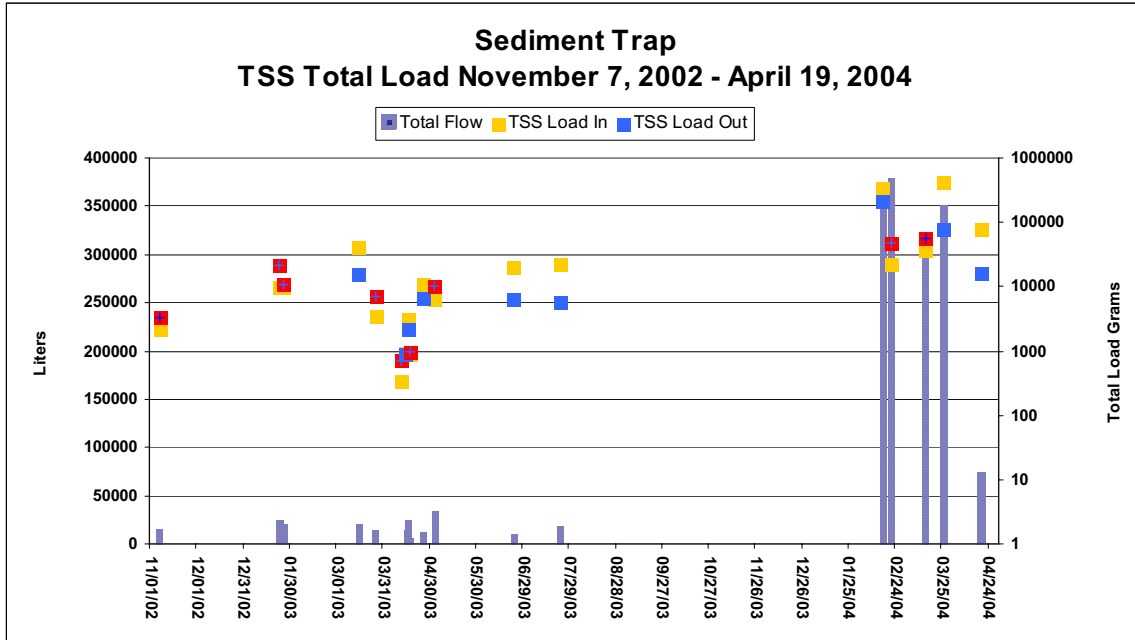


Figure 8.3. TSS loading to sediment trap (NDOT 2).

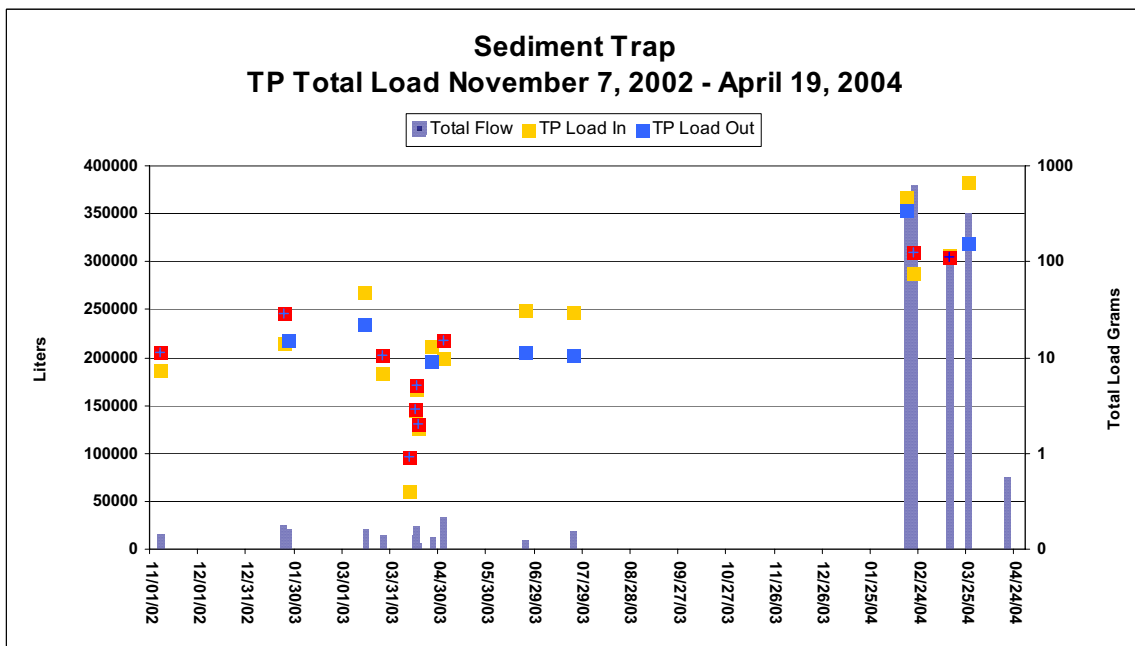


Figure 8.4. TP loading to sediment trap (NDOT 2).

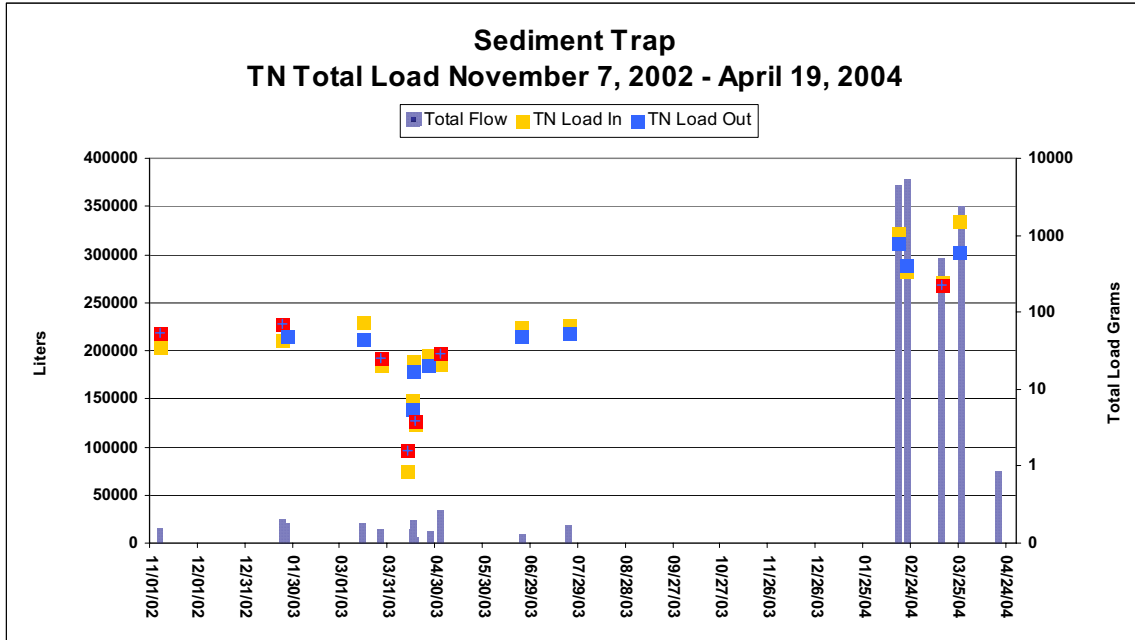


Figure 8.5. TN loading to sediment trap (NDOT 2).

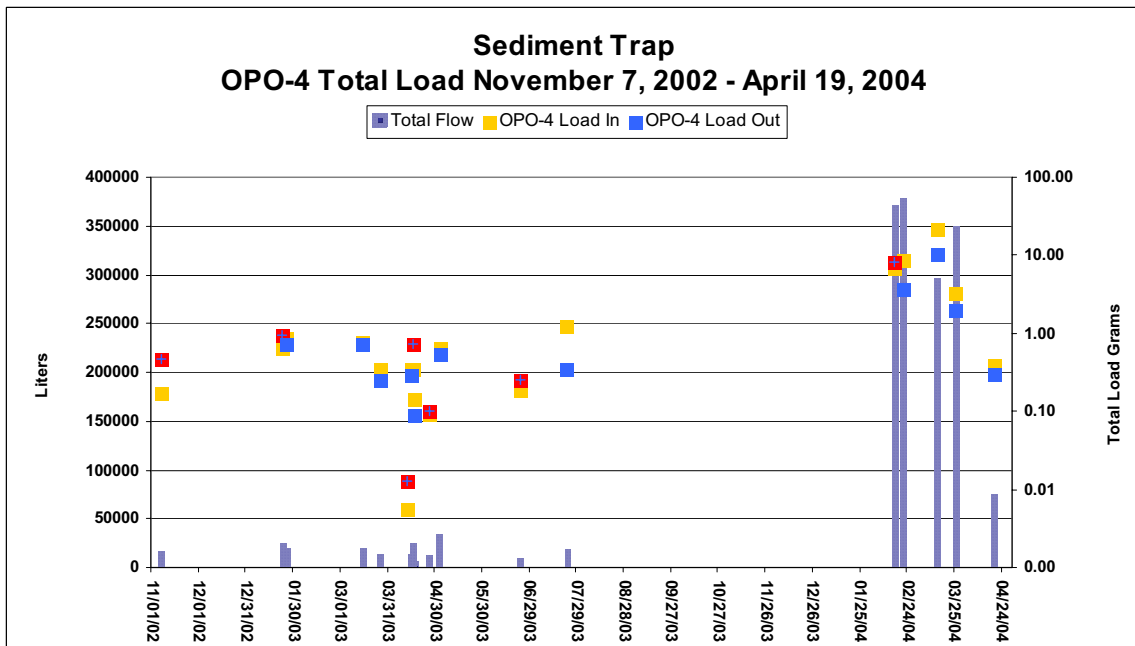


Figure 8.6. OPO<sub>4</sub> loading to sediment trap (NDOT 2).

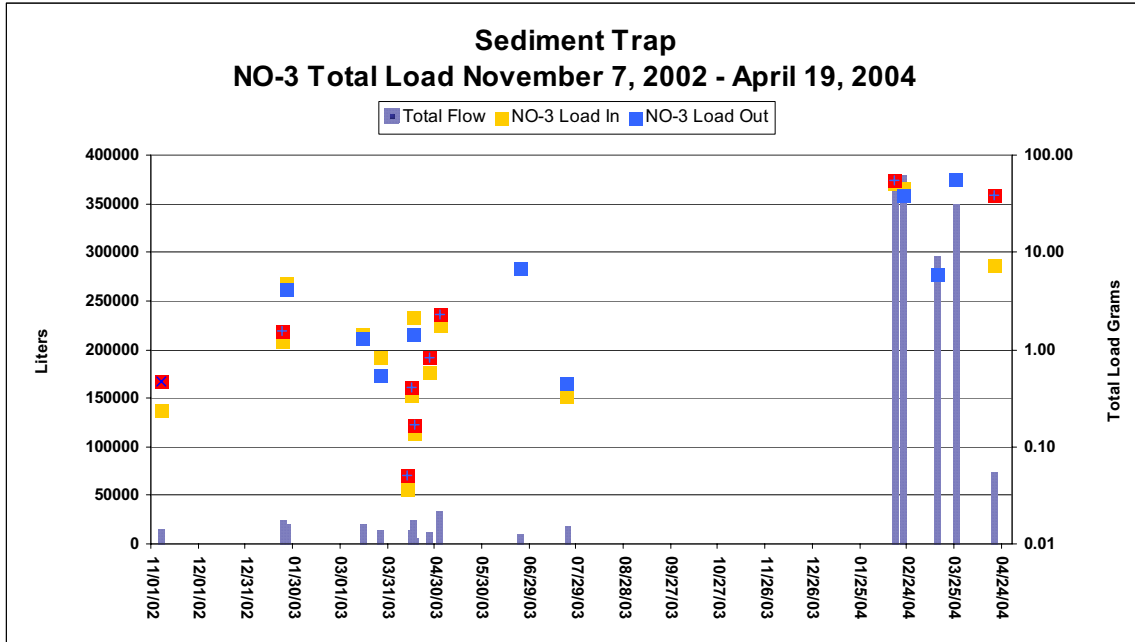


Figure 8.7. NO<sub>3</sub> loading to sediment trap (NDOT 2).

The NDOT 4 site followed a similar pattern with the exception of the greatest total load to the site for TSS, TP and TN was during the January 2003 storm. Orthophosphate and NO<sub>3</sub> loading was highest during summer thunderstorms (Figures 8.8 through 8.12).

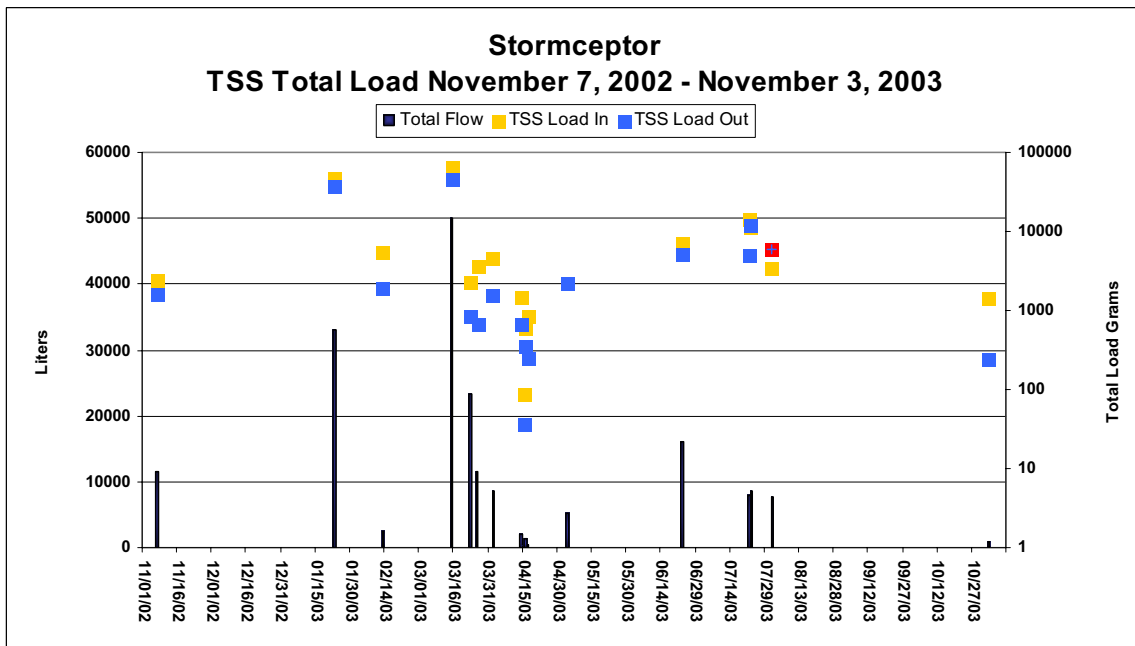


Figure 8.8. TSS loading to Stormceptor® (NDOT 4).

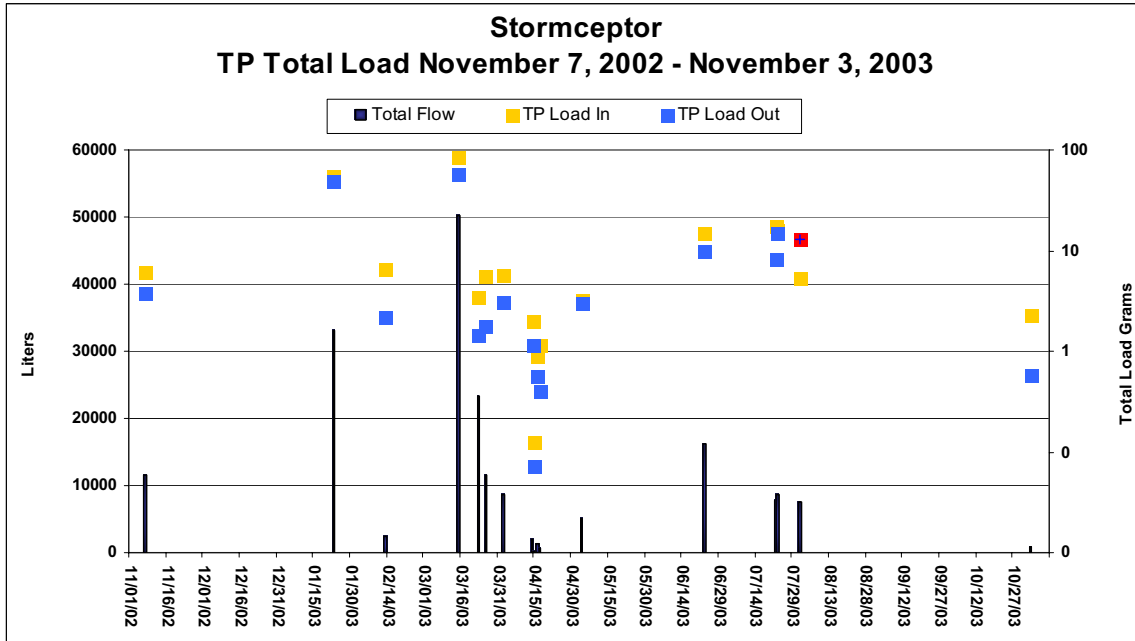


Figure 8.9. TP loading to Stormceptor® (NDOT 4).

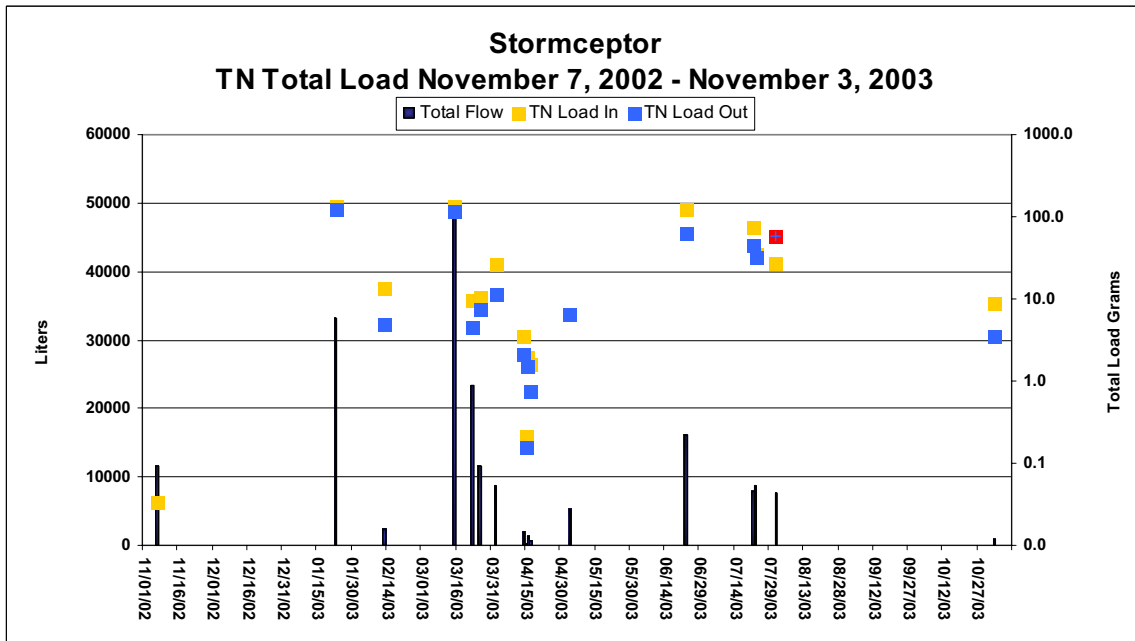


Figure 8.10. TN loading to Stormceptor® (NDOT 4).

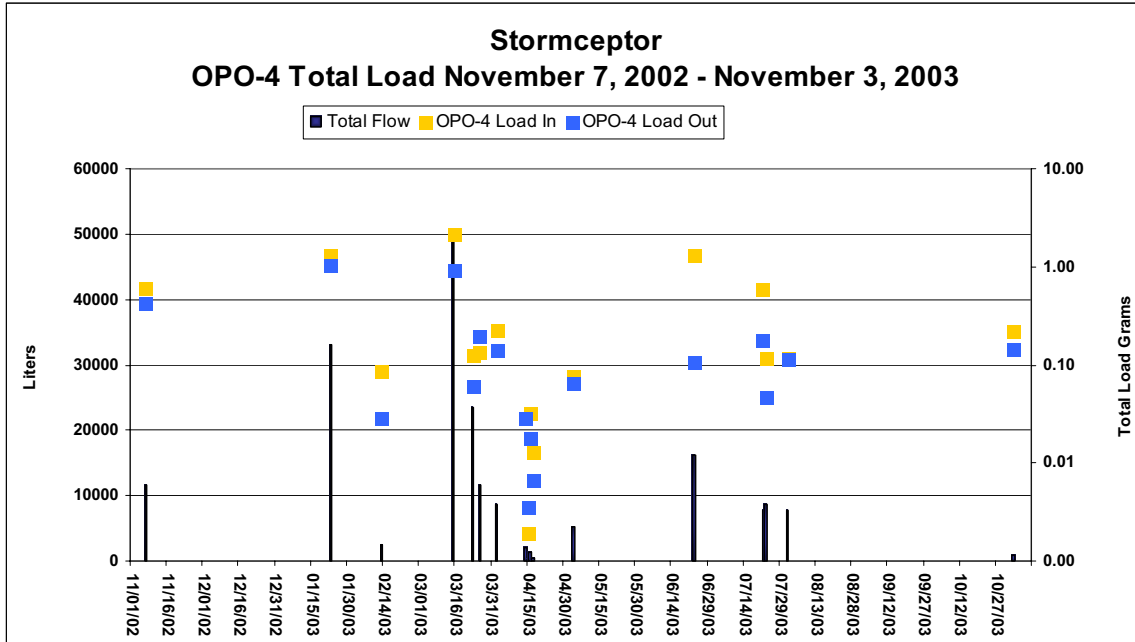


Figure 8.11. OPO<sub>4</sub> loading to Stormceptor® (NDOT 4).

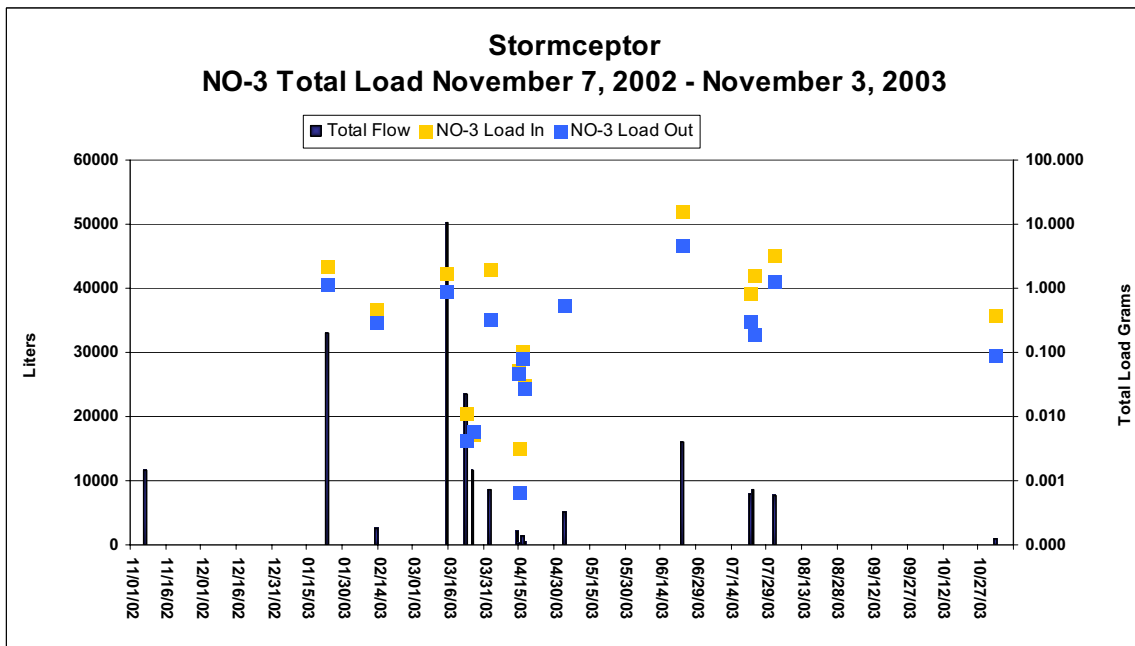


Figure 8.12. NO<sub>3</sub> loading to Stormceptor® (NDOT 4).

Comparisons between NDOT 2 and NDOT 4 yielded both expected and unexpected results. Table 8.1 lists overall efficiencies calculated as the percent of total pollutant removal using the total nutrient load, in grams, entering each BMP. Total nutrient loads for the monitoring period are listed in Table 8.2. Most surprising was the lack of statistical

significance between inflows and outflows to the sediment trap. Another unexpected result was the apparent removal of dissolved nutrients by the Stormceptor®. A possible mechanism for this reduction may be through bacterial activities with captured road oils serving as the carbon source. However, further investigation is needed to determine if this apparent reduction is real.

Table 8.1. Removal efficiencies for the three BMP structure types from November 2002 through April 2004.

NDOT BMP	Overall BMP Performance							
	TKN	TKN <sub>sol</sub>	NO <sub>3</sub> -N	TN	TP	TP <sub>sol</sub>	OPO <sub>4</sub> -P	TSS
Sediment Trap % Removal	33	10	-15	32	42	14	35	51
Sediment Trap P-values	0.123	0.118	0.200	0.116	0.123	0.222	0.097	0.082
Sediment Basin	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Stormceptor % Removal	21	27	65	21	25	40	51	31
Stormceptor P-values	0.039	0.091	0.048	0.050	0.031	0.026	0.020	0.016

Table 8.2. Total loading entering and exiting for the three BMPs from November 2002 through April 2004.

BMP TYPE (NDOT Site)	Total Nutrient Load In and Out (grams)							
	TKN	TKN <sub>sol</sub>	NO <sub>3</sub> -N	TN	TP	TP <sub>sol</sub>	OPO <sub>4</sub> -P	TSS (kg)
	In Out	In Out	In Out	In Out	In Out	In Out	In Out	In Out
Sediment Trap (NDOT2)	3,395 2,264	722 647	188 216	3,590 2,432	1,526 880	25 22	46 30	1,043.6 507.1
Sediment Basin (NDOT3)	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Stormceptor (NDOT4)	618 490	199 146	29 10	613 483	227 170	12 7	7 3	173.6 119.7

### NDOT 2 – Sediment Trap

Monitoring data for NDOT 2 were collected for 18 storms from November 07, 2002 through May 19, 2004. A total of 1,655,985 liters (437,465 gallons) was treated through this site. Two summer thunderstorms produced 23,657 liters (6,250 gallons) of runoff. Twelve winter storms contributed a total of 1,632,328 liters (431,215 gallons) or 98 percent of the total roadway runoff for the monitoring period.

NDOT 2 was the only structure to show a net export of nutrients and was the least effective of the three types of structures. Although, the differences in percent effectiveness for TSS and TP were similar to those of NDOT 4, p-values indicate no significant difference between influent pollutants and effluent pollutants. A possible explanation is the need for maintenance at this site. Although NDOT 2 did show a moderate removal of TP and TSS with total removal of 51 percent and 42 percent, respectively, these values can essentially be attributed to three storms, on March 15, 2003, June 23, 2003, and July 23, 2003 (Figures 8.13

through 8.17, Table 8.3). The NDOT 2 site removed 35 percent of the orthophosphate and had a negative treatment effect on removing nitrate entering this system.

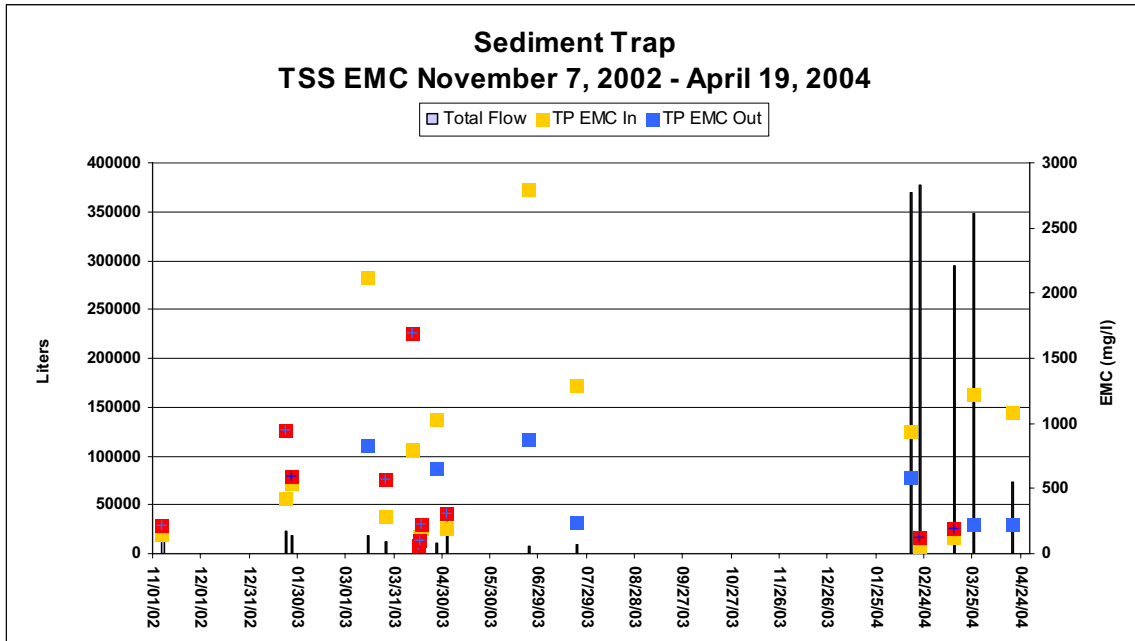


Figure 8.13. TSS EMC value for sediment trap.

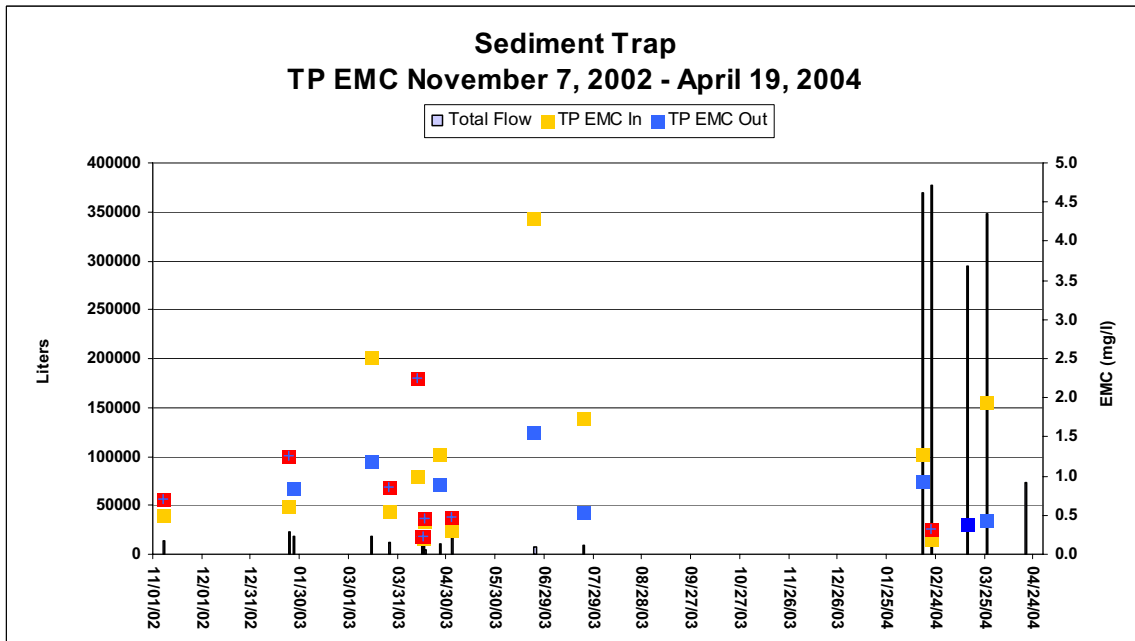


Figure 8.14. TP EMC value for sediment trap.

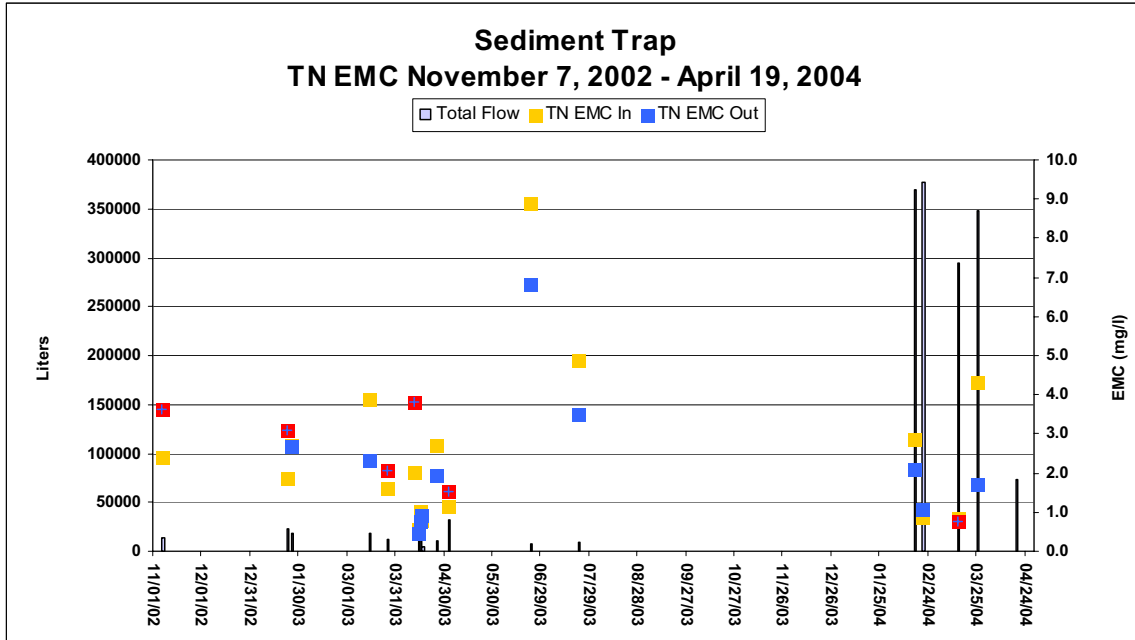


Figure 8.15. TN EMC value for sediment trap.

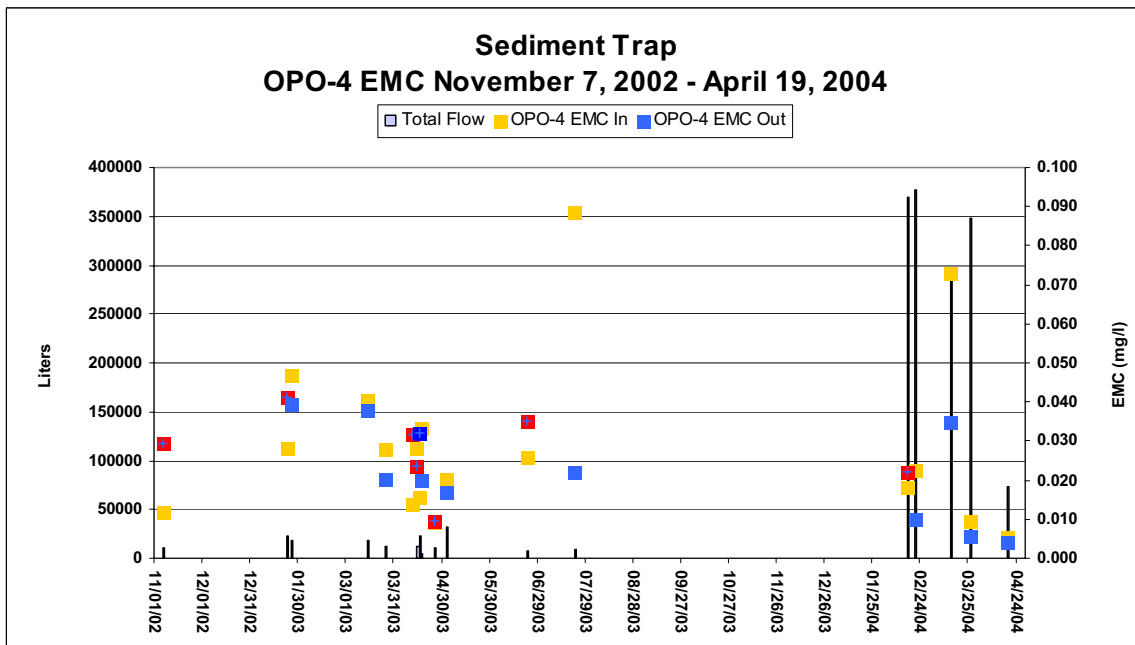


Figure 8.16. OPO<sub>4</sub> EMC value for sediment trap.



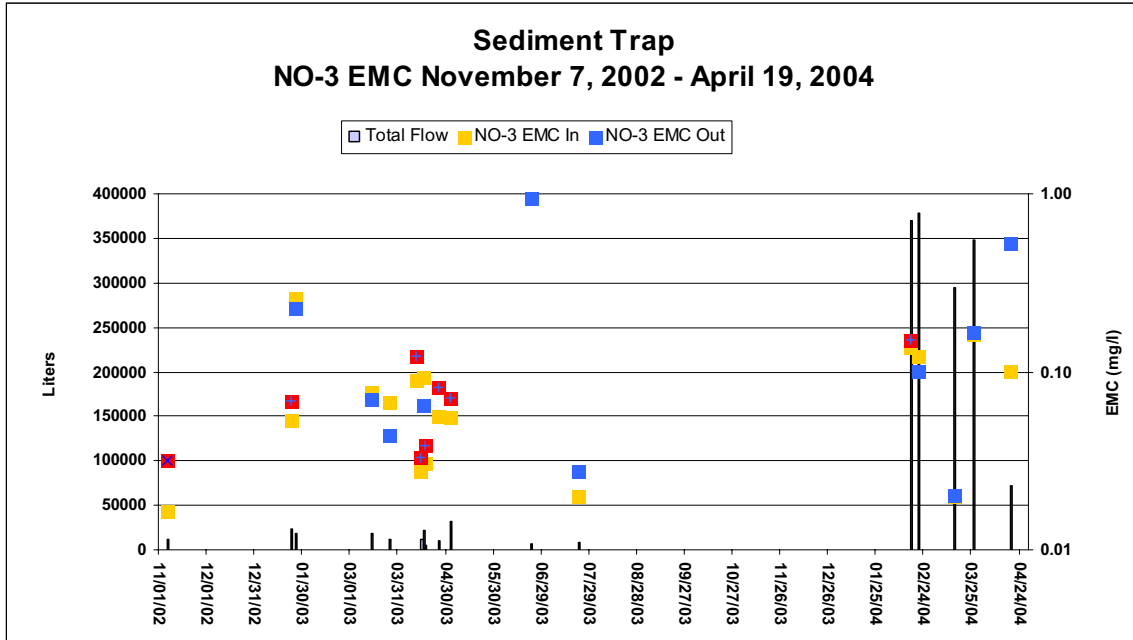


Figure 8.17. NO<sub>3</sub> EMC value for sediment trap.

Net export of all nutrients (markers shown in red) occurred during storms sampled starting on November 7, and ending November 10, 2002 and April 12, 2003. A possible explanation may be that the sediment trap was at capacity and treatment opportunities were not available. Seven out of the 13 storms sampled had a net export of TSS. Total nitrogen was greater in the outflow than in the inflow during six storm events. Total phosphorous was exported during eight storm events. Data show that net export of at least one nutrient occurred during every storm event.

Field observations indicated the sediment trap was at capacity and in need of maintenance by early April. It is important to note that this structure was cleaned, for the first time, on August 26, 2003 and again on November 14, 2003. This is a plausible explanation for the better performance during the 2004 storms and demonstrates the importance of regular BMP structure maintenance to ensure proper functioning of the structure. As described in Chapter 4, the sediment trap consists of three 36 inch corrugated metal pipes placed vertically in the ground with a grate on top. Each vertical can is connected by an 18 inch cross pipe to allow deposition of sediment as flow is conveyed through the three pipes. With no bypass feature, it would be expected that re-suspension of sediment would occur. Data analyses shows that the sediment trap is ineffective in capturing fine-grained sediments. Demonstration of effectiveness in capturing coarse-grained sediments has been shown as all three chambers filled and required maintenance within six months of installation.

Table 8.3. Removal efficiency of storm runoff at sediment trap site.

<b>Inflow</b>			Total Load grams							
Event No.	Date	Total Volume Runoff (l)	TKN	TKNsol	NO <sub>3</sub> -N	TN	TP	Tpsol	OPO <sub>4</sub> -P	TSS
1	11/07/02	14,524	35	12	0.2	35	7	1	0.2	2,116
2	01/23/03	22,741	41	9	1.2	43	14	1	0.6	9,531
3	01/26/03	18,240	45	11	4.8	50	15	1	0.9	9,719
4	03/15/03	19,019	73	7	1.5	74	48	1	0.8	40,299
5	03/26/03	12,328	19	5	0.8	20	7	1	0.3	3,557
6	04/12/03	409	1	0	0.0	1	0	0	0.0	326
7	04/15/03	12,470	7	2	0.3	7	3	0	0.4	927
8	04/16/03	22,398	21	11	2.1	23	5	1	0.3	3,136
9	04/17/03	4,394	3	1	0.1	4	2	0	0.1	856
10	04/26/03	10,207	27	6	0.6	28	13	0	0.1	10,550
11	05/03/03	31,897	20	7	1.8	22	10	1	0.6	6,168
12	06/23/03	7,266	58	19	6.8	65	31	1	0.2	20,340
13	07/23/03	16,391	78	27	0.3	69	30	2	1.2	22,304
14	02/16/04	370,196	1,016	151	51	1,067	473	6	7	347,381
15	02/21/04	377,450	266	154	46	337	76	10	9	23,044
16	03/14/04	294,857	239	41	6	245	114	--	21	37,009
17	03/26/04	348,462	1,446	260	57	1503	678	--	3	427,533
18	04/19/04	72,736	0	0	7	0	0	0	0	78,793
<b>Total Load</b>		<b>1,655,985</b>	<b>3,395</b>	<b>722</b>	<b>188</b>	<b>3,590</b>	<b>1,526</b>	<b>25</b>	<b>46</b>	<b>1,043,590</b>
<b>Outflow</b>										
Event No.	Date	Total Volume Runoff (l)	TKN	TKNsol	NO <sub>3</sub> -N	TN	TP	Tpsol	OPO <sub>4</sub> -P	TSS
1	11/07/02	14,524	54	21	0.5	55	11	1	0.5	3,351
2	01/23/03	22,741	69	9	1.6	70	29	1	0.9	21,502
3	01/26/03	18,240	44	11	4.2	49	15	1	0.7	10,830
4	03/15/03	19,019	43	8	1.3	45	22	1	0.7	15,947
5	03/26/03	12,328	25	5	0.5	25	11	1	0.2	7,013
6	04/12/03	409	2	0	0.1	2	1	0	0.0	694
7	04/15/03	12,470	5	2	0.4	6	3	0	0.3	881
8	04/16/03	22,398	16	10	1.5	17	5	1	0.7	2,225
9	04/17/03	4,394	4	1	0.2	4	2	0	0.1	988
10	04/26/03	10,207	19	6	0.8	20	9	0	0.1	6,680
11	05/03/03	31,897	27	8	2.3	28	15	1	0.5	9,916
12	06/23/03	7,266	43	20	6.8	50	11	1	0.3	6,443
13	07/23/03	16,391	63	32	0.5	54	11	1	0.4	5,654
14	02/16/04	370,196	720	134	56	775	345	6	8	217,416
15	02/21/04	377,450	369	143	38	407	123	6	4	46,742
16	03/14/04	294,857	216	35	6	222	112	--	10	55,722
17	03/26/04	348,462	546	203	58	604	154	--	2	78,568
18	04/19/04	72,736	0	0	38	0	0	0	0	16,487
<b>Total Load</b>		<b>1,655,985</b>	<b>2,264</b>	<b>647</b>	<b>216</b>	<b>2,432</b>	<b>880</b>	<b>22</b>	<b>30</b>	<b>507,059</b>

### NDOT 3 - Sediment Basin

Monitoring data for the NODT 3 site were collected for eight storms from November 11, 2002 through August 21, 2003. A total of 79,125 gallons was treated through this site. Two summer thunderstorms produced 47,675 gallons of runoff. Four winter storms contributed a total of 37,450 gallons or 44 percent of the total roadway runoff for the monitoring period.

Presumably, the NDOT 3 BMP structure was the most effective in removing nutrients from surface stormwater runoff. This is largely due to the volume of water that is stored within the basin. The basin design volume is 413 cubic feet. While suspended sediment typically remains trapped within the basin, much of the dissolved nutrients are infiltrated through the bottom of the structure. Monitoring effects of stormwater infiltration for nutrient removal and potential resulting effects on groundwater below this site was not part of this study.

Chemistry data were collected at this site for a total of eight storms. During storms where outflow was present, there were exports of nutrients on two occasions (Figures 8.18 and 8.19). Nutrient export occurred during the July 18, 2002 storm for total soluble phosphorus and orthophosphate and on August 2, 2003 for TKNsol, nitrate, total soluble phosphorus and orthophosphate. Concentration data indicate a reduction of TSS exiting the basin from that entering the basin (Figure 8.20). Accurate loading calculations could not be made for this data set. The total amount of stormwater runoff entering the basin far exceeded flows exiting the basin. However, repairs were made in August 2003.

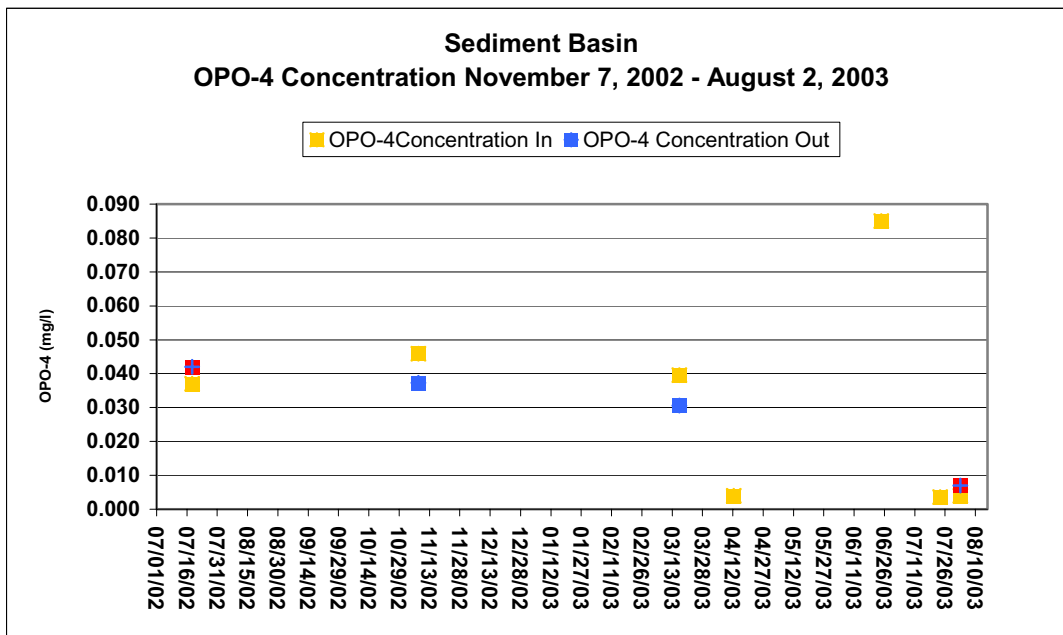


Figure 8.18. OPO<sub>4</sub> concentrations at NDOT 3.

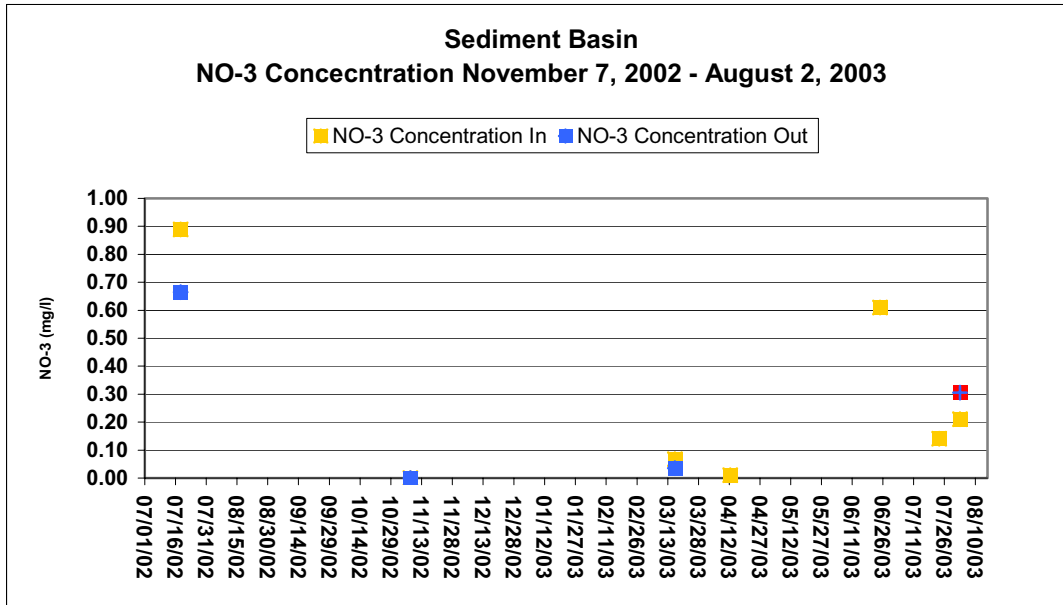


Figure 8.19. NO<sub>3</sub> concentrations at NDOT 3.

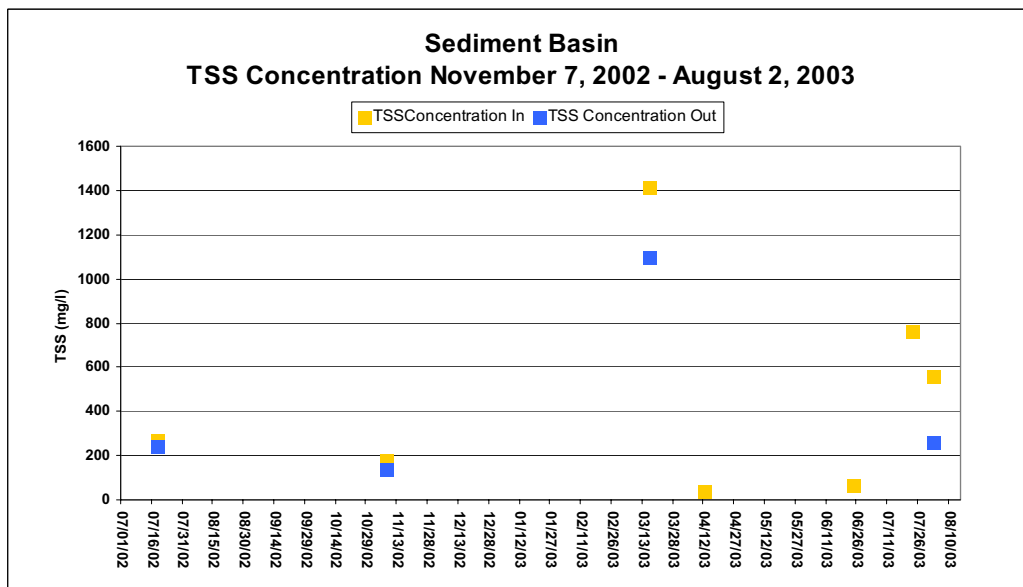


Figure 8.20. TSS concentrations at NDOT 3.

Flow and chemistry data were available for total loading calculations for storms on November 7, 2002 and March 15, 2003. However, accurate estimation of outflow cannot be determined at this time, because of discharge of flows over the side berm. A number of problems prevented complete data analyses for other storm events. Originally, the automated samplers were triggered by outflow. Thus, since it was rare that storm events at the sediment basin produced runoff volumes greater than the basin capacity, inflow rates and samples were not collected for numerous storms. The samplers were reset to collect inflow samples in

summer 2003. Flow data were not recorded for the July 18, 2002, August 2, 2003, and August 23, 2003 runoff events due to faulty depth sensors. Flow data and inflow chemistry data were collected for the July 22, 2003 convective storm, however, comparisons could not be made, as the outflow samplers failed to collect chemistry data. There were insufficient samples for analyses of TKN, TP and TSS for the December 2003 storm.

#### **NDOT 4 - Stormceptor®**

Monitoring data for NDOT 4 were collected for 18 storms from November 11, 2002 through August 1, 2003. A total of 191,412 liters (50,566 gallons) was treated through this site. Summer thunderstorms produced 40,239 liters (10,630) gallons of runoff. Thirteen winter storms contributed a total of 151,173 liters (39,935 gallons) or 79 percent of the total roadway runoff for the monitoring period.

Total nutrient removal at the NDOT 4 site was not as effective as the NDOT 3 site but the site performed better overall than NDOT 2. As with NDOT 2, NDOT 4 also showed net exports of nutrients but to a lesser extent. Nine out of 18 storm events had a net export of at least one nutrient. However, seven storm events showed a reduction in outflow loading for all nutrients. This is in stark contrast to NDOT 2, which yielded a net export of at least one nutrient at every storm event. At NDOT 4, efficiency in removing TSS, TP and TN for all the storms sampled was 31 percent, 25 percent and 21 percent, respectively. Noteworthy is that NDOT 2 had a net export of TSS for 9 out of the 18 storms, whereas NDOT 4 had a net export in only three out of 17 storms. Although the apparent overall percent effectiveness is similar between NDOT 2 and NDOT 4, the treatment effectiveness of the sediment trap is statistically insignificant as indicated in Table 8.3.

Stormceptor® product literature claims up to 80 percent removal of TSS. Several studies (USGS, 1999; Yu *et al.*, 2001) have reported TSS removals of 25 percent to 57 percent. Total suspended solids removal of 31 percent in this study is within range of other published studies but far lower than product literature. Residence time in the Stormceptor® vault, at most only minutes, is dependent on the flow rate of stormwater entering the vault and on storage volume at the time of the storm.

What is surprising and unreported to date, is the apparent removal of dissolved nutrients such as NO<sub>3</sub>-N, soluble TP and OPO<sub>4</sub> at 65 percent, 40 percent and 51 percent, respectively. Possible mechanisms for nutrient removal may be additional settling with suspended sediment and/or bacterial transformations of N and P in which oil captured from roadway runoff would serve as the carbon source. Overall, NDOT 4 has superior performance in removing all nutrients sampled.

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## CHAPTER 9. CONCLUSIONS

Of the three types of BMPs tested for this study, the sediment basin (NDOT 3 site) is assumed to be the most effective in removing overall total nutrients from surface water flows. Again, total loading could not be accurately calculated for this monitoring period. However, over the course of the monitoring period, more stormwater entered, was stored, and infiltrated than what exited through this basin. Numerous small storms, not recorded, as well as melt from snow removal piles were treated at this site through infiltration. At NDOT 4, the Stormceptor® was the better flow-through treatment structure when compared to the sediment trap (Table 8.1). Table 9.1 lists overall cost for pollutant removal for each structure.

Table 9.1. Cost per percent pollutant removed per acre per year (includes annual maintenance).

BMP TYPE (NDOT Site)	Pollutant							
	TKN	TKN <sub>sol</sub>	NO <sub>3</sub> -N	TN	TP	TP <sub>sol</sub>	OPO <sub>4</sub> -P	TSS
Sediment Trap	\$80	\$259	\$(178)	\$83	\$63	\$197	\$75	\$52
Sediment Basin	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
Stormceptor®	\$369	\$285	\$117	\$360	\$301	\$190	\$151	\$247

Plainly evident is the high cost for removal of pollutants from stormwater runoff. Stormceptor®, at first glance, appears to be the least cost effective. However, as previously shown, treatment through the sediment trap is not statically significant. Design modifications to the sediment trap along with regular maintenance should improve overall efficiency and may substantiate the lower costs indicated in Table 9.1.

Unexpectedly, the Stormceptor® was effective in removing all nutrients. Especially surprising was the removal of the dissolved nutrients from stormwater passing through the Stormceptor®. Reductions may be attributed to settling of suspended sediments or in various bacterial reactions. However, on several occasions a net export of nutrients did occur. Similar performance ranges are expected of other sand/oil separator products currently on the market. Keeping with the intent of the NDOT Master Plan, sand/oil separator installation, including but not limited to the Stormceptor® brand, where stormwater runoff would discharge into stream environment zones and in areas with high volumes of traffic such as beach parking areas, is recommended.

Least effective of the three types of highway BMPs was the sediment trap (NDOT 2 site). Stormwater runoff through the sediment trap actually contributed additional NO<sub>3</sub>-N to stormwater discharges during this study. Although TSS and TP removal was relatively similar to that of Stormceptor®, this efficiency can be contributed to only 50% of the storms. Net export of nutrients occurred during the majority of storms. Timely maintenance may have increased the performance level of this sediment trap. As previously stated, maintenance was needed in April 2003 but did not occur until August 2003.

Sediment traps are typically placed at the terminus of steep cut slopes where installation of riprap and revegetation treatment is not practical. Sediment traps have shown to be effective in capturing coarse grain sediment along with suspended sediment and associated TP, and use should continue at suitable locations.

The Nevada Department of Transportation is considering revising its strategy for treatment control. Presently, the Master Plan incorporates an approach of collecting and treating roadway runoff based upon early direction in the 1990s from TRPA (Amir Soltani, personal communication, 2003). Unintended consequences have arisen from collecting and concentrating storm flows. At issue is the erosion caused by stormwater concentrated and discharged at a single point. Typically, discharge occurs atop tall, steep hillsides along the majority of NDOT's roads in the Tahoe basin. This concentrated flow discharges into riprap channels that occasionally fail due to the steep slopes and erosive soils (Figure 9.1).



Figure 9.1. Riprap channel terminus on steep hillside below SR 28.

Additionally, the discharge of water collected and treated either through a series of drop inlets with additional sediment capacity, routed through sediment traps, sediment basins, or water quality vaults, and then discharged back onto bare ground, should be evaluated. Because of these issues, NDOT is considering alternatives to collect-and-treat methods, including various source control and flow dispersion methods where feasible. New techniques using bioengineering are also being investigated.

Mitigation measures, as recommended by Dorman *et al.* (1996) are not typically suitable for use in the Tahoe basin. Vegetative controls such as grass-lined channels and overland flow areas are the most common BMPs for treating highway stormwater runoff (Dorman *et al.*, 1996). Their flexibility, effectiveness, adaptability, and low cost lend to their extensive use. However, vegetative control systems are not a viable option for NDOT



roadways within the Tahoe basin, where the majority of roadway runoff is from winter precipitation in the form of snow. Slopes are typically very steep, with the average slope 2:1 (H:V) or steeper, and the average vegetative cover along the east shore of Lake Tahoe less than 60 percent (Harding Lawson Associates, 1998).

Numerous ultra-urban stormwater runoff treatment systems on the market are currently being evaluated for effectiveness. Some limitations of these systems are as follows. The large footprint associated with volume-based water quality vaults increases the likelihood of utility conflicts, increasing installation costs significantly. Consideration of annual maintenance costs and maintenance safety issues such as enclosed space hazards may lessen acceptability. Additionally, adequate treatment of highway runoff flows must be considered when considering flow-based systems. Suitability of outfall locations is also an important consideration, as previously noted.

Finally erosion caused by concentrated flow, the result of the collect-and-treat strategy, must be addressed. Managing stormwater runoff is an adaptive process, and lessons learned from this monitoring study will be applied as NDOT moves forward with completing the erosion control improvements to its roadways throughout Nevada. Methods for treating highway runoff are site specific and require input from federal, state and local agencies as well as local general improvement districts, homeowners associations, and private landowners. Stakeholder involvement will continue to be an integral part of NDOT's Lake Tahoe EIP program.

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## **APPENDIX A. NDOT 2 DATA**









SR 28 at Secret Harbor Creek March 26, 2003 Loading  
Sediment Trap Inflow

Lab #	Sample Name	Sample Time	TKN mg/l	TKNsol mg/l	NO3 mg/l	TP mg/l	TPsol mg/l	OPO4 mg/l	TSS mg/l	Average Concentration	Value Used for flow volumes without concentrations	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS	
											Interval Liters									
											Time									
	Average		1.54	0.40	0.07	0.54	0.053	0.028	280.33	3/26/03 8:00	0	0	0	0	0	0	0	0	0	0
	Average		1.54	0.40	0.07	0.54	0.053	0.028	280.33	3/26/03 8:30	1751	2703	695	119	2822	952	93	49	490948	
	Average		1.54	0.40	0.07	0.54	0.053	0.028	280.33	3/26/03 9:00	1740	2685	690	118	2804	946	93	49	487747	
56032	NDOT 2A-4	3/26/03 9:16	1.21	0.35	0.01	0.46	0.036	0.019	281.00	3/26/03 9:16	1879	2273	658	24	2298	857	68	36	527944	
	Average		1.54	0.40	0.07	0.54	0.053	0.028	280.33	3/26/03 10:00	2030	3133	805	138	3271	1104	108	57	569144	
56033	NDOT 2A-5	3/26/03 10:21	1.91	0.37	0.10	0.72	0.060	0.035	384.00	3/26/03 10:21	2048	3912	758	205	4117	1464	123	72	786437	
	Average		1.54	0.40	0.07	0.54	0.053	0.028	280.33	3/26/03 11:00	1600	2470	635	109	2579	870	85	45	448627	
56034	NDOT 2A-6	3/26/03 11:26	1.51	0.47	0.09	0.46	0.064	0.030	176.00	3/26/03 11:26	1079	1629	507	98	1728	496	69	32	189922	
	Average		1.54	0.40	0.07	0.54	0.053	0.028	280.33	3/26/03 12:00	200	309	79	14	322	109	11	6	56043	
	Average		1.54	0.40	0.07	0.54	0.053	0.028	280.33	3/26/03 12:30	0	0	0	0	0	0	0	0	0	
Total											12328	19114	4827	825	19940	6798	650	345	3556813	
EMC In											1.55	0.39	0.07	1.62	0.55	0.053	0.028	286.52		

Sediment Trap Outflow

Lab #	Sample Name	Sample Time	TKN mg/l	TKNsol mg/l	NO3 mg/l	TP mg/l	TPsol mg/l	OPO4 mg/l	TSS mg/l	Average Concentration	Value Used for flow volumes without concentrations	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS	
											Interval Liters									
											Time									
	Average		1.99	0.40	0.05	0.84	0.043	0.021	558.67	3/26/03 8:00	0	0	0	0	0	0	0	0	0	
	Average		1.99	0.40	0.05	0.84	0.043	0.021	558.67	3/26/03 8:30	1751	3491	701	79	3570	1470	75	36	978394	
	Average		1.99	0.40	0.05	0.84	0.043	0.021	558.67	3/26/03 9:00	1740	3468	696	79	3547	1460	74	36	972014	
56035	NDOT 2B-4	3/26/03 9:16	2.73	0.39	0.03	1.24	0.030	0.012	884.00	3/26/03 9:16	1879	5129	733	56	5186	2330	56	23	1660864	
	Average		1.99	0.40	0.05	0.84	0.043	0.021	558.67	3/26/03 10:00	2030	4047	812	92	4139	1704	87	42	1134228	
56036	NDOT 2B-5	3/26/03 10:21	1.61	0.37	0.04	0.68	0.045	0.022	420.00	3/26/03 10:21	2048	3297	758	76	3373	1391	92	45	860165	
	Average		1.99	0.40	0.05	0.84	0.043	0.021	558.67	3/26/03 11:00	1600	3190	640	73	3263	1343	68	33	894053	
56037	NDOT 2B-6	3/26/03 11:26	1.64	0.44	0.07	0.60	0.053	0.028	372.00	3/26/03 11:26	1079	1770	475	74	1844	646	57	30	401427	
	Average		1.99	0.40	0.05	0.84	0.043	0.021	558.67	3/26/03 12:00	200	398	80	9	408	168	9	4	111686	
	Average		1.99	0.40	0.05	0.84	0.043	0.021	558.67	3/26/03 12:30	0	0	0	0	0	0	0	0	0	
Total											12328	24791	4894	539	25329	10512	518	249	7012831	
EMC Out											2.01	0.40	0.04	2.05	0.85	0.042	0.020	568.87		

SR 28 at Secret Harbor Creek April 12, 2003 Loading

Sediment Trap Inflow

Lab #	Sample Name	Sample Time	Total Load (In) milligrams																				
			TKN	TKNsol	NO3-N	TN	TP	Tpsol	OPO4-P	TSS	Average Concentration	Value Used for flow volumes without concentrations	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	Tpsol	OPO4-P	TSS		
56148	NDOT 2A-4	4/12/03 16:41	2.14	0.68	0.09	2.23	1.24	0.029	0.013	1010.00	247	529	168	21	550	306	0	0	0	0	0	0	249449
	Average		1.86	0.75	0.09	1.95	0.88	0.031	0.014	698.00	45	83	33	4	87	39							31182
56149	NDOT 2A-5	4/12/03 17:46	1.58	0.81	0.10	1.68	0.51	0.032	0.015	388.00	31	48	25	3	51	16							11891
	Average		1.58	0.81	0.10	1.68	0.51	0.032	0.015	388.00	24	38	19	2	40	12							9248
	Average		1.58	0.81	0.10	1.68	0.51	0.032	0.015	388.00	19	30	15	2	32	10							7337
	Average		1.58	0.81	0.10	1.68	0.51	0.032	0.015	388.00	42	67	34	4	71	22							16388
	Average		1.58	0.81	0.10	1.68	0.51	0.032	0.015	388.00	2	3	2	0	4	1							859
	Average		1.58	0.81	0.10	1.68	0.51	0.032	0.015	388.00	0	0	0	0	0	0							0
	Total		409	798	297	37	835	406	12	0.99	0.99	2.04	0.09	2.04	0.99	0.030	0.030	0.014	0.014	0.014	0.014	0.014	326355
	EMC In		1.95	0.72	0.09	2.04	0.99	0.99	0.030	0.030	0.030	0.014	0.014	0.014	0.014	0.014							797

Sediment Trap Outflow

Lab #	Sample Name	Sample Time	Total Load (Out) milligrams																				
			TKN	TKNsol	NO3-N	TN	TP	Tpsol	OPO4-P	TSS	Average Concentration	Value Used for flow volumes without concentrations	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	Tpsol	OPO4-P	TSS		
56150	NDOT 2B-4	4/12/03 16:41	4.55	1.36	0.14	4.69	2.85	0.057	0.037	2180.00	247	1124	336	35	1158	704							538414
	Average		3.29	1.08	0.12	3.41	1.97	0.050	0.029	1470.00	45	147	48	5	152	88							65576
56151	NDOT 2B-5	4/12/03 17:46	2.03	0.80	0.09	2.12	1.08	0.043	0.021	760.00	31	62	25	3	65	33							23292
	Average		2.03	0.80	0.09	2.12	1.08	0.043	0.021	760.00	24	48	19	2	51	26							18116
	Average		2.03	0.80	0.09	2.12	1.08	0.043	0.021	760.00	19	38	15	2	40	20							14371
	Average		2.03	0.80	0.09	2.12	1.08	0.043	0.021	760.00	42	86	34	4	90	46							32100
	Average		2.03	0.80	0.09	2.12	1.08	0.043	0.021	760.00	2	4	2	0	5	2							1684
	Average		2.03	0.80	0.09	2.12	1.08	0.043	0.021	760.00	0	0	0	0	0	0							0
	Total		409	1510	478	50	1560	919	21	13	693552	3.69	1.17	0.12	3.81	2.24							1694
	EMC Out		1.95	0.72	0.09	2.04	0.99	0.99	0.030	0.030	0.030	0.014	0.014	0.014	0.014	0.014							797

SK 28 at Secret Harbor Creek April 15-17, 2003 Loading

Sediment Trap Inflow table with columns: Lab #, Sample Name, Sample Time, TKN, TN, TP, TSS, TPO4-P, TPO4-P, TSS, Average Concentration Value, Interval, TKN, TN, TP, TPO4-P, TSS. Rows include sample 56212 and 56213.

Sediment Trap Inflow table with columns: Lab #, Sample Name, Sample Time, TKN, TN, TP, TSS, TPO4-P, TPO4-P, TSS, Average Concentration Value, Interval, TKN, TN, TP, TPO4-P, TSS. Rows include sample 56216 and 56217.

Sediment Trap Inflow table with columns: Lab #, Sample Name, Sample Time, TKN, TN, TP, TSS, TPO4-P, TPO4-P, TSS, Average Concentration Value, Interval, TKN, TN, TP, TPO4-P, TSS. Rows include sample 56224 and 56225.

Sediment Trap Outflow table with columns: Time, TKN, TN, TP, TSS, TPO4-P, TPO4-P, TSS, Average Concentration Value, Interval, TKN, TN, TP, TPO4-P, TSS. Rows include sample 56232 and 56233.

Sediment Trap Outflow table with columns: Time, TKN, TN, TP, TSS, TPO4-P, TPO4-P, TSS, Average Concentration Value, Interval, TKN, TN, TP, TPO4-P, TSS. Rows include sample 56236 and 56237.

Sediment Trap Outflow table with columns: Time, TKN, TN, TP, TSS, TPO4-P, TPO4-P, TSS, Average Concentration Value, Interval, TKN, TN, TP, TPO4-P, TSS. Rows include sample 56244 and 56245.

SR 28 at Secret Harbor Creek April 26, 2003 Loading  
Sediment Trap Inflow

Lab #	Sample Name	Sample Time	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS	
	Average	4/26/03 9:30	2.55	0.54	0.06	1.21	0.023	0.009	976.00	4/26/03 9:30	0	0	0	0	0	0	0	0	
	Average	4/26/03 10:00	2.55	0.54	0.06	1.21	0.023	0.009	976.00	4/26/03 10:00	24	62	13	1	63	29	1	0	23722
	Average	4/26/03 10:30	2.55	0.54	0.06	1.21	0.023	0.009	976.00	4/26/03 10:30	1581	4023	858	87	4110	1907	36	14	1542848
56381	NDOT 2A-2	4/26/03 10:56	4.22	0.67	0.06	1.90	0.026	0.011	1580.00	4/26/03 10:56	852	3594	571	50	3644	1618	22	9	1345528
	Average	4/26/03 11:30	2.55	0.54	0.06	1.21	0.023	0.009	976.00	4/26/03 11:30	840	2137	456	46	2184	1013	19	8	819652
	Average	4/26/03 12:00	2.55	0.54	0.06	1.21	0.023	0.009	976.00	4/26/03 12:00	1671	4252	906	92	4344	2016	38	15	1630459
56382	NDOT 2A-3	4/26/03 12:01	3.66	0.62	0.07	1.96	0.026	0.011	1580.00	4/26/03 12:01	1651	6044	1024	111	6155	3237	43	18	2609316
	Average	4/26/03 13:00	2.55	0.54	0.06	1.21	0.023	0.009	976.00	4/26/03 13:00	1043	2655	566	58	2713	1259	24	9	1018261
56383	NDOT 2A-4	4/26/03 13:06	1.62	0.46	0.06	0.75	0.020	0.007	588.00	4/26/03 13:06	1061	1719	488	58	1777	793	21	7	623954
	Average	4/26/03 14:00	2.55	0.54	0.06	1.21	0.023	0.009	976.00	4/26/03 14:00	794	2021	431	44	2065	958	18	7	775195
56384	NDOT 2A-5	4/26/03 14:11	0.68	0.42	0.04	0.22	0.020	0.007	156.00	4/26/03 14:11	625	425	262	25	450	137	12	4	97499
	Average	4/26/03 15:00	2.55	0.54	0.06	1.21	0.023	0.009	976.00	4/26/03 15:00	65	165	35	4	169	78	1	1	63291
	Total	4/26/03 15:30								10207	27098	5610	577	27674	13045	237	93	10549725	
	EMC In										2.65	0.55	0.06	2.71	1.28	0.023	0.009	1033.57	

Sediment Trap Outflow

Lab #	Sample Name	Sample Time	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS	
	Average	4/26/03 9:30	1.81	0.54	0.08	0.86	0.025	0.010	624.00	4/26/03 9:30	0	0	0	0	0	0	0	0	
	Average	4/26/03 10:00	1.81	0.54	0.08	0.86	0.025	0.010	624.00	4/26/03 10:00	24	44	13	2	46	21	1	0	15166
	Average	4/26/03 10:30	1.81	0.54	0.08	0.86	0.025	0.010	624.00	4/26/03 10:30	1581	2853	854	127	2981	1355	39	15	986411
56388	NDOT 2B-2	4/26/03 10:56	1.58	0.43	0.10	0.65	0.024	0.008	468.00	4/26/03 10:56	852	1346	366	85	1431	554	20	7	398549
	Average	4/26/03 11:30	1.81	0.54	0.08	0.86	0.025	0.010	624.00	4/26/03 11:30	840	1516	453	68	1583	720	21	8	524040
	Average	4/26/03 12:00	1.81	0.54	0.08	0.86	0.025	0.010	624.00	4/26/03 12:00	1671	3015	902	134	3150	1432	41	16	1042424
56389	NDOT 2B-3	4/26/03 12:01	2.37	0.58	0.09	1.22	0.028	0.011	900.00	4/26/03 12:01	1651	3914	958	144	4058	2015	46	18	1486319
	Average	4/26/03 13:00	1.81	0.54	0.08	0.86	0.025	0.010	624.00	4/26/03 13:00	1043	1883	563	84	1967	894	26	10	651019
56390	NDOT 2B-4	4/26/03 13:06	1.95	0.63	0.07	1.04	0.024	0.012	768.00	4/26/03 13:06	1061	2069	669	77	2147	1104	25	13	814960
	Average	4/26/03 14:00	1.81	0.54	0.08	0.86	0.025	0.010	624.00	4/26/03 14:00	794	1434	429	64	1498	681	19	8	495616
56391	NDOT 2B-5	4/26/03 14:11	1.32	0.52	0.06	0.52	0.022	0.007	360.00	4/26/03 14:11	625	825	325	39	864	324	14	4	224997
	Average	4/26/03 15:00	1.81	0.54	0.08	0.86	0.025	0.010	624.00	4/26/03 15:00	65	117	35	5	122	56	2	1	40465
	Total	4/26/03 15:30								10207	19016	5567	829	19845	9155	253	99	6679968	
	EMC Out										1.86	0.55	0.08	1.94	0.90	0.025	0.010	654.45	





SR 28 at Secret Harbor Creek July 23, 2003 Loading  
Sediment Trap Inflow

Lab #	Sample Name	Sample Times	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TN mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Total Load (IN) Grams		TP	TPsol	OPO4-P	TSS
											Average Concentration	Value Used for flow volumes without concentrations				
		Time	Interval	Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS				
57145	NDOT 2A-2	7/23/03 15:21	4.45	1.35	0.024	4.47	1.80	0.049	0.010	1480	312	1388	0	0	0	0
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	2765	13013	4662	561	15	3
57146	NDOT 2A-3	7/23/03 16:26	4.76	1.10	0.018	4.78	2.71	0.065	0.021	2160	1955	9306	2151	35	9341	215
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	1868	8789	3149	38	7156	251
57147	NDOT 2A-4	7/23/03 17:31	4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	1671	7861	2817	34	6401	130
	Average		5.69	1.74	0.027	5.72	1.69	0.104	0.050	1485	1485	8451	2584	40	8491	74
57148	NDOT 2A-5	7/23/03 18:36	4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	1215	5720	2049	25	4657	163
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	1001	4473	2191	15	4488	197
57149	NDOT 2A-6	7/23/03 19:41	4.16	2.05	0.018	4.18	1.20	0.256	0.179	440	720	2996	1477	13	3009	122
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	602	2834	1015	12	2308	81
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	560	2633	943	11	2144	75
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	435	2046	733	9	1666	58
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	312	1467	525	6	1194	42
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	219	1031	369	4	839	29
	Average		4.71	1.686	0.020	3.83	1.74	0.134	0.078	1297	182	857	307	4	698	24
	Average		4.71	1.69	0.020	4.73	1.74	0.134	0.078	1297	182	855	306	4	859	24
	Total		16391	77985	27232	333	68722	29532	2144	1226	22303706	1360.71				

Sediment Trap Outflow

Lab #	Sample Name	Sample Times	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TN mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Total Load (Out) milligrams		TP	TPsol	OPO4-P	TSS
											Average Concentration	Value Used for flow volumes without concentrations				
		Time	Interval	Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS				
57150	NDOT 2B-2	7/23/03 15:21	5.74	2.24	0.027	5.77	1.44	0.05	0.019	1000	0	699	0	0	0	0
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	10678	5346	76	8097	166	59
57151	NDOT 2B-3	7/23/03 16:26	4.82	2.01	0.028	4.85	0.75	0.06	0.022	456	9424	3930	55	9478	119	43
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	7212	3611	51	5468	112	40
57152	NDOT 2B-4	7/23/03 17:31	3.34	2.16	0.026	3.37	0.52	0.07	0.022	212	6451	3208	46	4891	1130	101
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	4961	3208	39	4999	771	100
57153	NDOT 2B-5	7/23/03 18:36	2.95	1.77	0.029	2.98	0.47	0.07	0.024	172	2952	1771	29	2981	466	69
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	3506	1755	25	2658	614	55
57154	NDOT 2B-6	7/23/03 19:41	3.02	1.62	0.028	3.05	0.45	0.07	0.023	172	2175	1167	20	2195	325	48
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	2326	1164	17	1763	408	36
57155	NDOT 2B-7	7/23/03 20:46	3.30	1.80	0.027	3.33	0.43	0.04	0.017	160	1846	1007	15	1862	242	25
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	1679	841	12	1273	294	26
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	1204	603	9	913	211	19
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	846	423	6	641	148	13
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	704	352	5	533	123	11
	Average		3.86	1.93	0.028	2.93	0.68	0.06	0.021	362	702	351	5	532	123	11
	Total		16391	63149	31808	451	53644	10731	1000	351	5653613	344.92				
	EMC Out		3.85	1.94	0.03	3.27	0.65	0.061	0.021	362	3.85	1.94	0.03	3.27	0.65	0.021











SR 28 at Secret Harbor Creek April 19-20, 2004 Loading  
Sediment Trap Inflow

Lab #	Sample Name	Sample Date	OPO4-P mg/l	NO3-N mg/l	NO2-N mg/l	TSS mg/l	Total Load (In) milligrams		Average Concentration Value Used for flow volumes without concentrations					TSS
							Time	Interval	OPO4-P	NO3-N	NO2-N	TSS		
59928	NDOT 2A-1	4/18/04 22:21	0.009	0.204	0.063	203	4/18/04 22:21	82	1	17	5	16714		
59929	NDOT 2A-2	4/18/04 23:26	0.008	0.234	0.265	10100	4/18/04 23:26	388	3	13	103	3916936		
59930	NDOT 2A-3	4/19/04 0:31	0.004	0.025	0.665	3190	4/19/04 0:31	2401	10	60	1597	7660070		
59931	NDOT 2A-4	4/19/04 1:36	0.008	0.030	1.04	2400	4/19/04 1:36	5663	45	170	5889	13591143		
59932	NDOT 2A-5	4/19/04 2:41	0.007	0.016	0.848	1510	4/19/04 2:41	8682	61	139	7362	13109296		
59933	NDOT 2A-6	4/19/04 3:46	0.005	0.007	1.06	1190	4/19/04 3:46	10576	53	74	11211	125685964		
59934	NDOT 2A-7	4/19/04 4:51	0.006	0.018	0.944	955	4/19/04 4:51	10826	65	195	10220	10339095		
59935	NDOT 2A-8	4/19/04 5:56	0.003	0.020	0.842	883	4/19/04 5:56	6617	20	132	5572	5843057		
59936	NDOT 2A-9	4/19/04 7:01	0.006	0.019	0.764	724	4/19/04 7:01	696	4	13	532	5038666		
59937	NDOT 2A-10	4/19/04 8:06	0.005	0.020	1.01	689	4/19/04 8:06	2015	10	40	2035	1388057		
59938	NDOT 2A-11	4/19/04 9:11	0.005	1.05	0.350	744	4/19/04 9:11	927	5	974	325	689864		
59939	NDOT 2A-12	4/19/04 10:16	0.004	0.530	0.091	1470	4/19/04 10:16	279	1	148	25	410664		
59940	NDOT 2A-13	4/19/04 11:21	0.003	0.358	0.071	1090	4/19/04 11:21	804	2	288	57	875971		
59941	NDOT 2A-14	4/19/04 12:26	0.008	0.316	0.063	706	4/19/04 12:26	1474	12	466	93	1040405		
59942	NDOT 2A-15	4/19/04 13:31	0.002	0.296	0.066	845	4/19/04 13:31	1673	3	495	110	1413654		
59943	NDOT 2A-16	4/19/04 14:36	0.006	0.271	0.074	378	4/19/04 14:36	1893	11	513	140	715514		
59944	NDOT 2A-17	4/19/04 15:41	0.003	0.269	0.070	320	4/19/04 15:41	1406	4	378	98	4495949		
59945	NDOT 2A-18	4/19/04 16:46	0.003	0.209	0.074	294	4/19/04 16:46	666	2	139	49	195817		
59946	NDOT 2A-19	4/19/04 19:36	0.006	0.186	0.078	287	4/19/04 19:36	1372	8	255	107	393825		
59947	NDOT 2A-20	4/19/04 20:41	0.008	0.179	0.073	267	4/19/04 20:41	3316	27	594	242	885428		
59948	NDOT 2A-21	4/19/04 21:46	0.004	0.207	0.068	267	4/19/04 21:46	3765	15	779	256	1005146		
59949	NDOT 2A-22	4/19/04 22:51	0.003	0.210	0.067	242	4/19/04 22:51	3473	10	729	233	840448		
59950	NDOT 2A-23	4/19/04 23:56	0.004	0.208	0.066	255	4/19/04 23:56	2568	10	534	170	654894		
59951	NDOT 2A-24	4/20/04 1:01	0.007	0.210	0.065	228	4/20/04 1:01	1174	8	246	76	267596		
	Total	EMC In						72736	391	7392	46507	78793372		
									0.005	0.102	0.639	1083		

Sediment Trap Outflow

Lab #	Sample Name	Sample Date	OPO4-P mg/l	NO3-N mg/l	NO2-N mg/l	TSS mg/l	Total Load (Out) milligrams		Average Concentration Value Used for flow volumes without concentrations					TSS
							Time	Interval	OPO4-P	NO3-N	NO2-N	TSS		
59952	NDOT 2B-1	4/18/04 22:21	0.003	0.46	0.052	145	4/18/04 22:21	82	0.247	38	4	11938		
59953	NDOT 2B-2	4/18/04 23:26	0.003	0.49	0.032	206	4/18/04 23:26	388	1.163	190	12	79890		
59954	NDOT 2B-3	4/19/04 0:31	0.005	0.569	0.04	238	4/19/04 0:31	2401	12.006	1366	96	571504		
59955	NDOT 2B-4	4/19/04 1:36	0.003	0.566	0.039	200	4/19/04 1:36	5663	16.989	3205	221	1132595		
59956	NDOT 2B-5	4/19/04 2:41	0.004	0.555	0.039	215	4/19/04 2:41	8682	34.727	4818	339	1866555		
59957	NDOT 2B-6	4/19/04 3:46	0.005	0.556	0.039	196	4/19/04 3:46	10576	52.882	5881	412	2072982		
59958	NDOT 2B-7	4/19/04 4:51	0.006	0.552	0.039	190	4/19/04 4:51	10826	64.958	5976	422	2056993		
59959	NDOT 2B-8	4/19/04 5:56	0.003	0.550	0.039	165	4/19/04 5:56	6617	19.852	3640	258	1091851		
59960	NDOT 2B-9	4/19/04 7:01	0.004	0.554	0.038	172	4/19/04 7:01	696	2.784	386	26	119703		
59961	NDOT 2B-10	4/19/04 8:06	0.003	0.534	0.038	157	4/19/04 8:06	2015	6.044	1076	77	316292		
59962	NDOT 2B-11	4/19/04 9:11	0.002	0.535	0.039	148	4/19/04 9:11	927	1.854	496	36	137231		
59963	NDOT 2B-12	4/19/04 10:16	0.004	0.530	0.045	428	4/19/04 10:16	279	1.117	148	13	119568		
59964	NDOT 2B-13	4/19/04 11:21	0.009	0.524	0.048	433	4/19/04 11:21	804	6.429	421	39	347977		
59965	NDOT 2B-14	4/19/04 12:26	0.008	0.513	0.049	354	4/19/04 12:26	1474	13.263	756	72	521676		
59966	NDOT 2B-15	4/19/04 13:31	0.005	0.505	0.051	422	4/19/04 13:31	1673	8.365	845	85	705990		
59967	NDOT 2B-16	4/19/04 14:36	0.002	0.494	0.052	400	4/19/04 14:36	1893	3.786	935	98	757158		
59968	NDOT 2B-17	4/19/04 15:41	0.003	0.494	0.053	338	4/19/04 15:41	1406	4.218	695	75	475259		
59969	NDOT 2B-18	4/19/04 16:46	0.003	0.486	0.053	283	4/19/04 16:46	666	1.998	324	35	188490		
59970	NDOT 2B-19	4/19/04 19:36	0.001	0.473	0.055	258	4/19/04 19:36	1372	1.372	649	75	354031		
59971	NDOT 2B-20	4/19/04 20:41	0.007	0.457	0.058	365	4/19/04 20:41	3316	23.213	1516	192	1210417		
59972	NDOT 2B-21	4/19/04 21:46	0.003	0.456	0.057	210	4/19/04 21:46	3765	11.294	1717	215	790564		
59973	NDOT 2B-22	4/19/04 22:51	0.002	0.464	0.055	236	4/19/04 22:51	3473	6.946	1611	191	819611		
59974	NDOT 2B-23	4/19/04 23:56	0.003	0.469	0.053	201	4/19/04 23:56	2568	7.705	1204	136	516211		
59975	NDOT 2B-24	4/20/04 1:01	0.002	0.504	0.056	190	4/20/04 1:01	1174	2.347	592	66	222997		
	Total	EMC OUT						72736	306	38483	3196	16487482		
									0.004	0.529	0.044	227		

## **APPENDIX B. NDOT 3 DATA**

Basin Parameters

Volume: 413 cubic feet

Infiltration Rate:

Notes for Each Storm

**07/18/02**

1. No Flow data

**11/08/02**

1. Supposed storage far exceeds basin volume
2. Loading calculations based on 1 inflow and 1 outflow composite sample

**03/16/03**

1. Supposed storage far exceeds basin volume

**04/12/03**

1. Grab sample only. No estimation of volume.
2. No associated flow volume.
3. No recent storms. Where did water come from?

**05/12/03**

1. Grab Sample

**06/23/03**

1. Supposed storage exceeds basin volume but may be accounted for by infiltration rate: Flow data shows only inflow
2. Grab Sample

**07/23/03**

1. Supposed storage far exceeds basin volume
2. No outflow chemistry data

**08/02/03**

1. Inflow data sensor failed
2. Concentration values show an overall reduction

**08/21/03**

1. Inflow data sensor failed
2. Concentration values fluctuate throughout inflow and outflow
3. Supposed storage far exceeds basin volume

**12/06/03**

1. Uncertain best method to calculate

US 50 Sediment Basin

Lab #	Sample Name	Sample Date	TKN mg/l as N	TKNsol mg/l as N	TP mg/l as N	TPsol mg/l as P	OPO4 mg/l as P	NO3NO2 mg/l as N	TSS mg/l	TU ntu
54040	NDOT-3 INFLOW	18-Jul-02	2.23	1.14	0.469	0.061	0.037	0.889	272	165
54041	NDOT-3 OUTFLOW	18-Jul-02	2.15	1.06	0.405	0.062	0.042	0.665	244	222

INFLOW and OUTFLOW samples are grab samples from the second storm on July 18th



US 50 Sediment Basin  
 Supposed storage far exceeds basin volume  
 Loading calculations based on 1 inflow and 1 outflow composite sample

US 50 Sediment Basin

Lab #	Sample Name	Sample Date	Sample Time	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TN mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Tu ntu	NH4-N mg/l	TPsol	OPO4-P	TSS	
54954	NDOT 3A-1,6,7,11 Composite	8-Nov-02	11/7/2002 19:25	0.73	0.28	0.080	0.810	0.265	0.062	0.052	116	70.1	0.006	214	50	42	89488
Average Concentration Value Used for flow volumes without concentrations EMC in mg/l      Liters/hour      TKN      NO3-N      TN      TP      TPNsol      OPO4-P      TSS																	
11/7/02 19:00      806      588      226      64      653      214      50      42      89488 11/7/02 20:00      1250      9213      3534      1010      10223      3344      762      656      1463873 11/7/02 21:00      4911      1884      538      5449      1783      417      350      780352 11/7/02 22:00      4151      3030      1162      3362      1100      257      216      481518 11/7/02 23:00      2186      1895      612      175      1770      579      136      114      253530 11/8/02 0:00      1328      970      372      106      1076      352      82      69      154080 11/8/02 1:00      1291      942      361      103      1046      342      80      67      149749 11/8/02 2:00      1328      970      372      106      1076      352      82      69      154080 11/8/02 3:00      1481      1081      415      118      1200      392      92      77      171790 11/8/02 4:00      1679      1228      470      134      1360      445      104      87      194772 11/8/02 5:00      1843      1346      516      147      1493      488      114      96      213807 11/8/02 6:00      4205      3070      1177      336      3406      1114      261      219      487787 11/8/02 7:00      5331      3892      1493      427      4318      1413      331      277      618432 11/8/02 8:00      4151      3030      1162      332      3362      1100      257      216      481518 11/8/02 9:00      2876      2099      805      230      2329      762      178      150      333965 11/8/02 10:00      2868      1961      752      215      2175      712      167      140      311544 11/8/02 11:00      2733      1995      765      219      2214      724      169      142      317004 11/8/02 12:00      3990      2913      1117      319      3232      1057      247      207      462867 Sample Total      61413      44831      17196      4913      49744      16274      3808      3193      7123854 EMC In      0.73      0.28      0.08      0.81      0.265      0.062      0.052      116																	

Lab #	Sample Name	Sample Date	Sample Time	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TN mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Tu ntu	NH4-N mg/l	TPsol	OPO4-P	TSS	
54955	NDOT 3B-1,6,7,11 Composite	8-Nov-02	11/7/2002 19:25	1.27	0.56	0.152	1.422	0.328	0.040	0.029	171	135	0.008	214	50	42	89488
Average Concentration Value Used for flow volumes without concentrations EMC Out mg/l      Liters/hour      TKN      NO3-N      TN      TP      TPNsol      OPO4-P      TSS																	
11/7/02 19:00      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0      0 11/7/02 20:00      1005      1276      563      153      1429      330      40      29      171836 11/7/02 21:00      681      865      382      104      969      223      27      20      116505 11/7/02 22:00      303      385      170      46      431      99      12      9      51802 11/7/02 23:00      1969      2501      1103      299      2800      646      79      57      336766 11/8/02 0:00      11      14      6      2      16      4      0      0      1901 11/8/02 1:00      0      0      0      0      0      0      0      0      0 11/8/02 2:00      0      0      0      0      0      0      0      0      0 11/8/02 3:00      0      0      0      0      0      0      0      0      0 11/8/02 4:00      0      0      0      0      0      0      0      0      0 11/8/02 5:00      0      0      0      0      0      0      0      0      0 11/8/02 6:00      214      272      120      33      304      70      9      6      36612 11/8/02 7:00      3218      4086      1802      489      4575      1055      129      93      550200 11/8/02 8:00      0      0      0      0      0      0      0      0      0 11/8/02 9:00      4      5      2      1      6      1      0      0      687 11/8/02 10:00      11      14      6      2      16      4      0      0      1901 11/8/02 11:00      401      509      225      61      570      132      16      12      69575 11/8/02 12:00      0      0      0      0      0      0      0      0      0 Sample Total      7817      9928      4378      1188      11116      2564      313      227      1336785 EMC Out      1.270      0.560      0.152      1.422      0.328      0.040      0.029      171																	

Lab #	Sample Name	Sample Date	Sample Time	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TN mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Tu ntu	NH4-N mg/l	TPsol	OPO4-P	TSS	
54954	NDOT 3A-1,6,7,11 Composite	8-Nov-02	11/7/2002 19:25	0.73	0.28	0.080	0.810	0.265	0.062	0.052	116	70.1	0.006	214	50	42	89488
54955	NDOT 3B-1,6,7,11 Composite	8-Nov-02	11/7/2002 19:25	1.27	0.56	0.152	1.422	0.328	0.040	0.029	171	135	0.008	214	50	42	89488
Total Load In      TKN      NO3-N      TN      TP      TPNsol      OPO4-P      TSS 44831      17196      4913      49744      16274      3808      3193      7123854 Total Load Out      9928      4378      1188      11116      2564      313      227      1336785 Percent Difference      76%      75%      76%      78%      84%      92%      93%      81%																	



US 50 Sediment Basin

Grab sample only. No estimation of volume.

No associated flow volume.

No recent storms. Where did water come from?

Lab #	Sample Name	Sample Date	TKN mg/l	NO3-N mg/l	NH4-N mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l
56536	NDOT 3 Basin	12-May-03	0.77	0.01	0.022	0.135	0.014	0.004	42.0



TSS

0  
2,822,960.87  
5,899,520.71  
3,374,810.52  
1,653,026.96  
1,010,304.48  
583,711.33  
642591  
300169  
103539  
54697  
51165  
49428  
48567  
47710  
46858  
46858  
46011  
45169  
45169  
44333  
44333  
43501  
43501  
43501  
43501  
43501  
42674  
42674  
42674  
42674  
42674  
41852  
41852  
41852  
41852  
17,601,886.11  
766



US 50 Sediment Basin

1. Inflow data sensor failed
2. Concentration values fluctuate throughout inflow and outflow
3. Supposed storage far exceeds basin volume

Lab #	Sample Name	Sample Date	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TN mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Tu ntu
57408	NDOT 3A-2	23-Aug-03	2.09	1.08	0.47	2.56	0.348	0.013	0.002	166	60.5
57409	NDOT 3A-3	23-Aug-03	1.84	1.27	0.65	2.49	0.340	0.017	0.003	152	58.5
57410	NDOT 3A-4	23-Aug-03	1.41	0.91	0.29	1.7	0.318	0.016	0.003	154	59.7
57411	NDOT 3A-5	23-Aug-03	1.27	0.68	0.38	1.65	0.319	0.012	0.002	176	56.8
57412	NDOT 3A-6	23-Aug-03	0.89	0.43	0.26	1.15	0.254	0.009	0.002	144	59.1
57413	NDOT 3A-7	23-Aug-03	0.70	0.39	0.13	0.83	0.217	0.008	0.001	114	53.1
57414	NDOT 3A-8	23-Aug-03	0.66	0.42	0.40	1.06	0.162	0.007	0.001	66	37.6
57415	NDOT 3A-9	23-Aug-03	0.64	0.43	0.48	1.12	0.142	0.008	0.001	48	31.9
57416	NDOT 3A-10	23-Aug-03	0.76	0.46	0.57	1.33	0.139	0.008	0.001	44	28.8
57417	NDOT 3B-1	23-Aug-03	1.07	0.50	0.60	1.67	0.452	0.010	0.001	290	96.3
57418	NDOT 3B-2	23-Aug-03	0.70	0.29	0.30	1.00	0.280	0.014	0.004	166	61.4
57419	NDOT 3B-3	23-Aug-03	0.36	0.22	0.12	0.48	0.191	0.011	0.003	111	49.2
57420	MDOT 3B-4	23-Aug-03	0.36	0.25	0.11	0.47	0.395	0.006	0.001	284	59.8
57421	NDOT 3B-5	23-Aug-03	0.42	0.29	0.39	0.81	0.159	0.006	0.001	97	29.2
57422	NDOT 3B-6	23-Aug-03	0.53	0.35	0.49	1.02	0.148	0.007	0.001	71	26.2
57423	NDOT 3B-7	23-Aug-03	0.70	0.55	0.82	1.52	0.152	0.011	0.001	67	25.7
57424	NDOT 3B-8	23-Aug-03	0.77	0.53	0.84	1.61	0.138	0.013	0.003	64	24.9

## **APPENDIX C. NDOT 4 DATA**



SR 28 at Secret Harbor Creek November 7-9, 2002 Loading Stormceptor Inflow

Lab #	Sample Name	Time	TKN	TKNsol	NO3-N	TP	TPsol	OPO4-P	TSS	Average Concentration Value Time	interval Liter:	TKN	TKNsol	NO3-N	TP	TPsol	OPO4-P	TSS
54874	NDOT 4-1	11/7/02 7:40	8.06	4.30	0.304	0.921	0.104	0.070	238	11/7/02 8:00	72	580	309	22	66	7	5	17130
54875	NDOT 4-2	11/7/02 8:05	9.51	3.86	0.861	1.080	0.196	0.123	258	11/7/02 9:00	1569	14919	6055	1351	1694	307	193	404731
54876	NDOT 4-3	11/7/02 9:00	3.76	1.72	0.290	0.969	0.117	0.056	420	11/7/02 9:00	5898	2698	455	1520	184	88		658864
55104	NDOT 4A-9	11/7/02 21:00	1.40	0.46	NA	NA	0.01	0.00	NA	No Corresponding Flow								
55105	NDOT 4A-10	11/7/02 22:00	1.53	0.28	NA	NA	0.03	0.02	NA	No Corresponding Flow								
54991	NDOT 4A-1	11/8/02 15:55	1.41	0.38	NA	0.331	0.035	0.022	159	11/8/02 15:00	0	1692	456	NA	397	42	26	190785
54992	NDOT 4A-2	11/8/02 16:00	1.44	0.4	NA	0.256	0.044	0.03	190	11/8/02 17:00	1200	2408	669	NA	428	74	50	317697
54993	NDOT 4A-3	11/8/02 17:00	1.42	0.35	NA	0.347	0.048	0.033	195	11/8/02 18:00	686	974	240	NA	238	33	23	133687
54994	NDOT 4A-4	11/8/02 18:00	1.12	0.29	NA	0.298	0.052	0.039	127	11/8/02 19:00	654	732	190	NA	195	34	25	83002
54995	NDOT 4A-5	11/8/02 19:00	1.13	0.31	NA	0.265	0.056	0.042	97	11/8/02 20:00	2432	2748	754	NA	644	136	102	235894
54996	NDOT 4A-6	11/8/02 20:00	0.93	0.26	NA	0.247	0.046	0.031	101	11/8/02 21:00	880	819	229	NA	217	40	27	88900
54997	NDOT 4A-7	11/8/02 21:00	0.82	0.24	NA	0.209	0.047	0.035	79	11/8/02 22:00	566	464	136	NA	118	27	20	44725
54998	NDOT 4A-8	11/8/02 22:00	0.74	0.27	NA	0.191	0.057	0.043	56	11/8/02 23:00	41	30	11	NA	8	2	2	2284
54999	NDOT 4A-9	11/9/02 15:15	0.73	0.27	NA	0.144	0.051	0.04	39	11/9/02 15:00	0	112	41	NA	22	8	6	5961
55000	NDOT 4A-10	11/9/02 23:05	0.88	0.32	NA	0.191	0.045	0.032	50	11/9/02 23:00	0	37	14	NA	8	2	1	2115
55001	NDOT 4A-11	11/10/02 11:45	1.22	0.31	NA	0.27	0.03	0.02	110.67	11/10/02 10:00	0	3	1	NA	1	0	0	307
55002	NDOT 4A-12	11/10/02 12:00	1.19	0.44	NA	0.231	0.025	0.01	82	11/10/02 12:00	15	18	7	NA	4	0	0	1243
55003	NDOT 4A-13	11/10/02 13:00	1.36	0.25	NA	0.269	0.018	0.007	97	11/10/02 13:00	904	1230	226	NA	243	16	6	87711
			1.1	0.25	NA	0.299	0.055	0.04	153	11/10/02 14:00	706	777	177	NA	211	39	28	108087
										11/10/02 15:00	53	64	17	NA	14	2	1	5862
										Totals	11648	33505	12228	NA	6029	954	605	2388983
										EMC in	2.88	2.88	1.05	NA	0.52	0.08	0.05	205

Stormceptor Outflow

Lab #	Sample Name	Time	TKN	TKNsol	NO3-N	TP	TPsol	OPO4-P	TSS	Average Concentration Value Time	interval Liter:	TKN	TKNsol	NO3-N	TP	TPsol	OPO4-P	TSS
54877	NDOT 4B-3	11/7/02 9:00	4.18	2.52	0.022	0.574	0.100	0.045	165	11/7/02 8:00	72	6557	3953	35	900	157	71	258839
55106	NDOT 4B-9	11/7/02 21:00	0.98	0.27	NA	NA	0.01	0.00	NA	11/7/02 9:00	1569							
55107	NDOT 4B-10	11/7/02 22:00	0.93	0.28	NA	NA	0.05	0.03	NA	11/8/02 15:00	0	1512	288	#VALUE!	386	49	36	203984
55004	NDOT 4B-1	11/8/02 15:55	1.26	0.24	NA	0.322	0.041	0.03	170	11/8/02 16:00	1200	1438	368	#VALUE!	380	84	67	155504
55005	NDOT 4B-2	11/8/02 16:00	0.86	0.22	NA	0.227	0.05	0.04	93	11/8/02 17:00	1672	747	233	#VALUE!	183	46	34	49361
55006	NDOT 4B-3	11/8/02 17:00	1.09	0.34	NA	0.267	0.067	0.049	72	11/8/02 18:00	686	621	209	#VALUE!	149	46	34	63769
55007	NDOT 4B-4	11/8/02 18:00	0.95	0.32	NA	0.228	0.071	0.052	leaked	11/8/02 19:00	654	1629	486	#VALUE!	426	126	100	119163
55008	NDOT 4B-5	11/8/02 19:00	0.67	0.2	NA	0.175	0.052	0.041	49	11/8/02 20:00	2432	634	220	#VALUE!	122	49	38	35208
55009	NDOT 4B-6	11/8/02 20:00	0.72	0.25	NA	0.139	0.056	0.043	40	11/8/02 21:00	880	425	170	#VALUE!	96	42	32	14153
55010	NDOT 4B-7	11/8/02 21:00	0.75	0.3	NA	0.169	0.075	0.056	25	11/8/02 22:00	566	97	26	#VALUE!	17	1	0	9545
55011	NDOT 4B-8	11/8/02 22:00	2.37	0.64	NA	0.417	0.017	0.002	234	11/8/02 23:00	41	425	97	26	#VALUE!	17	0	
			2.37	0.64	NA	0.417	0.017	Average	98	11/9/02 15:00	0							

55012	NDOT 4B-9	11/9/02 15:15	2.4	0.98	NA	0.358	0.015	0.004	204	11/9/02 16:00	153	367	150	#VALUE!	55	2	1	31178
55013	NDOT 4B-10	11/9/02 23:05	2.22	0.73	NA	0.541	0.017	0.008	340	11/9/02 23:00	0	94	31	#VALUE!	23	1	0	14385
										11/10/02 0:00	42							
55014	NDOT 4B-11	11/10/02 11:45	1.83	0.47	NA	0.59	0.023	0.01	375	11/10/02 10:00	0	5	1	#VALUE!	2	0	0	1040
55015	NDOT 4B-12	11/10/02 12:00	2.01	0.61	NA	0.64	0.022	0.012	leaked	11/10/02 11:00	3	30	9	#VALUE!	10	0	0	5675
55016	NDOT 4B-13	11/10/02 13:00	1.97	0.33	NA	0.802	0.028	0.019	558	11/10/02 12:00	15	1781	298	#VALUE!	725	25	17	504564
			1.51	0.46	NA	0.334	0.018	0.007	191	11/10/02 13:00	904	1067	325	#VALUE!	236	13	5	134932
										11/10/02 14:00	706	97	25	#VALUE!	31	1	1	19836
										11/10/02 15:00	53	17101	6793	#VALUE!	3741	644	434	1621138
										Totals	11648							

SR 28 at Secret Harbor Creek January 23, 2003 Loading Stormceptor Inflow

Total Load (In) milligrams																			
Average Concentration Value Used for flow volumes without concentrations																			
Lab #	Sample Name	Time	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS	
55475	NODT 4A-1	1/23/03 13:05	4.16	0.46	0.04	1.39	0.026	0.014	1150.00	352	1417	166	23	1441	581	20	14	0	505604
55476	NODT 4A-2	1/23/03 13:10	4.22	0.50	0.05	1.74	0.068	0.052	1430.00	284	1144	134	19	1163	469	16	11	0	408055
55477	NODT 4A-3	1/23/03 14:00	3.01	0.56	0.12	0.94	0.070	0.047	1100.00	1703	6889	789	78	6967	2573	77	54	0	2120848
55478	NODT 4A-5	1/23/03 16:00	4.70	0.36	0.05	2.52	0.060	0.045	2060.00	1644	4949	921	197	5146	1547	115	77	0	1808475
	Average		4.02	0.47	0.07	1.65	0.056	0.040	1435.00	4217	16964	1982	280	17244	6949	236	167	0	6051723
	Average		3.99	0.47	0.07	1.71	0.064	0.046	1506.25	6076	24439	2856	404	24843	10011	340	240	16	725614
	Average		3.93	0.47	0.08	1.71	0.062	0.044	1525.31	6896	27739	3241	459	28197	11363	386	272	9895622	8718536
	Average		4.16	0.44	0.07	1.90	0.060	0.044	1631.64	8137	32732	3825	541	33273	13408	456	321	11676995	311676895
	Average		4.03	0.46	0.07	1.74	0.061	0.043	1524.55	2392	9624	1124	159	9783	3942	134	95	3433161	11676995
	Average		4.03	0.46	0.07	1.76	0.062	0.044	1546.94	542	2180	255	36	2216	893	30	21	777841	21777841
	Average		4.04	0.46	0.07	1.78	0.061	0.044	1557.11	192	772	90	13	785	316	11	8	275423	275423
	Average		4.06	0.46	0.07	1.79	0.061	0.044	1565.06	112	452	53	7	460	185	6	4	161378	161378
	Average		4.04	0.46	0.07	1.77	0.061	0.044	1548.41	112	452	53	7	460	185	6	4	161378	161378
	Average		4.04	0.46	0.07	1.78	0.061	0.044	1554.38	89	359	42	6	365	147	5	4	128082	128082
	Average		4.04	0.46	0.07	1.78	0.061	0.044	1556.24	32	127	15	2	129	52	2	1	45304	45304
	Average		4.05	0.46	0.07	1.78	0.061	0.044	1556.02	0	0	0	0	0	0	0	0	0	0
Total											33134	131895	15671	2251	134146	53509	1862	1310	46894238
EMC in											3.98	0.47	0.07	4.05	1.61	0.056	0.040	1415.28	

Stormceptor Outflow

Total Load (Out) milligrams																			
Average Concentration Value Used for flow volumes without concentrations																			
Lab #	Sample Name	Time	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS	
55479	NODT 4B-1	Average	3.65	0.41	0.03	1.49	0.046	0.030	1116	0	0	0	0	0	0	0	0	0	393208
55480	NODT 4B-2	1/23/03 13:05	2.75	0.44	0.02	0.88	0.016	0.002	664.00	352	1285	145	12	1297	525	16	11	0	317345
55481	NODT 4B-3	1/23/03 13:10	3.86	0.48	0.05	1.50	0.047	0.032	1080.00	284	1037	117	10	1047	423	13	9	0	317345
55482	NODT 4B-5	1/23/03 14:00	3.44	0.43	0.05	1.38	0.069	0.049	980.00	1703	5434	756	50	5484	1954	52	28	0	1433627
	Average		4.54	0.30	0.03	2.20	0.051	0.038	1740.00	1644	5656	707	74	5730	2269	113	81	0	1611187
	Average		3.65	0.41	0.03	1.49	0.046	0.030	1116.00	4217	15382	1740	147	15629	6281	193	128	0	4706427
	Average		3.87	0.41	0.04	1.64	0.053	0.037	1229.00	352	1600	106	12	1611	775	18	13	0	613066
	Average		3.87	0.39	0.04	1.68	0.055	0.039	1266.25	6076	22161	2506	211	22372	9048	278	184	0	6780408
	Average		3.98	0.38	0.04	1.75	0.051	0.036	1337.81	6896	25153	2845	240	25392	10270	315	209	0	7695829
	Average		3.84	0.40	0.04	1.64	0.051	0.036	1237.27	8137	29681	3357	283	29963	12118	372	246	0	9081203
	Average		3.89	0.39	0.04	1.68	0.052	0.037	1267.58	542	1977	224	19	1996	807	25	16	0	2669970
	Average		3.90	0.39	0.04	1.69	0.052	0.037	1277.23	192	700	79	7	707	286	9	6	0	604927
	Average		3.91	0.39	0.04	1.69	0.052	0.036	1279.97	112	410	46	4	414	167	5	3	0	214197
	Average		3.89	0.39	0.04	1.67	0.052	0.036	1265.51	112	410	46	4	414	167	5	3	0	125503
	Average		3.90	0.39	0.04	1.68	0.052	0.037	1272.57	89	326	37	3	329	133	4	3	0	99610
	Average		3.90	0.39	0.04	1.68	0.052	0.037	1273.82	32	115	13	1	116	47	1	1	0	35233
	Average		3.90	0.39	0.04	1.68	0.052	0.036	1272.97	0	0	0	0	0	0	0	0	0	0
Total											33134	120053	13711	1159	121211	48834	1530	1012	36507244
EMC out											3.62	0.41	0.03	3.66	1.47	0.046	0.031	1101.80	







SR 28 at Secret Harbor Creek April 2, 2003 Loading

Stormceptor Inflow

Lab #	Sample Name	Time	TKN mg/l	TKNsol mg/l	NO3 mg/l	TP mg/l	TPsol mg/l	OPO4 mg/l	TSS mg/l	Average Concentration Value Used for flow volumes without concentrations	TKN Interval Liters	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS
		Average	2.80	1.71	0.24	0.66	0.063	0.025	532.50	0	0	0	0	0	0	0	0	0
		Average	2.80	1.71	0.24	0.66	0.063	0.025	532.50	368	1028	629	86	1114	244	23	9	195770
		Average	2.80	1.71	0.24	0.66	0.063	0.025	532.50	1349	3770	2306	317	4087	894	85	33	718198
		Average	2.80	1.71	0.24	0.66	0.063	0.025	532.50	599	1675	1025	141	1816	397	38	15	319174
		Average	2.80	1.71	0.24	0.66	0.063	0.025	532.50	499	1396	854	117	1513	331	32	12	265898
		Average	2.80	1.71	0.24	0.66	0.063	0.025	532.50	1170	3271	2001	275	3546	776	29	29	623188
56088	NDOT 4A-2	4/2/03 15:20	2.80	1.63	0.23	0.66	0.048	0.016	532.50	1411	3951	2300	325	4275	919	68	23	751329
		Average	2.80	1.71	0.24	0.66	0.063	0.025	532.50	429	1198	733	101	1299	284	27	11	228272
		Average	2.80	1.71	0.24	0.66	0.063	0.025	532.50	1136	3175	1942	267	3442	753	72	28	604834
		Average	2.80	1.79	0.24	0.68	0.079	0.033	532.50	646	1804	1156	155	1959	436	51	21	343771
56089	NDOT 4A-4	4/2/03 20:05	2.79	1.95	0.25	0.70	0.109	0.050	508.00	476	1329	929	119	1448	333	52	24	241904
		Average	2.64	1.91	0.24	0.67	0.112	0.050	532.50	272	719	519	65	785	183	30	13	145058
56090	NDOT 4A-5	4/2/03 21:10	2.49	1.86	0.23	0.64	0.114	0.049	557.00	177	442	330	41	482	114	20	9	98769
		Average	2.64	1.91	0.24	0.67	0.112	0.050	532.50	88	232	167	21	253	59	10	4	46707
		Total							8620	23988	14890	2030	26018	5722	582	230		4582892
									EMC in	2.78	1.73	0.24	3.02	0.66	0.067	0.027		532

Stormceptor Outflow

Lab #	Sample Name	Time	TKN mg/l	TKNsol mg/l	NO3-N mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Average Concentration Value Used for flow volumes without concentrations	TKN Interval Liters	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	0	0	0	0	0	0	0	0	0
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	368	463	210	13	477	132	14	6	66176
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	1349	1699	769	49	1749	484	53	21	242771
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	599	755	342	22	777	215	23	9	107890
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	499	629	285	18	647	179	19	8	89881
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	1170	1475	667	43	1517	420	46	18	210655
56091	NDOT 4B-2	4/2/03 15:20	1.15	0.52	0.01	0.32	0.055	0.027	128.00	1411	1623	734	13	1635	452	78	38	180601
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	429	540	244	16	556	154	17	7	77162
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	1136	1431	647	41	1473	407	44	18	204451
		Average	1.26	0.57	0.04	0.36	0.039	0.016	180.00	646	813	368	24	837	231	25	10	116204
56092	NDOT 4B-4	4/2/03 20:05	1.37	0.62	0.06	0.40	0.023	0.004	232.00	476	652	295	30	683	189	11	2	110476
		Average	1.41	0.65	0.08	0.39	0.032	0.008	222.00	272	384	177	22	406	107	9	2	60475
56093	NDOT 4B-5	4/2/03 21:10	1.45	0.68	0.10	0.39	0.040	0.012	212.00	177	257	121	18	275	69	7	2	37600
		Average	1.41	0.65	0.08	0.39	0.032	0.008	222.00	88	124	57	7	131	35	3	1	19472
		Total							8620	10846	4915	317	11163	3073	349	141		1523815
									EMC out	1.26	0.57	0.04	1.29	0.36	0.040	0.016		177









SR 28 at Secret Harbor Creek June 22, 2003 Loading

Stormceptor Inflow

Lab #	Sample Name	Sample Time	Total Load (In) milligrams																
			TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS
57088	NDOT 4A-2	7/22/03 16:30	9.88	3.62	0.10	9.98	2.38	0.059	0.008	2000.00	6262	61870	22669	626	62497	14904	369	50	12524361
57089	NDOT 4A-3	7/22/03 17:35	7.03	3.53	0.16	7.19	1.53	0.469	0.346	1070.00	1551	10903	5475	248	11151	2373	727	537	1659516
											7813	72774	28144	874	73648	17277	1097	587	14183877
											EMC in	9.31	3.60	0.11	9.43	2.21	0.140	0.075	1815

Stormceptor Outflow

Lab #	Sample Name	Time	Total Load (Out) milligrams																
			TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS	Average Concentr	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS
57090	NDOT 4B-2	7/22/03 16:30	6.17	3.10	0.04	6.21	1.08	0.112	0.025	680.00	6262	38638	19413	257	38894	6763	701	157	4258283
57091	NDOT 4B-3	7/22/03 17:35	4.49	2.10	0.04	4.53	0.91	0.048	0.013	464.00	1551	6964	3257	54	7018	1405	74	20	719640
											7813	45601	22670	311	45912	8168	776	177	4977923
											EMC out	5.84	2.90	0.04	5.88	1.05	0.099	0.023	637

SR 28 at Secret Harbor Creek July 23, 2003 Loading

Stormceptor Inflow

Lab #	Sample Name	Time	Total Load (In) milligrams																
			TKN mg/l	TKNsol mg/l	NO3-N mg/l	TN mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS
57119	NDOT 4A-2	7/23/03 15:20	4.33	1.40	0.20	4.53	1.95	0.031	0.004	1470.00	6662	28848	9327	1332	30180	12992	207	27	9793621
57120	NDOT 4A-3	7/23/03 16:25	2.15	0.52	0.16	2.31	1.31	0.092	0.046	788.00	1982	4262	1031	317	4579	2597	182	91	1561914
											8644	33109	10358	1650	34759	15588	389	118	11355535
											EMC in	3.83	1.20	0.19	4.02	1.80	0.04	0.014	1314

Stormceptor Outflow

Lab #	Sample Name	Time	Total Load (Out) milligrams																
			TKN mg/l	TKNsol mg/l	NO3-N mg/l	TN mg/l	TP mg/l	TPsol mg/l	OPO4-P mg/l	TSS mg/l	Interval Liters	TKN	TKNsol	NO3-N	TN	TP	TPsol	OPO4-P	TSS
57121	NDOT 4B-2	7/23/03 15:20	4.10	1.43	0.02	4.12	1.85	0.034	0.006	1540.00	6662	27316	9527	133	27449	12325	227	40	10259984
57122	NDOT 4B-3	7/23/03 16:25	2.25	0.60	0.027	2.28	1.15	0.028	0.004	772.00	1982	4460	1189	54	4513	2279	55	8	1530200
											8644	31775	10716	187	31962	14605	282	48	11790184
											EMC out	3.68	1.24	0.02	3.70	1.69	0.03	0.006	1364



