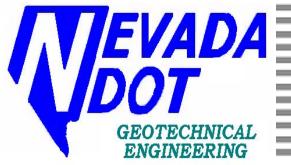
#### **GEOTECHNICAL REPORT**

CARSON FREEWAY
CLEARVIEW DRIVE GRADE SEPARATION
CARSON CITY
EA 72781
DECEMBER 2003





**MATERIALS DIVISION** 

# STATE OF NEVADA DEPARTMENT OF TRANSPORTATION MATERIALS DIVISION GEOTECHNICAL SECTION

## GEOTECHNICAL REPORT CARSON FREEWAY CLEARVIEW DRIVE GRADE SEPARATION

December 2003

E.A. 72781 Fund 1 CARSON CITY, NEVADA

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#### **INTRODUCTION**

#### <u>General</u>

This report has been prepared for the planned grade separation located at Clearview Drive, crossing over the proposed Carson Freeway in Carson City, Nevada. Clearview Drive runs generally east-west in this location, and is currently one lane wide in each direction (See Photo 1). The proposed freeway will run in a north-south direction, approximately 20 to 25 below existing grade, crossing under Clearview Drive approximately 200 feet west of South Edmonds Drive. To date, the proposed plan calls for construction of a double span concrete structure. For a more detailed description, see the contract plans. A site plan for the project is presented in Appendix A.



Photo 1. Clearview Drive: Looking West toward US 50.

#### Purpose and Scope

The purpose of this report is to provide information regarding the subsurface soil conditions at the proposed project site. This report also provides geotechnical design recommendations for the bridge structure proposed for this project. The scope of this report consists primarily of geotechnical investigation, analysis, and recommendations for both design and construction. The investigation included gathering data from past field explorations and reports, in addition to information obtained from recent subsurface explorations, soil sampling, and analysis of field and laboratory testing data. This report includes boring logs and summaries of test results from the field investigations and the laboratory testing regimen. These may be found in appendices B and C, respectively.

#### PROJECT DESCRIPTION

The project site is located in southwestern Carson City (See Photo 2). The freeway runs approximately 20 feet below the existing grade as shown in the current plans, and will pass under Clearview Drive. Preliminary plans indicate the proposed bridge will be designed as a double span concrete structure over the freeway alignment, conveying two lanes of traffic in each direction. It will be supported on spread footings founded in native soil. The new structure will be approximately 60 feet in width and 210 feet in length.



Photo 2. Clearview Drive: Looking East toward S. Edmonds Drive.

#### **GEOLOGIC CONDITIONS and SEISMICITY**

The site is founded primarily in pediment and alluvial fan deposits (Qpa). These deposits are generally grayish-orange, tan, and gray-brown muddy sands and sandy gravels<sup>1</sup>. Although not anticipated, variable site conditions include the possibility of encountering large cobbles, boulders, or other adverse soil conditions.

This area lies at an elevation of approximately 4740 feet and slopes gently downward ( $\approx$ 3%) to the west<sup>2</sup>. Groundwater was measured nine weeks after drilling at a depth of approximately 72 feet in borehole CV-1. There are several seismic features near the project site; among them are three significant Fault Zones. The Genoa Fault Zone, approximately 4.0 miles to the west-southwest; the Carson City Fault, which lies about 2.0 miles to the west-northwest; and the Eastern Prison Hill Fault Zone, which lies about 7 miles to the northeast. These Holocene faults (<11,000 years old) are capable of producing large (magnitude 6.6 to 7.4) earthquakes. Estimates for the interval of

recurrence for these faults range from once every 1350 years, to less than once every 16,000 years<sup>3,4,5,6</sup>.

#### **FIELD INVESTIGATION**

The Geotechnical Section conducted a subsurface investigation at the proposed project site in July 2002. Subsurface soil conditions were explored in the investigation by drilling three boreholes placed along the Clearview Drive alignment near the proposed locations for the center pier and each abutment. The approximate location of each borehole is shown on the <u>Borehole Location</u> sheet in Appendix A. Boreholes CV-1, CV-2, and CV-3 were drilled to depths of 88.5 feet, 40.0 feet, and 118.0 feet, respectively. The surface elevations were obtained for the borehole locations by surveying from a known elevation point.

Drilling was accomplished utilizing a Mobile B-80 drill rig using wet rotary drilling with bentonite slurry on boreholes CV-1, and CV-3. Borehole CV-2 was drilled with a Mobile B-57 drill rig with 6-inch hollow stem auger. Both drill rigs were equipped for soil sampling. Soil samples and standard penetration resistance values (N-Values) were obtained utilizing the Standard Penetration Test (SPT) procedure as set forth in ASTM test number T206. The uncorrected blow counts are shown on the boring logs in Appendix B. Soil conditions were not suitable for using thin-walled Shelby tubes (SH), allowing only disturbed samples to be obtained. All soil samples were classified, both visually and using laboratory data, using the Unified Soil Classification System (USCS) described in ASTM test number D2487.

#### LABORATORY ANALYSIS

Laboratory tests were performed on the samples collected from the boreholes. The testing program consisted of sieve analyses, moisture and unit weight, Atterberg limits, direct shear tests, specific gravities, and chemical analyses (chlorides, resistivity, pH). The results of this testing program show that the soils consist primarily of silty and clayey sands, with occasional gravel and interspersed clay layers. Further information is presented in the summaries of test results in Appendix C. Dry unit weights from 25 samples ranged from 96.4 pounds per cubic foot (pcf) in sandy lean clay, to 123.7 pcf in silty sand. The average dry unit weight for the soils was 115 pcf.

#### **DISCUSSION**

The project site is located in one of the most seismically active regions in the state, which places this area at risk for liquefaction. Possible causes of liquefaction include seismic activity or induced vibrations. However, upon examination of specific site data, it has been determined that liquefaction will probably not occur due to soil densities, and low moisture content in combination with Atterberg limits<sup>7</sup>.

High soil densities and a deep water table combine to make the site suitable for the use of spread footings for the bridge foundation. Initial settlement due to loading at the abutments is estimated to be between ½" and 1½", depending on the width and depth of the footing (see Table 1) with differential settlement being approximately one-half of the total settlement. This settlement should be immediate, occurring during construction, and is based on loading the foundations to four kips per square foot (4 ksf). Settlement due to consolidation should be negligible. The proposed construction of the bridge follows the

existing vertical profile over the depressed freeway, and has no significant increase in overburden in embankment. No additional settlement is expected to occur in these areas.

	CLEARVIEW DRIVE- SETTLEMENT SUMMARY  Compilation of Settlement Ranges in Inches based on 4 ksf loading										
	WE	ST ABUTM	ENT		ENTER PIE		EAS	ST ABUTME	ENT		
Footing Width	3'	4'	5'	Bottom of Footing Depth 3' 4' 5'			3' 4' 5'				
4'	3/4"	3/4"	3/4"	1/2"	1/2"	1/2"	1/2"	1/2"	1/2"		
6'	1"	3/4"	3/4"	1/2"	1/2"	1/2"	3/4"	3/4"	3/4"		
8'	1-1/4"	1"	1"	3/4"	3/4"	1/2"	1"	1"	1"		
10'	1-1/4"	1-1/4"	1-1/4"	1"	1"	1"	1-1/2"	1-1/4"	1-1/4"		

**Table 1. Settlement Summary** 

#### RECOMMENDATIONS

All excavation shall be performed in accordance with the NDOT <u>2001 Standard Specifications for Road and Bridge Construction</u>. All permanent slopes should be constructed to lie at a maximum of 2:1 (Horiz:Vert) slope. The contractor shall be responsible for all necessary shoring for any excavation and/or construction. Although not anticipated, variable site conditions include the possibility of encountering large cobbles, boulders, very soft soils, or other adverse soil conditions.

The very dense sandy soils are well suited for spread footings. AASHTO recommends using a factor of safety of 3.00 in conjunction with this type of analysis. This factor of safety was used to calculate the allowable bearing capacity of the spread footings. Abutment footings placed on cut slopes in native ground should be a minimum of eight feet wide and extend a minimum of six feet deep. These footings will have an allowable bearing capacity of 4500 psf. The center pier footings should be a minimum of six feet wide and extend a minimum of four feet deep. These footings will have an allowable bearing capacity of 7000 psf.

#### **Abutment Retaining Walls**

The Acceleration Coefficient (A), Soil Profile Type, and Site Coefficient (S), are all obtained from AASHTO Standard Specifications for Highway Bridges, Division 1-A, Section 3. The horizontal Acceleration Coefficient (Kh) is obtained from AASHTO Standard Specifications for Highway Bridges, Division 1-A, Section 6. The vertical Acceleration Coefficient (Kv) is assumed to be zero. Earth pressure coefficients are calculated using Coulombs analysis method utilizing the Mononobe-Okabe equation for Ka, Kp, Kae, and Kpe. The structure - soil interface angle is taken as <sup>2</sup>/<sub>3</sub>φ. These design parameters are found in tables 1 and 2.

#### **Recommended Design Parameters for Abutment Retaining Walls**

Backfill Slope	2H:1V
$\phi_1$ = soil friction angle (native)	32°
$\delta_1$ = structure - soil interface angle (native)	21.3°
$\gamma_1$ ' = effective soil unit weight	115 pcf
A = Acceleration Coefficient (AASHTO)	0.40
Soil Profile Type (AASHTO)	II
S = Site Coefficient (AASHTO)	1.2
K <sub>a</sub> = Active Earth Pressure Coefficient (Coulomb)	0.275
K <sub>p</sub> = Passive Earth Pressure Coefficient (Coulomb)	N/A
$K_h$ = Horizontal Acceleration Coefficient (Abutments May Displace)	0.20
$K_h$ = Horizontal Acceleration Coefficient (Abutments Restrained)	0.60
$K_v = Vertical Acceleration Coefficient$	0.00
K <sub>ae</sub> = Dynamic Active Earth Pressure Coefficient (Mononobe-Okabe)	0.688
K <sub>pe</sub> = Dynamic Passive Earth Pressure Coefficient (Mononobe-Okabe)	N/A
Coefficient of Base Friction (Sliding)	0.40

**TABLE 1 - Native Soil** 

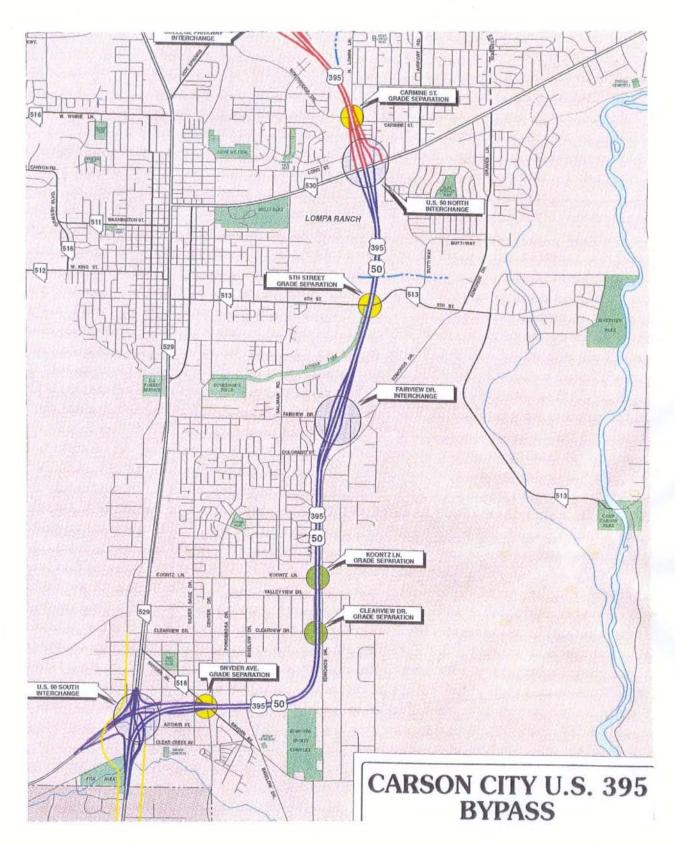
Backfill Slope	2H:1V
$\phi_2$ = soil friction angle (backfill)	34°
$\delta_2$ = structure - soil interface angle (backfill)	22.7°
$\gamma_2$ ' = effective soil unit weight	125 pcf
A = Acceleration Coefficient (AASHTO)	0.40
K <sub>a</sub> = Active Earth Pressure Coefficient (Coulomb)	0.254
K <sub>p</sub> = Passive Earth Pressure Coefficient (Coulomb)	N/A
$K_h$ = Horizontal Acceleration Coefficient (Abutments May Displace)	0.20
$K_h$ = Horizontal Acceleration Coefficient (Abutments Restrained)	0.60
$K_v$ = Vertical Acceleration Coefficient	0.00
K <sub>ae</sub> = Dynamic Active Earth Pressure Coefficient (Mononobe-Okabe)	0.426
K <sub>pe</sub> = Dynamic Passive Earth Pressure Coefficient (Mononobe-Okabe)	N/A
Coefficient of Base Friction (Sliding)	0.40

TABLE 2 - Backfill

#### **REFERENCES**

- New Empire Geologic Map; Nevada Bureau of Mines and Geology, Map 59, 1977.
- 2. New Empire Folio Slope Map; Nevada Bureau of Mines and Geology, 1973.
- 3. <u>Earthquake Occurrence in the Reno-Carson City Urban Corridor; dePolo, Anderson, dePolo, and Price;</u> Seismological Research Letters, Volume 68; May/June 1997; from Internet article dated 12/31/01 modified by The Nevada Seismological Laboratory.
- 4. New Empire Quadrangle Earthquake Hazards Map; Nevada Bureau of Mines and Geology, Map 1Bi, Bell and Trexler, 1979.
- 5. Genoa Quadrangle Earthquake Hazards Map; Nevada Bureau of Mines and Geology, Map 1Ci, Pease, 1979.
- 6. Carson City Quadrangle Earthquake Hazards Map; Nevada Bureau of Mines and Geology, Map 1Ai, Trexler and Bell, 1979.
- 7. FHWA Geotechnical Earthquake Engineering, FHWA HI-99-012, 1998.
- 8. AASHTO <u>Standard Specifications for Highway Bridges</u>, sixteenth edition, 1996; with interims through 1999.
- 9. <u>Standard Specifications for Road and Bridge Construction</u>, State of Nevada Department of Transportation, 2001.

### APPENDIX A



SITE PLAN

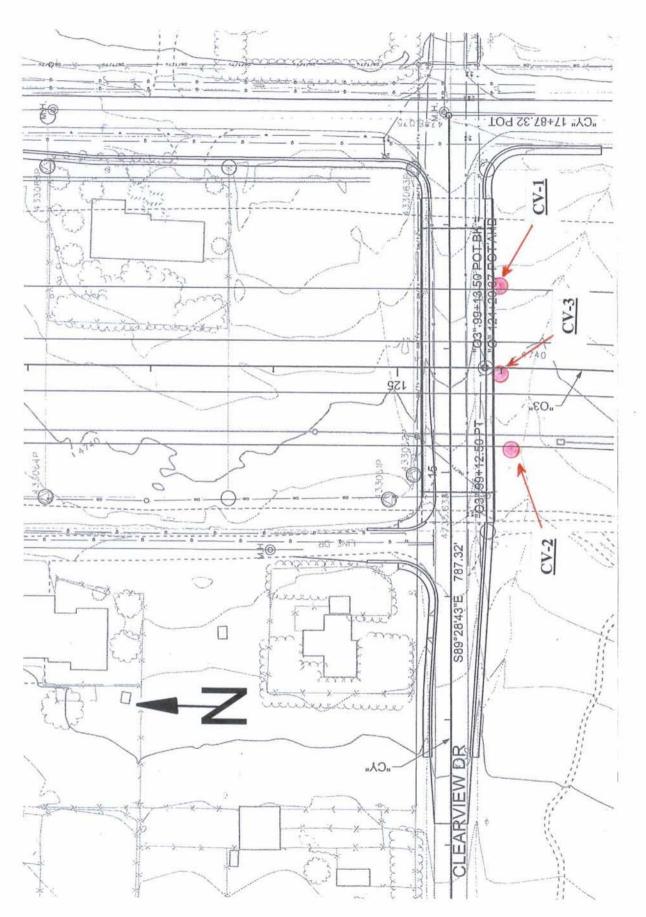


Plate 2

## APPENDIX B

#### **KEY TO BORING LOGS**

CLAY	SILT		SAND		GR	AVEL	COBBLES	BOULDERS
		FINE	MEDIUM	COARSE	FINE	COARSE		
	1							

USCS GROUP	TYPICAL SOIL DESCRIPTION
GW	Well graded gravels, gravel-sand mixtures, little or no fines
GP	Poorly graded gravels, gravel-sand mixtures, little or no fines
GM	Silty gravels, poorly graded gravel-sand-silt mixtures
GC	Clayey gravels, poorly graded gravel-sand-clay mixtures
sw	Well graded sands, gravelly sands, little or no fines
SP	Poorly graded sands, gravelly sands, little or no fines
SM	Silty sands, poorly graded sand-silt mixtures
sc	Clayey sands, poorly graded sand-clay mixtures
ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands with slight plasticity
CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays
OL	Organic silts and organic silt-clays of low plasticity
MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts
СН	Inorganic clays of high plasticity, fat clays
ОН	Organic clays of medium to high plasticity
CS	Claystone/Siltstone
PT	Peat and other highly organic soils

#### MOISTURE CONDITION CRITERIA

#### SOIL CEMENTATION CRITERIA

moior order c	ONDITION CRITERIA	SOIL CEMEN	IATION CRITERIA
Description	Criteria	Description	Criteria
Dry	Absence of moisture, dusty, dry to touch.	Weak	Crumbles or breaks with handling or little finger pressure.
Moist Wet	Damp, no visible free water. Visible free water, usually below	Moderate	Crumbles or breaks with considerable finger pressure.
	groundwater table.	Strong	Won't break or crumble w/finger pressure

 $\nabla$ 

**Groundwater Elevation Symbols** 

G	RANULAR SOIL	CLAYEY SOIL		
BLOWS/FT	DENSITY	BLOWS/FT	CONSISTENCY	
0 - 4	VERY LOOSE	0 - 1	VERY SOFT	
5 - 10	LOOSE	2 - 4	SOFT	
11 - 30	MEDIUM DENSE	5 - 8	MEDIUM STIFF	
31 - 50	DENSE	9 - 15	STIFF	
OVER 50	VERY DENSE	16 - 30	VERY STIFF	
*Standard Penet	ration Test (N) 140 lb hammer	31 - 60	HARD	
30 inch free fall	on 2 inch O.D. x 1.4 inch I.D. sampler.	OVER 60	VERY HARD	

Blow counts on Calif. Modified Sampler (N<sub>CMS</sub>) can be converted to N<sub>SPT</sub> by: (N<sub>CMS</sub>)(0.62) = N<sub>SPT</sub>

Blow counts from Automatic or Safety Hammer can be converted to Standard SPT  $N_{60}$  by:  $(N_{AUTOMATIC})(1.25) = N_{60}$   $(N_{SAFETY})(1.17) = N_{60}$ 

TEST	ABBREVIATIONS			SAMI	PLER NOTATION
CD	CONSOLIDATED DRAINED CHEMICAL (CORROSIVENESS)	o oc	ORGANIC CONTENT CONSOLIDATIONCPT	CMS	CALIF. MODIFIED SAMPLER CONE PENETRATION
CM	COMPACTION	PI	PLASTICITY INDEX	cs	CONTINUOUS SAMPLER®
CU	CONSOLIDATED UNDRAINED	RQD	ROCK QUALITY DESIGNATION	CSS	CALIFORNIA SPLIT SPOON <sup>®</sup>
D	DISPERSIVE SOILS	RV	R-VALUE	P	PUSHED (NOT DRIVEN)
DS	DIRECT SHEAR	S	SIEVE ANALYSIS	PB	PITCHER BARREL
E	EXPANSIVE SOIL	SL	SHRINKAGE LIMIT	RC	ROCK CORE®
G	SPECIFIC GRAVITY	U	UNCONFINED COMPRESSION	SH	SHELBY TUBE®
H	HYDROMETER	UU	UNCONSOLIDATED UNDRAINED	SPT	STANDARD PENETRATION TEST
HC	HYDRO-COLLAPSE	UW	UNIT WEIGHT	TP	TEST PIT
K	PERMEABILITY	W	MOISTURE CONTENT		
				①- I.D.=	2.421 inch
20000000		-C-1112-112-1		②- I.D.=	3.228 inch with tube; 3.50 inch w/o tube
SOIL	COLOR DESIGNATIONS ARE FROM	THE MU	NSELL SOIL COLOR CHART.	3)- NXB	I.D.= 1.875 inch
	EXAMPLE: (7.5 YR 5/3) BROY	WN		4 I.D.=	2.875 inch



7/1/02 START DATE

7/2/02

END DATE JOB DESCRIPTION CARSON FREEWAY

LOCATION CV-1

**CLEARVIEW DRIVE GRADE SEPARATION** 

**BORING** 

E.A.#

72781

GROUND ELEV. 4743.03 (ft)

HAMMER DROP SYSTEM SAFETY

**EXPLORATION LOG** 

**GROUNDWATER LEVEL** 

DATE | DEPTH ft | ELEV. ft

7/8/02 56.10 4686.9 9/3/02 72.50 4670.5

SHEET 1 OF 3

"CV"16+51 STATION

43' Right OFFSET

**BOOMHOWER ENGINEER** MOBILE B-80 **EQUIPMENT** 

**ALTAMIRANO OPERATOR** 

DRILLING METHOD Wet w/ Bentonite Slurry

BACKFILLED \_\_\_\_\_ DATE \_

ELEV.	DEPTH		/PLE	BLOW CO	Last	Percent	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
(ft)	(ft)	NO.	TYPE	Increments	1 foot	Recov'd		Group	Waterway Beattin Hait	1
	-								SILTY SAND dry, with scrub brush	
	2.00	Λ	CMS	32	50/5"	100			<u>SILTY SAND</u> damp, brownish yellow (10 YR	
	2.90	A		50/5" 35				SM	6/6), very dense, partially cemented	
	3.80	В	SPT	50/5"	50/5"	100				
4738.0 -	<b>-</b> 5									
00.0									5.50 SILTY CLAYEY SAND damp, brownish yellow	
	7.00							SC SM	(10 YR 6/6), very dense, partially cemented	
	7.90	С	CMS	52 50/4.5"	50/4.5"	100		SIVI		
	8.70	D	SPT		50/3.5"	100			CLAYEY SAND damp, brownish yellow (10 YR 6/6), very dense, partially cemented	
	-							SC		
4733.0 -	10								10.00 SILTY SAND damp, brownish yellow (10 YR	-
	-								6/6), very dense, partially cemented	
	12.00			23						
	- 13.25	E	SPT	52 50/3"	50/3"	80				
	-			30/3						
4728.0 -	— 15									Gravel layer @ 14'.
	17.00									
		F	SPT	23 54	50/5"	76				(F) Rock in sampler shoe.
	18.40			50/5"						'
	-									
4723.0 -	-20							SM		
	-									
	22.00			16						
	23.33	G	SPT	35 50/4"	50/4"	94				
	-									
4718.0 -	—25									
	-									
	27.00									
	27.75	Н	SPT	36 50/3"	50/3"	100			<u>SILTY SAND</u> fine, dry, yellowish brown (10 YR 5/4), very dense	



7/1/02 START DATE

7/2/02

END DATE **CARSON FREEWAY** JOB DESCRIPTION

LOCATION

CLEARVIEW DRIVE GRADE SEPARATION

**BORING** 

E.A.#

CV-1 72781 **GROUNDWATER LEVEL** DATE | DEPTH ft | ELEV. ft

**EXPLORATION LOG** 

"CV"16+51 STATION

43' Right OFFSET

**ENGINEER** 

**BOOMHOWER** MOBILE B-80

SHEET 2 OF 3

**EQUIPMENT ALTAMIRANO OPERATOR** 

DRILLING METHOD Wet w/ Bentonite Slurry

GEOTECI ENGINI	HNICAL			ROUND ELE		_	AFETY		7/8/02 56.10 4686.9 9/3/02 72.50 4670.5 BACKFILLED	ATE
ELEV.	DEPTH		MPLE	BLOW Co 6 inch Increments	OUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
(ft)	(ft)	NO.	ITFE	Increments	1 foot	Recov'd		Group	SILTY SAND fine, dry, very dense, partially	
	_								cemented	
	32.00			19						
	33.50	I	SPT	31 32	63	83				
	-							-		
4708.0 -	-35									
	-									
	37.00			25				SM		
	38.40	J	SPT	25 46	50/5"	100				
	36.40			50/5"						
4703.0 -	40									
4703.0	40									
									43.00	
	_							CL	43.50 <u>CLAY</u>	Clay layer fror 43' to 43.5'.
	_								SILTY CLAYEY SAND fine, dry, yellowish brown (10 YR 5/4), very dense	43 (0 43.5 .
4698.0 -	<del>-</del> 45									
	47.00			23						
	48.50	K	CMS	31 34	65	89				
										End day 1 @ 48.5'
4693.0 -	-50									
	_									
								SC SM		
	_									
4688.0 -	55									
	¥ ¥									
=	57.00									
		L	SPT	27 40	50/3"	100				(L) Rock in sampler shoe.
	- 58.25			50/3"						
	F							1	I	1



7/1/02 START DATE

7/2/02 END DATE

**CARSON FREEWAY** JOB DESCRIPTION

**CLEARVIEW DRIVE GRADE SEPARATION** LOCATION

CV-1 **BORING** 72781 E.A.#

#### **EXPLORATION LOG**

**GROUNDWATER LEVEL** 

DATE | DEPTH ft | ELEV. ft

SHEET 3 OF 3

"CV"16+51 STATION

**EQUIPMENT** 

43' Right OFFSET **BOOMHOWER ENGINEER** 

MOBILE B-80

**ALTAMIRANO OPERATOR** DRILLING METHOD Wet w/ Bentonite Slurry

	GROUND ELEV. 4743.03 (ft)								T/8/02 56.10 4686.9 DRILLING METHOD Wet w/ Bentonite Slurry
GEOTEC ENGIN	HNICAL IEERING			AMMER DR			AFETY	[	9/3/02 72.50 4670.5 BACKFILLED DATE
ELEV. (ft)	DEPTH (ft)	SAI NO.	MPLE TYPE	BLOW C 6 inch Increments	OUNT	Percent	LAB TESTS	USCS Group	MATERIAL DESCRIPTION REMARKS
(it)	-			Increments	11000	Recova		SC SM	SILTY CLAYEY SAND fine, dry, yellowish brown (10 YR 5/4), very dense
4678.0									
	68.50	М	SPT	17 30 60	90	100		SC	CLAYEY SAND medium to coarse, yellowish brown (10 YR 5/4), very dense (M) Rock in sampler shoe.
4673.0	<b>70</b>								
	<u>*</u>								72.50
4668.0	75								
	77.00	N	SPT	19 32 50	82	100			SILTY SAND fine to medium, dry, yellowish brown (10 YR 5/4), very dense
4663.0	- 80							SM	Gravel and cobbles @ 79' to 80.5'; hard drilling.
	_								Hard drilling froi 82' to 83.5'.
4658.0	<del>-</del> 85								
	87.00	0	SPT	27 32	87	100			SILTY SAND fine to medium, dry, yellowish brown (10 YR 5/4), very dense, some gravel
	88.50			55					88.50 Flushed hole wi clean water.



END DATE 7/3/02

JOB DESCRIPTION CARSON FREEWAY

LOCATION CLEARVIEW DRIVE GRADE SEPARATION
BORING CV-2

E.A.# 72781

GROUND ELEV. 4736.95 (ft)

HAMMER DROP SYSTEM AUTOMATIC

**EXPLORATION LOG** 

**GROUNDWATER LEVEL** 

DATE DEPTH ft ELEV. ft

OFFSET 50' Right

ENGINEER BOOMHOWER
EQUIPMENT MOBILE B-57

OPERATOR ALTAMIRANO

DRILLING 6" H.S. AUGER

BACKFILLED Yes DATE 7/3/2002

SHEET 1 OF 2

ELEV. (ft)	DEPTH (ft)		MPLE TYPE	C:	Last	Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
	1.00								SILTY SAND dry, very pale brown (10 YR 7/4), with scrub brush	
		^	ח וו וכ			100			That out an order	
	2.50	А	BULK			100		SM		
	3.00									
		В	CMS	8 14	42	100			4.00	
	4.50		Oivio	28	72	100			SILTY CLAYEY SAND dry to damp, yellowish	•
4732.0 -	-5	С	SPT	16 38	25/2"	100		00	brown (10 YR 5/4), very dense, lightly cemented	
	5.70			25/2"				SC SM		
	-							<u></u>	7.00 SILTY SAND dry to damp, yellowish brown (10	Quartz gravel.
	8.00								YR 5/4), very dense, lightly cemented	gaa. = g.a. o
	8.90	D	CMS	43 50/5"	50/5"	91				
	-			50/5				SM		
4727.0 -	10									
									11.00	
									CLAYEY SAND yellowish brown (10 YR 5/4),	
	-								very dense	
	13.00									
		Е	SPT	49 45	84	100				
	14.50	_	01 1	39	04	100				
4722.0 -	<b>—</b> 15									End day 1 @ 14.5'.
	_									11.0.
	19.00									
	18.00	F	CMS	62	50/3"	100		00	CLAYEY SAND with gravel, light reddish brown	
	18.80	'	CIVIO	50/3"	30/3	100		SC	(5 YR 6/4), very dense	
4717.0 -	-20									
	23.00			12						
		G	SPT	43 58	128	100			<u>CLAYEY SAND</u> with gravel, dry, light reddish brown (5 YR 6/4), very dense, cemented	
	24.50			70		100			( 2. 7, 12.) 22.103, 65.104.105	
4712.0 -	25									
									26.00	
									SILTY CLAYEY SAND light reddish brown (5 YR 6/4), very dense	
	28.00							sc		Very hard drillir @ 27'.
				28				SM		
	29.50	Н	SPT	48 70	118	89				
	29.50			10				1	30.00	



START DATE	7/2/02

END DATE 7/3/02

JOB DESCRIPTION CARSON FREEWAY

LOCATION

CLEARVIEW DRIVE GRADE SEPARATION

BORING E.A.# 72781

GROUND ELEV. 4736.95 (ft)

HAMMER DROP SYSTEM AUTOMATIC

**EXPLORATION LOG** 

**GROUNDWATER LEVEL** 

DATE DEPTH ft ELEV. ft

**EQUIPMENT** 

**OPERATOR** 

OFFSET 50' Right

ENGINEER BOOMHOWER

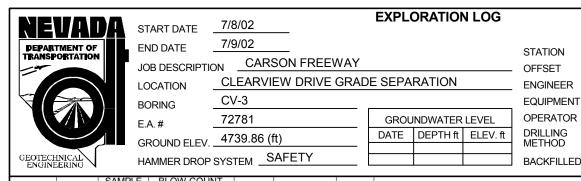
MOBILE B-57 ALTAMIRANO

SHEET 2 OF 2

DRILLING 6" H.S. AUGER

BACKFILLED Yes DATE 7/3/2002

ELEV. (ft)	DEPTH (ft)	SAI NO.	MPLE TYPE	BLOW Co 6 inch Increments	OUNT Last 1 foot	Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
4702.0 -	- - - - 35.00	)		18				sc	CLAYEY SAND with gravel, dry, light reddish brown (5 YR 6/4), very dense, cemented	Very hard drilling @ 31'.
	36.50	I	SPT	23 37	60	100				Very hard drilling @ 37'.
4697.0 -	- - - -								40.00 B.O.H.	Auger vibrating severely; terminate drilling.
4692.0 -	- - - 45 -									
4687.0 -	50									
NV DOI CLERVIEW.GPJ NV DOI GDI 10/6/06  9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- - - - -									



	GEOTECHNICAL HAMMER DROP SYSTEM SAFETY  ELEV DEDTH SAMPLE BLOW COUNT 1 1988								
ELEV. [	DEPTH (ft)	NO.	TYPE	6 inch Increments	Last 1 foot	Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION REMARKS
-								SM	SILTY SAND dry, with scrub brush
4734.9	-5 7.00 7.90	A	SPT	17 50/5"	50/5"	91		sc	<u>CLAYEY SAND</u> dry, light reddish brown to yellowish brown (5 YR 6/4 to 10 YR 5/4), lightly
4729.9	-10								cemented  12.50 SILTY CLAYEY SAND
4724.9	-15 17.00			16					
4719.9	18.50 -20	В	SPT	32 56	88	89		SC SM	
-									23.00 SANDY LEAN CLAY damp, yellowish red (5 YR 5/6)
4714.9	- <b>25</b> 27.00			10				CL	
-	28.50 29.30	C	CMS	13 21 56 40 50/4"	77 50/4"	100 90		sc	27.80  CLAYEY SAND damp, reddish brown (5 YR 5/4), very dense

SHEET 1 OF 4

"CV"15+83

**BOOMHOWER** 

Wet w/ Bentonite Slurry

MOBILE B-80

MARSHALL

44' Right



END DATE 7/9/02

JOB DESCRIPTION CARSON FREEWAY

LOCATION CV-3

CLEARVIEW DRIVE GRADE SEPARATION

BORING CV-3 E.A.# 72781

GROUND ELEV. 4739.86 (ft)

HAMMER DROP SYSTEM SAFETY

#### **EXPLORATION LOG**

**GROUNDWATER LEVEL** 

DATE DEPTH ft ELEV. ft

SHEET 2 OF 4

OFFSET 44' Right

ENGINEER BOOMHOWER
EQUIPMENT MOBILE B-80

OPERATOR MARSHALL

DRILLING METHOD Wet w/ Bentonite Slurry

BACKFILLED \_\_\_\_\_ DATE \_

ELEV.	DEPTH		MPLE TYPE	BLOW CO 6 inch Increments	Last	Percent	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
(ft)	(ft)	NO.	ITPE	Increments	1 foot	Recov'd		Group	SILTY SAND medium to coarse, yellowish brown	
	_								(10 YR 5/4)	
	32.00									
	32.80	Е	CMS	56 50/4"	50/4"	100				
	-									
4704.9 -	-35									
	-									
	37.00									
	20.20	F	SPT	38 54	50/4"	92				
	38.30			50/4"				1		
4699.9 -	<del>-4</del> 0									
	-									
	42.00			10				_	OU TV CAND with ODANE! we dissue to account	
		G	SPT	19 38	88	100		SM	SILTY SAND with GRAVEL medium to coarse	
	43.50			50						
4694.9 -	<del></del> 45									
	-									
	47.00			22				-	SILTY SAND dry, medium to coarse, yellowish	
	40.50	Н	SPT	34	74	100			brown (10 YR 5/4)	
	48.50			40						
4689.9 -	<b>—50</b>									
	52.00	1	SPT	34	50/5"	100		-	SILTY SAND damp, fine to medium, yellowish brown (10 YR 5/4)	
	52.90	'	SF I	50/5"	30/3	100			brown (10 YR 5/4)	
	_									
4684.9 -	—55								55.00	
	55								CLAYEY SAND moist, fine to medium, yellowish red (5 YR 5/6)	
	F7.00								,	
	57.00			18				SC		
	58.50	J	SPT	34 43	77	100				
	-							1		End day 1 @
									60.00	58.5'.



START DATE

7/8/02

7/9/02

END DATE **CARSON FREEWAY** JOB DESCRIPTION

SAFETY

**CLEARVIEW DRIVE GRADE SEPARATION** LOCATION

CV-3 **BORING** 72781 E.A. #

4739.86 (ft) GROUND ELEV. HAMMER DROP SYSTEM .

**GROUNDWATER LEVEL** DATE | DEPTH ft | ELEV. ft

**EXPLORATION LOG** 

"CV"15+83 STATION

**EQUIPMENT** 

**OPERATOR** 

44' Right OFFSET **BOOMHOWER ENGINEER** 

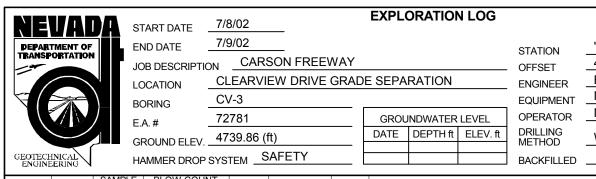
MOBILE B-80 MARSHALL

DRILLING METHOD Wet w/ Bentonite Slurry

SHEET 3 OF 4

BACKFILLED DATE

ELEV.	DEPTH	SAN	MPLE	BLOW CO	JUNT	Percent	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
(ft)	(ft)	NO.	TYPE	BLOW CO 6 inch Increments	1 foot	Percent Recov'd	L.D ILOIO	Group	WATENAL DESCRIPTION	KLWAKKS
	62.00			10					CLAVEY SAND damp, vollowich rod (5 VD 5/6)	
		K	CMS	18 27	66	89			<u>CLAYEY SAND</u> damp, yellowish red (5 YR 5/6), very dense	
	63.50			39					,	
4674.9 -	<del></del> 65									
	_									
	67.00									
	67.00			25					CLAYEY SAND damp, yellowish red (5 YR 5/6),	
		L	SPT	49	104	94			very dense	
	68.50			55						
	_									
4660.0										
4669.9 -	_/0									
	_									
	72.00									
	. 2.00			22						
		М	SPT	42	92	100				
	73.50			50						
	_									
4664.9 -	<b>-75</b>									
.000										
	_							sc		
	77.00									
			ОРТ	24	70	400			CLAYEY SAND damp, yellowish red (5 YR 5/6),	
		N	SPT	28 44	72	100			very dense	
	70.50			77						
	_									
4659.9 -	<b>–</b> 80									
	82.00			20						
		0	SPT	22 34	84	100				
	83.50	Ĺ		50						
1654.9 -	<del>-</del> 85									
	_									
	97.00									
	87.00			24					CLAYEY SAND moist, yellowish red (5 YR 5/6),	
		Р	CMS	34	78	100			very dense, some gravel	
	88.50			44						
	-									
									90.00	

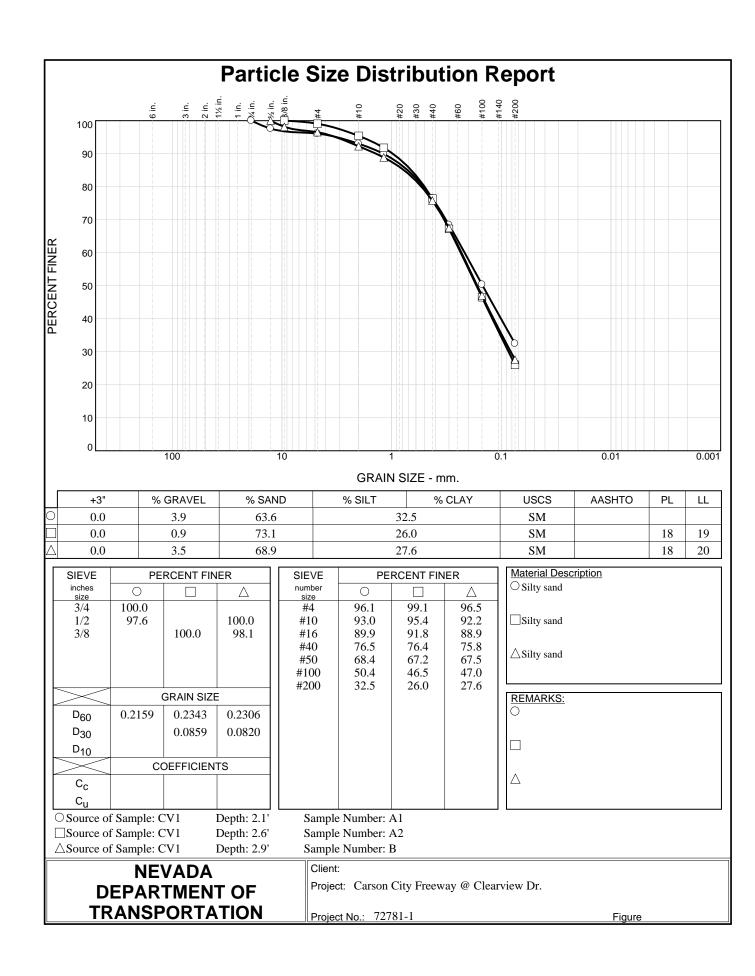


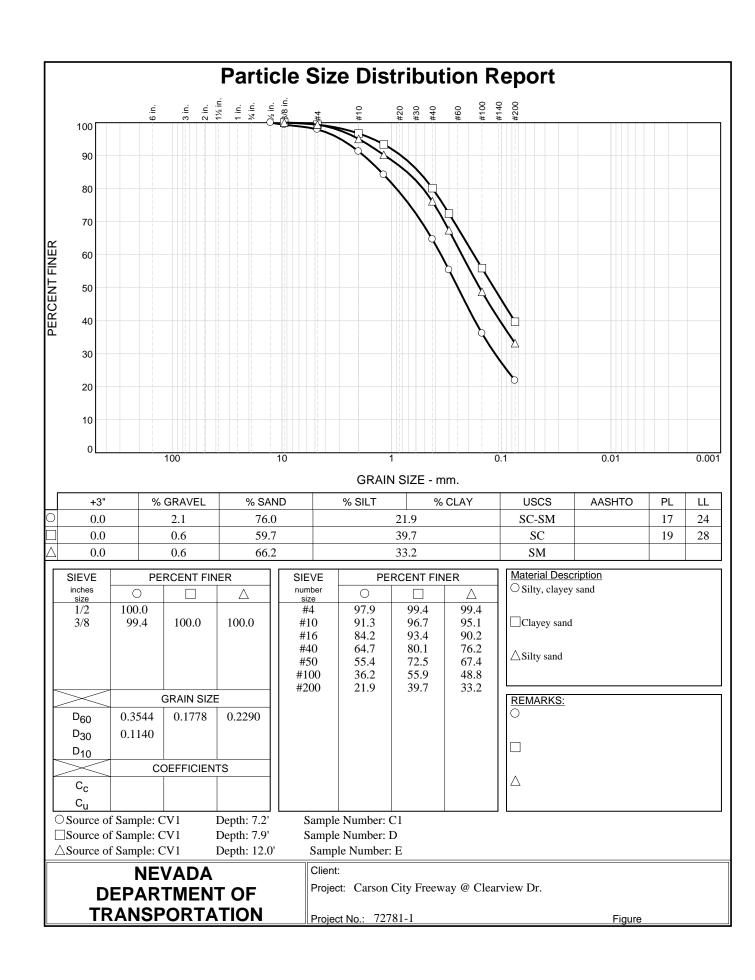
			STATION	"CV"15+83		
			OFFSET	44' Right		
E SEPA	RATION		ENGINEER	BOOMHOWER		
			EQUIPMENT	MOBILE B-80		
GROU	INDWATER	I EVEI	OPERATOR	MARSHALL		
DATE	DEPTH ft		DRILLING	Wet w/ Bentonite Slurry		
			METHOD	Wet W/ Bentonite Glarry		
			BACKFILLED	DATE		

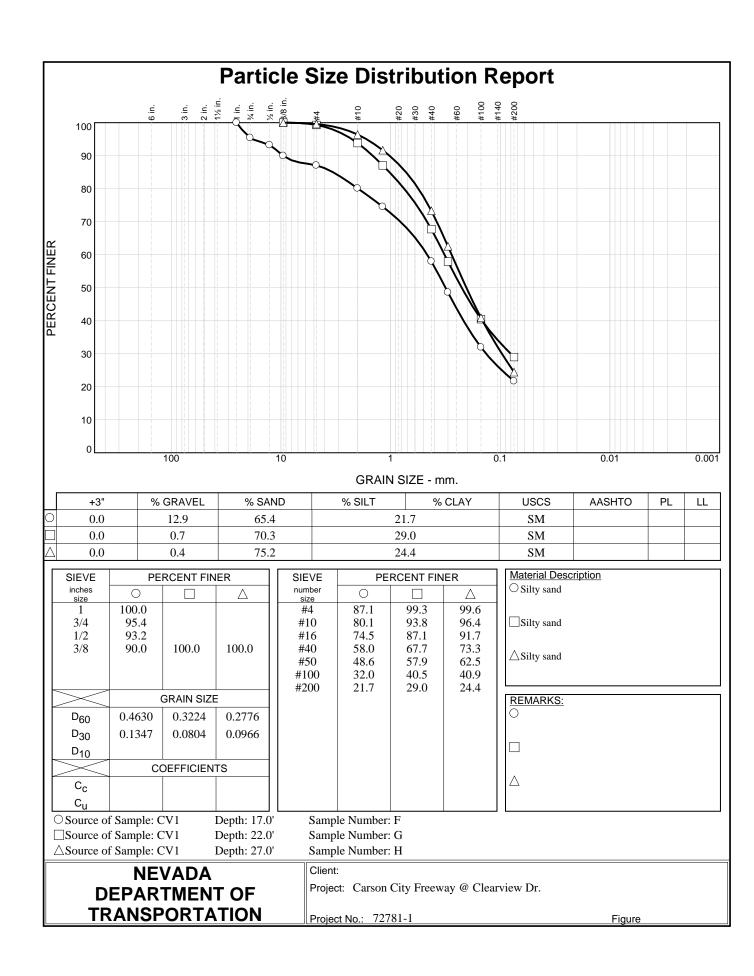
SHEET 4 OF 4

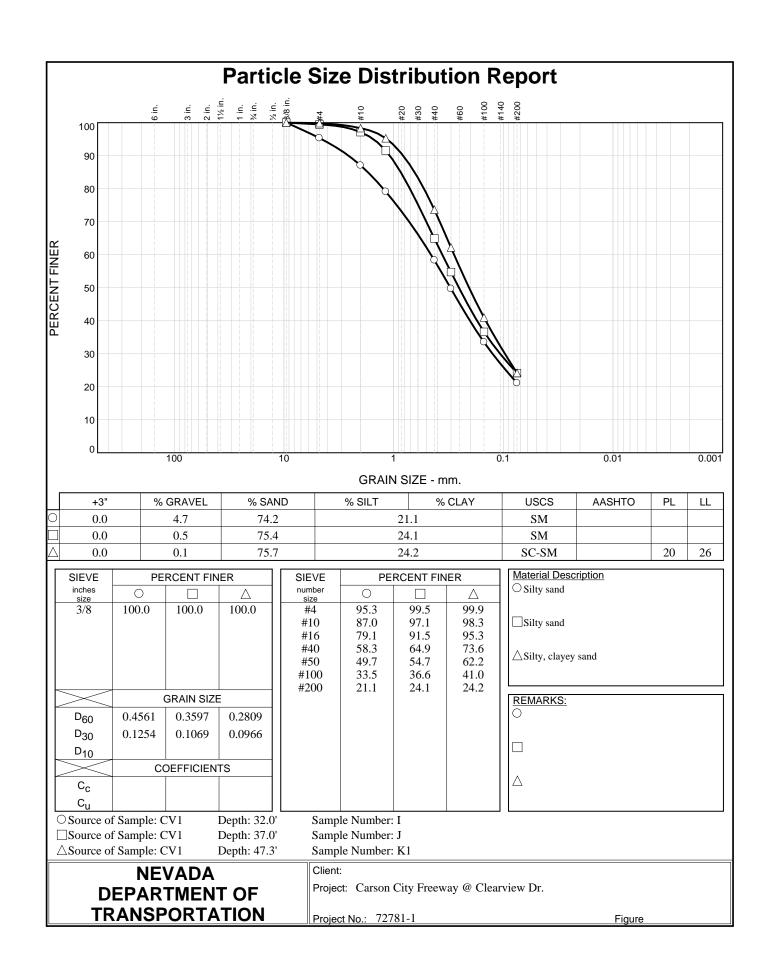
ELEV.	DEPTH (ft)	SAN NO.	MPLE TYPE	BLOW Co 6 inch Increments	OUNT Last 1 foot	Percent	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
(11)	(II)			increments	1 1001	Recov'd		Стопр	CLAYEY SAND damp, yellowish red (5 YR 5/6), very dense	
	92.00									
	93.30	Q	SPT	25 30	50/4"	100				
	- 00.00			50/4"				SC		
4644.9	<b>—</b> 95									
	-							<u> </u>	97.00  POORLY GRADED GRAVEL very dense, yellowish red to brownish yellow (5 YR 5/6 to 10	
	-								yellowish red to brownish yellow (5 YR 5/6 to 10 YR 6/6)	
	-									
4639.9	100									
	182.00									Hard drilling @ 101'
	102:25	R	SPT	50/3"	50/3"	67		GP		
4634.9	— 105									
	-									
	-								107.00	_
	-									
	-									Very hard drilling @ 109' to 112'.
4629.9	110									@ 109' to 112'.
	112.00									
3	112.00							_		(s) No recovery.
4624.9	— —115	s	RC			0				
2										
	-									
L L	118.00								118.00	
4624.9 ·	-								В.О.Н.	

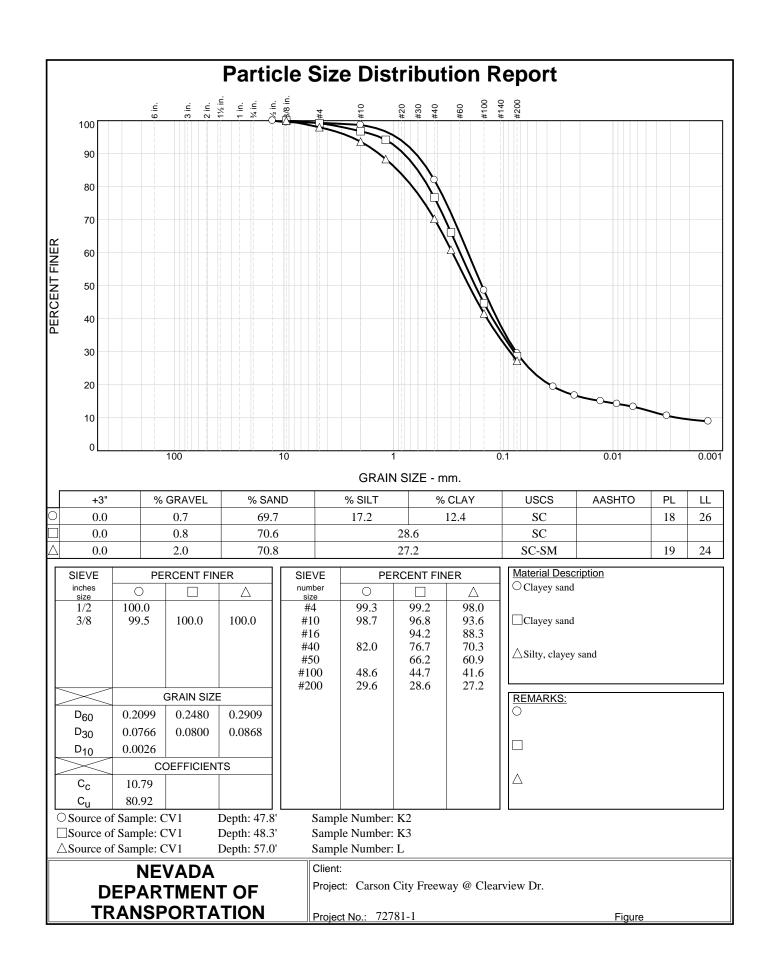
## APPENDIX C

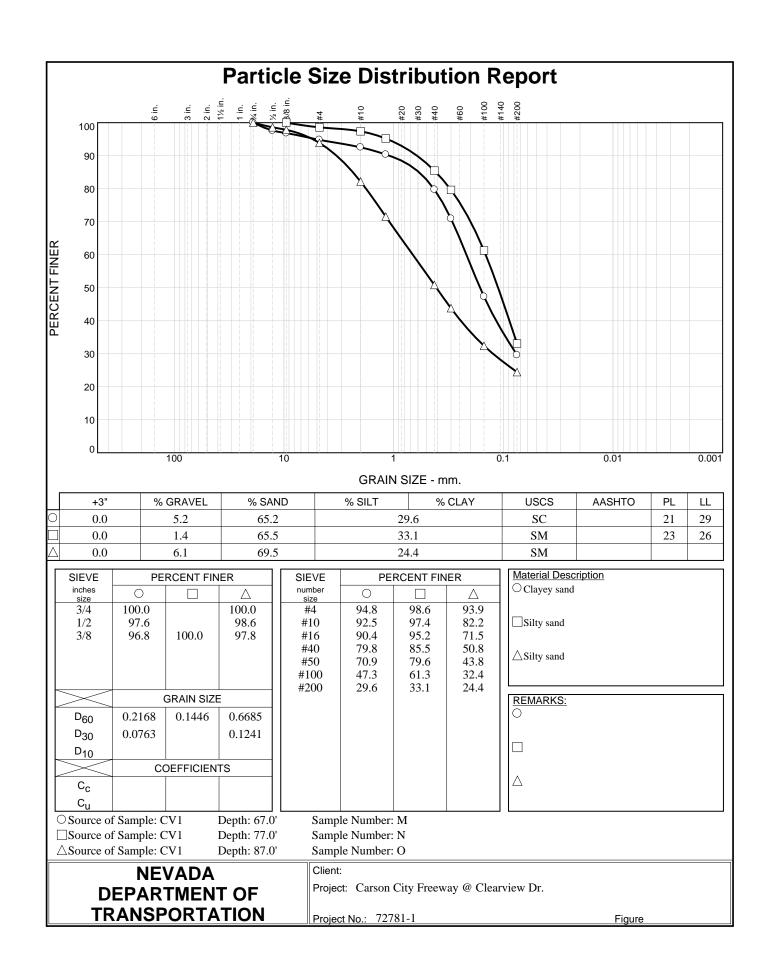


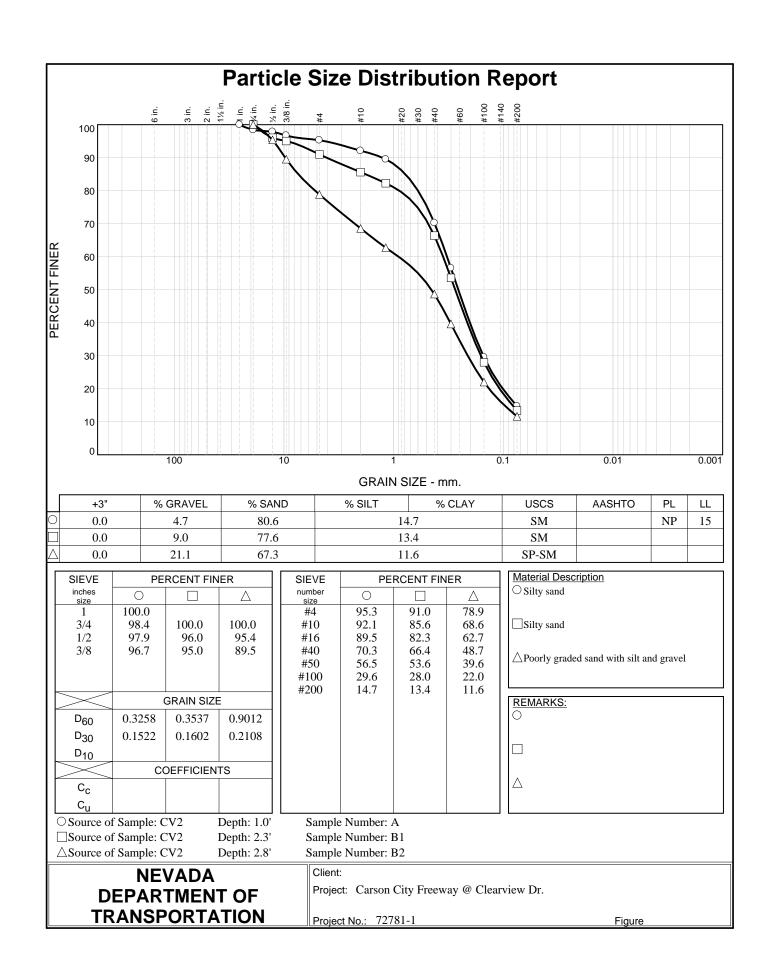


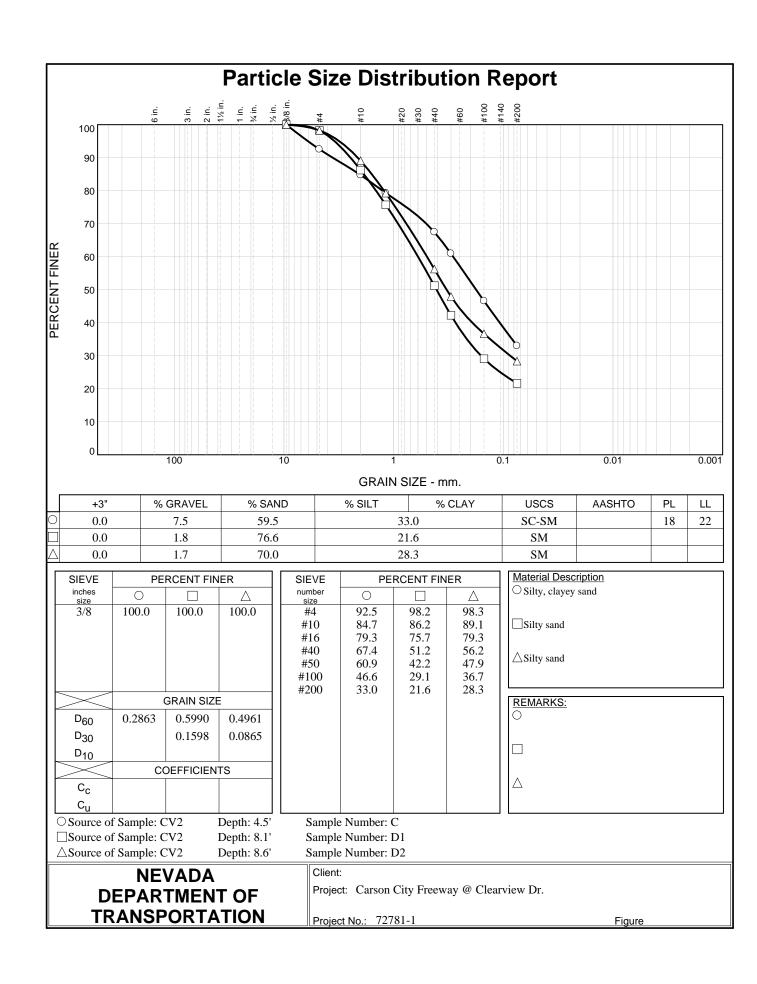


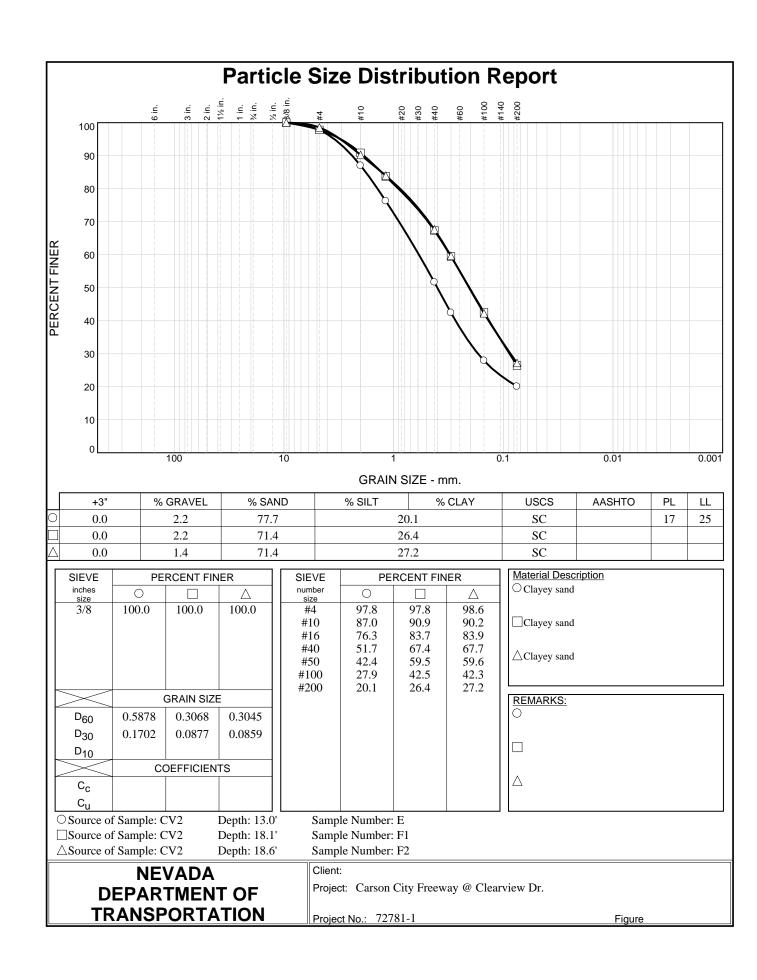


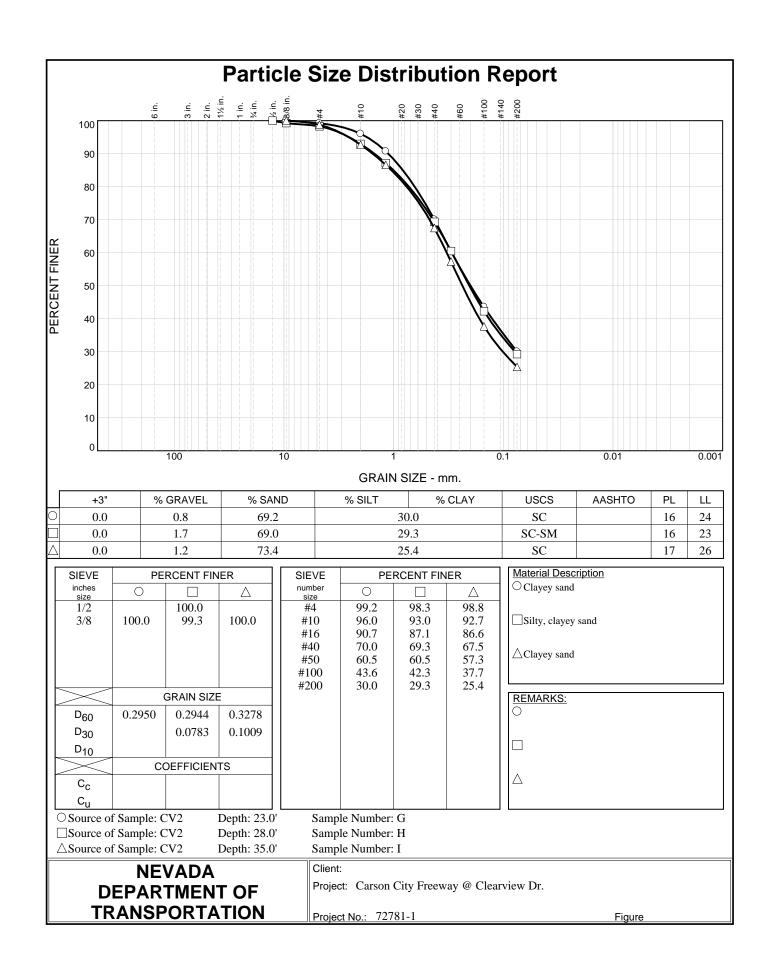


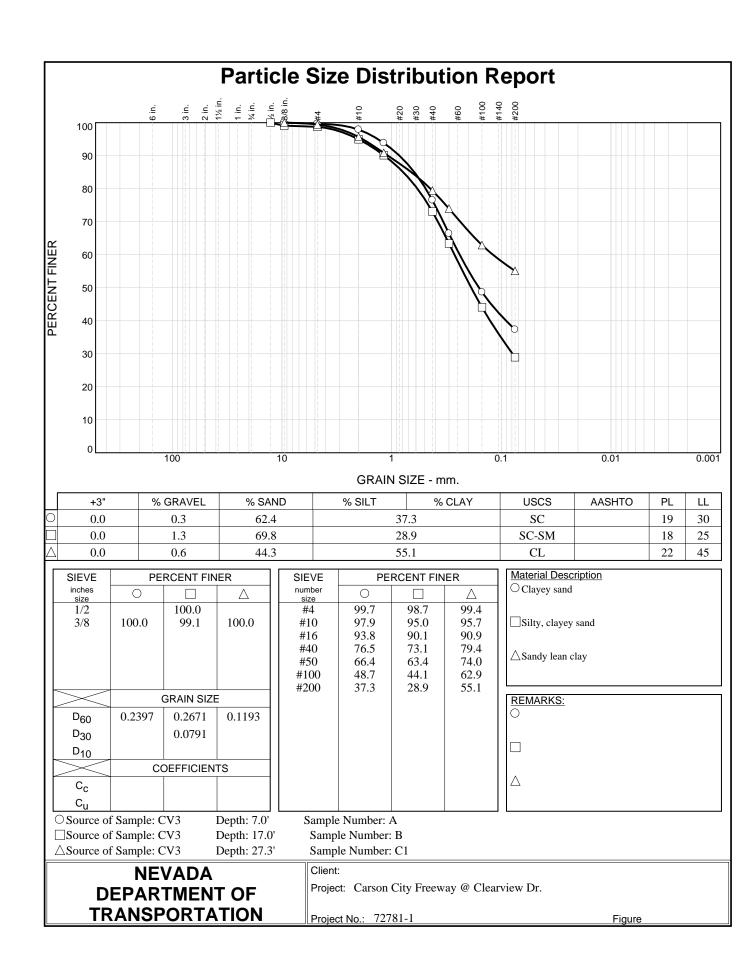


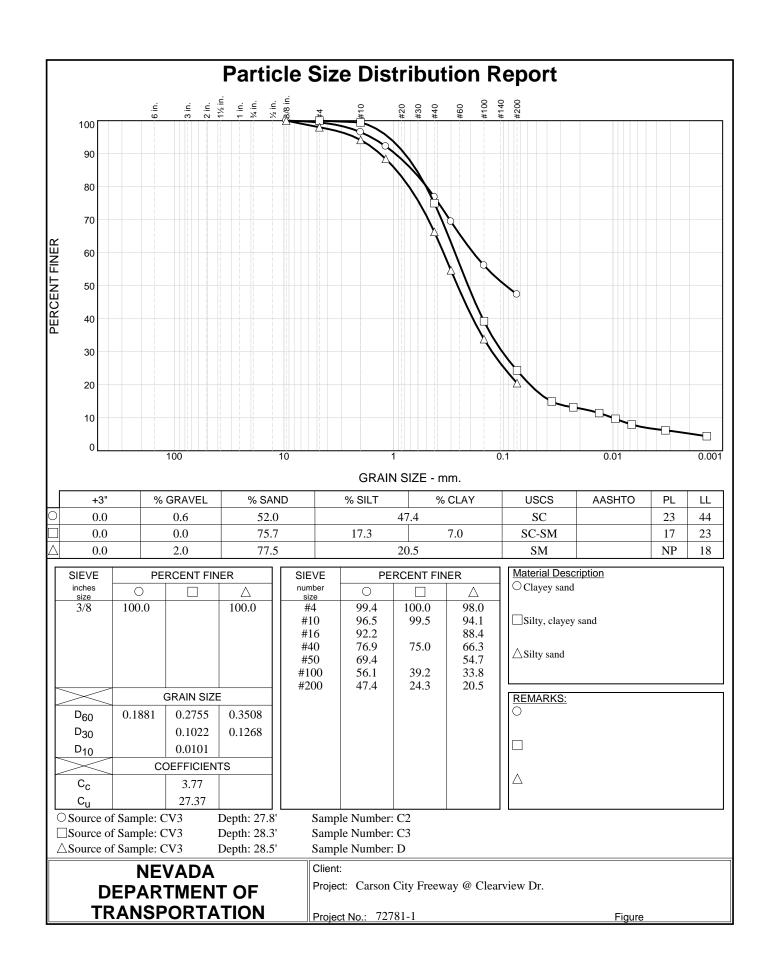


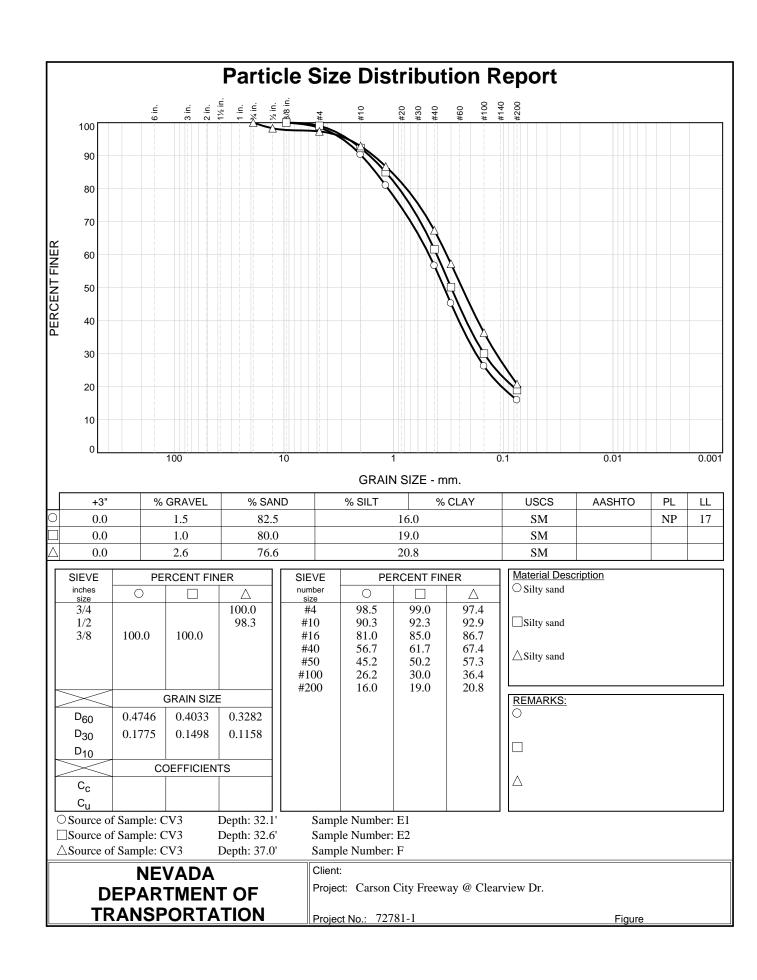


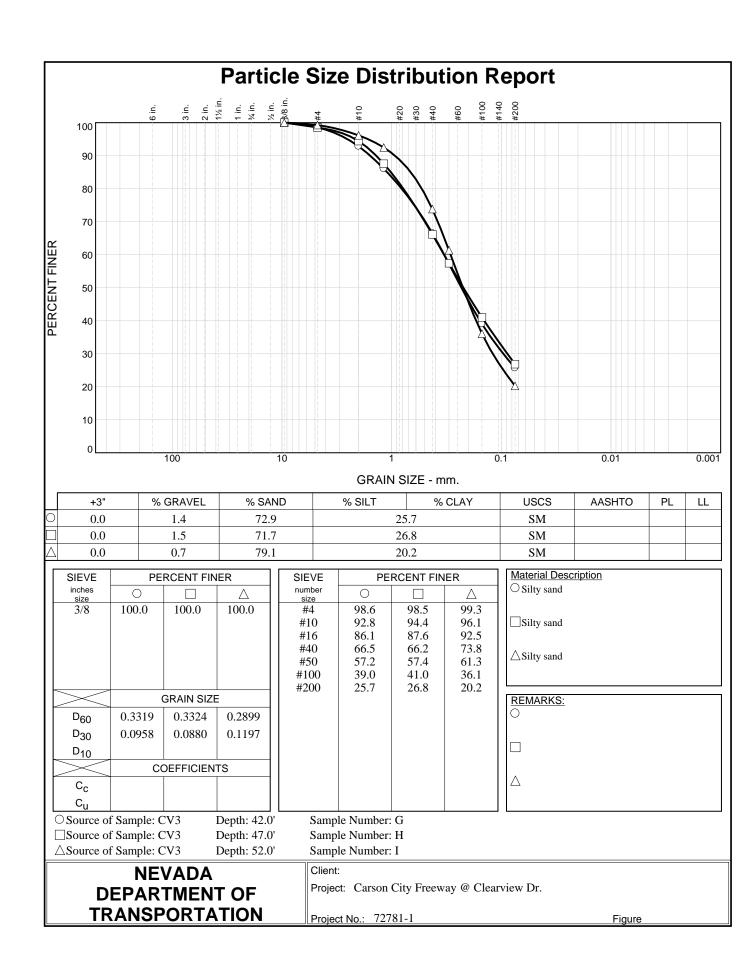


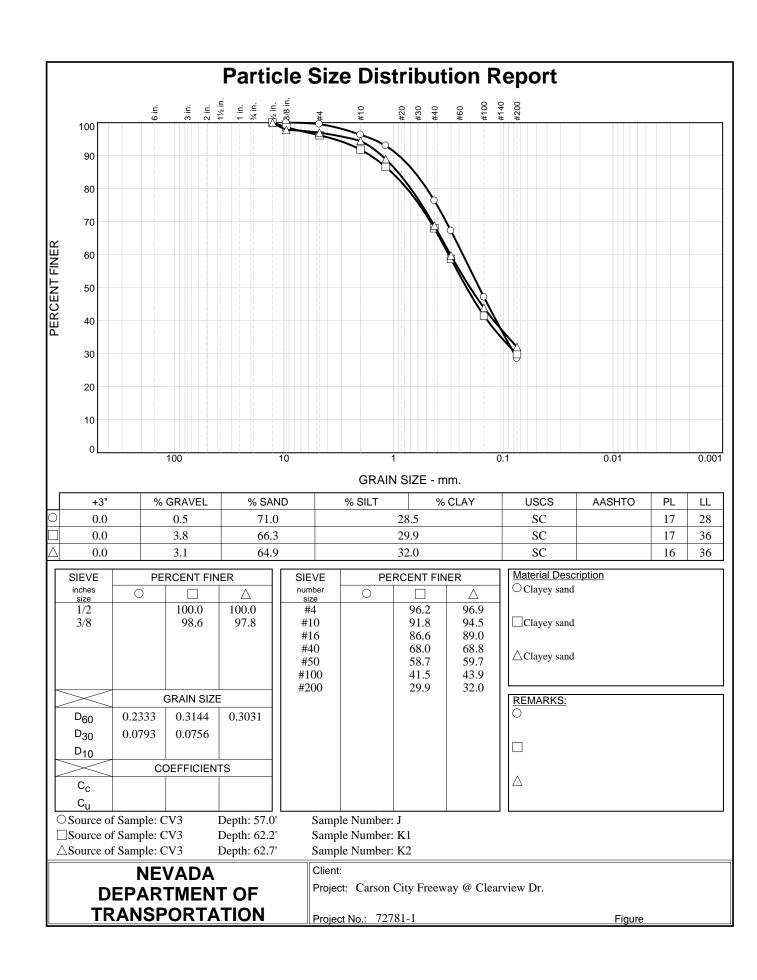


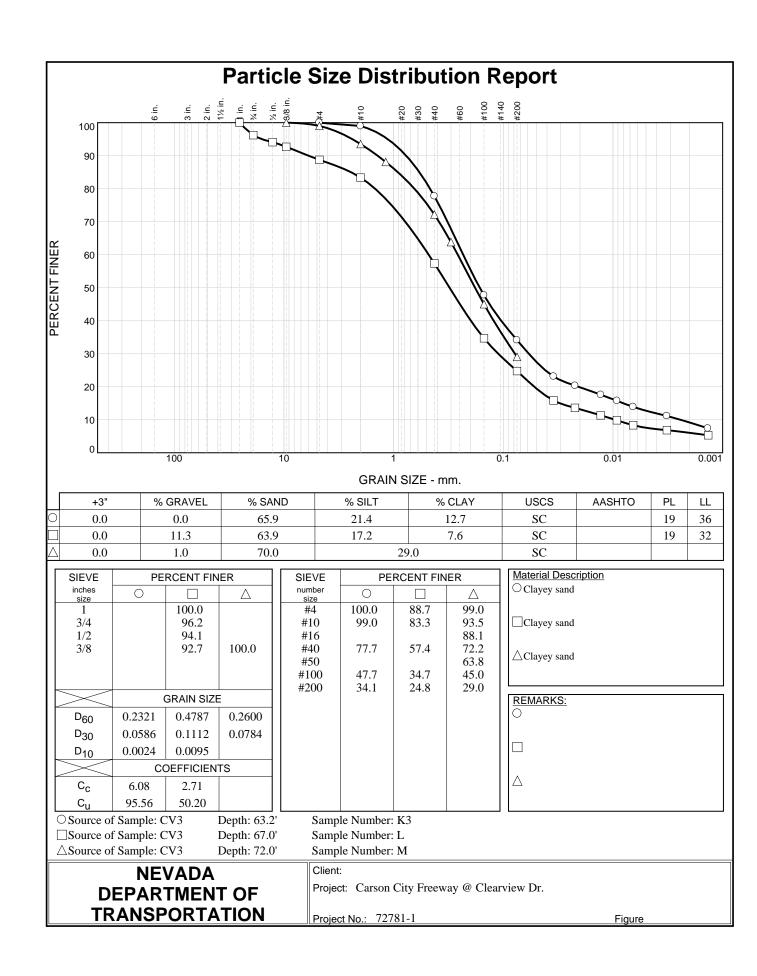


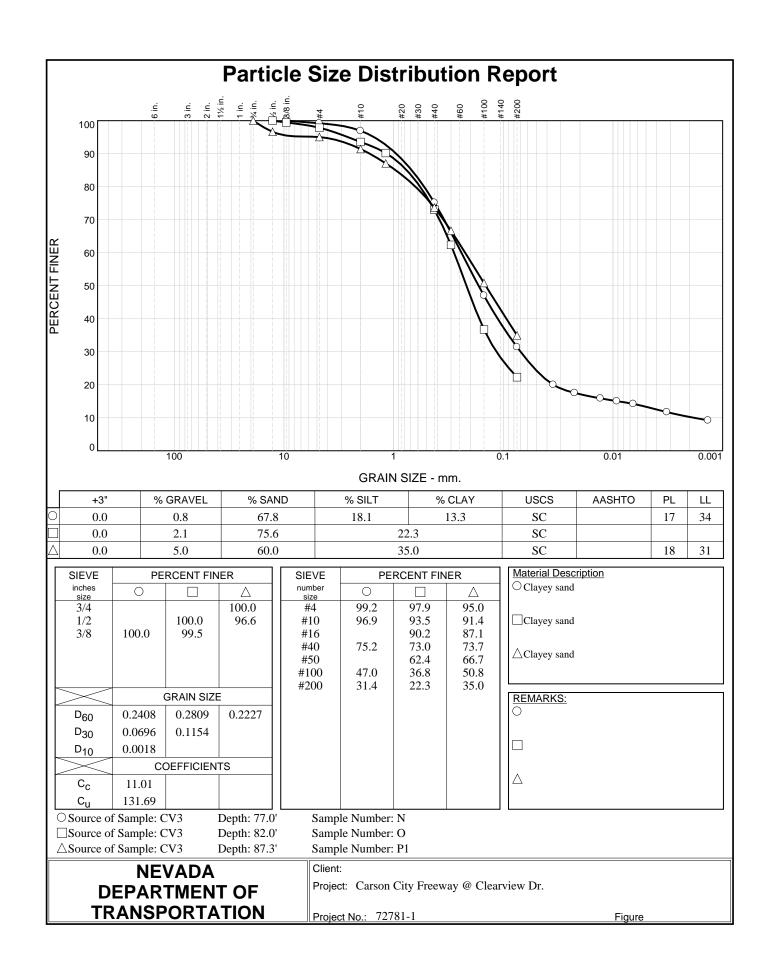


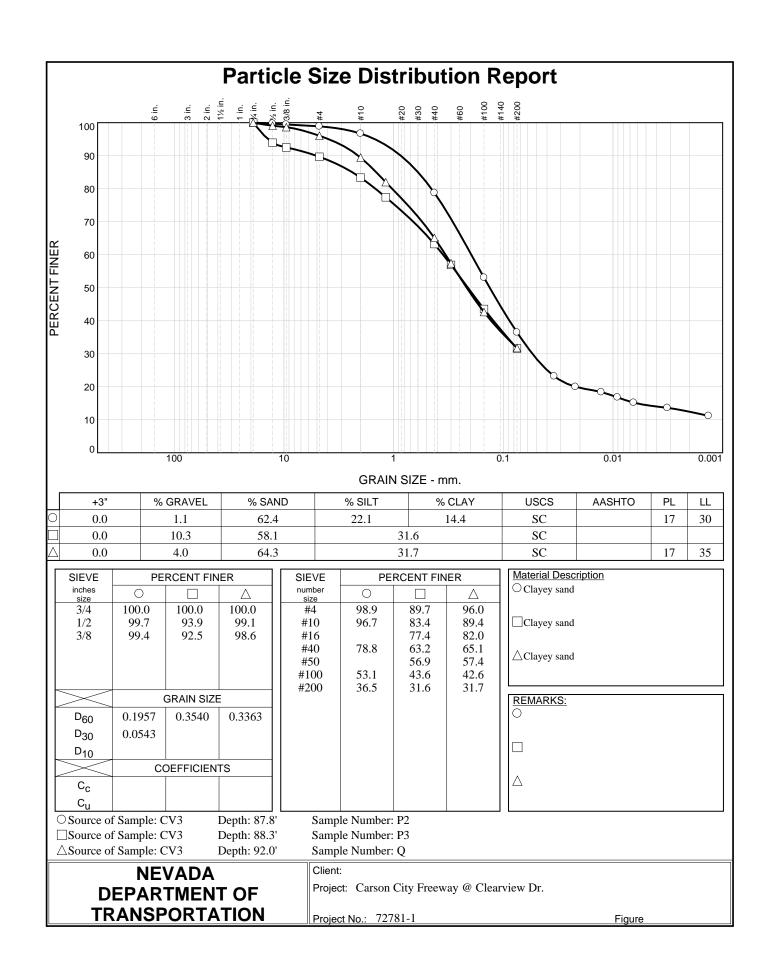












**EA/Cont #** 72781-1

Job Description Carson City Freeway @ Clearview Dr.

Boring No. CV1

**Elevation (ft)** 4743.03'

Station "CV" 16+51 43' RT.

	SAMPLE	SAMP-	N			DRY	%					STF	RENGTH T	EST		
SAMPLE	DEPTH	LER	BLOWS	SOIL	W%	UW	PASS	LL	PL	PI	TEST	φ	C	φ	C	OTHERS
NO.	(ft)	TYPE	per ft.	GROUP		pcf	#200	%	%	%	TYPE	deg.	psi eak	deg.	psi idual	
<u> </u>												ГС	an	1762	luuai	
A1	2.1 - 2.6	CMS		SM	6.7	123.6	32.5									
A2	2.6 - 2.9	CMS		SM			26.0	19	18	1						
В	2.9 - 3.8	SPT		SM			27.6	20	18	2						
C1	7.2 - 7.7	CMS		SC-SM	8.58*	113.25*	21.9*	24*	17*	7*	DS	37	4.26	37	-0.07	
a	1.1"															
b	1.1"				7.6	113.3										
С	1.1"				8.2	112.3										
d	1.1"				9.2	111.9										
e	1.42"				9.3	115.5										
C2	7.7 - 7.9	CMS						26	19	7						
D	7.9 - 8.7	SPT		sc			39.7	28	19	9						
Е	12.0 - 13.25+B45	SPT		SM			33.2									

CMS = California Modified Sampler 61mm ID

SPT = Standard Penetration 35mm ID

CS = Continuous Sample 82mm ID

RC = Rock Core

PB = Pitcher Barrel

CSS = Calif. Split Spoon 61.5mm ID

CPT = Cone Penetration Test

TP = Test Pit

P = Pushed, not driven

R = Refusal

Sh = Shelby Tube 73 mm ID

U = Unconfined Compressive

UU = Unconsolidated Undrained

CD = Consolidated Drained

CU = Consolidated Undrained

DS = Direct Shear

Φ = Friction C = Cohesion

N = No. of blows per 0.3m, sampler

N = Field SPT  $N = (N_{css})(0.62)$ 

H = Hydrometer

S = Sieve

G = Specific Gravity

PI = Plasticity Index LL = Liquid Limit

LL = Liquid Limit PL = Plastic Limit

NP = Non-Plastic
OC = Consolidation

Ch = Chemical RV = R - Value

MD = Moisture Density

CM = Compaction

E = Swell/Pressure on Expansive Soils

SL = Shrinkage Limit UW= Unit Weight W = Moisture Content

K = PermeabilityO = Organic ContentD = Dispersive

RQD = Rock Quality Designation

X = X-Ray Defraction

<sup>\* =</sup> Average of subsamples

EA/Cont # 72781-1 Job Description Carson City Freeway @ Clearview Dr.

**Boring No.** CV1 Elevation (ft) Station

	SAMPLE	SAMP-	N			DRY	%					STI	RENGTH T	EST		
SAMPLE	DEPTH	LER	BLOWS	SOIL	W%	UW	PASS	LL	PL	PI	TEST	φ	C	φ	С	OTHERS
NO.	(ft)	TYPE	pcf	GROUP		pcf	#200	%	%	%	TYPE	deg.	psi	deg.	psi	
												PE	ak	Res	idual	
F	17.0 - 18.4	SPT		SM			21.7									
G	22.0 - 23.3	SPT		SM			29.0									
Н	27.0 - 27.75	SPT		SM			24.4									
I	32.0 - 33.5	SPT		SM			21.1									
J	37.0 - 38.4	SPT		SM			24.1									
K1	47.3 - 47.8	CMS		SC-SM	10.25*	116.33*	24.2*	26*	20*	6*	DS	36	5.69	32	1.8	
a	1.15"				10.8	114.7										
ь	1.15"				10.6	116.3										
С	1.15"				10.2	117.2										
d	2.55"				9.4	117.1										
K2	47.8 - 48.3	CMS		SC	9.7	120.8	29.6	26	18	8						
K3	48.3 - 48.5	CMS		SC			28.6									

CMS = California Modified Sampler 61mm ID

SPT = Standard Penetration 35mm ID

CS = Continuous Sample 82mm ID

RC = Rock Core

PB = Pitcher Barrel

CSS = Calif. Split Spoon 61.5mm ID

CPT = Cone Penetration Test

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DS = Direct Shear

 Friction C = Cohesion

N = No. of blows per 0.3m, sampler

N = Field SPT  $N = (N_{css})(0.62)$ 

\* = Average of subsamples

H = Hydrometer

S = Sieve

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O = Organic Content D = Dispersive

RQD = Rock Quality Designation

X = X-Ray Defraction

EA/Cont # 72781-1 Job Description Carson City Freeway @ Clearview Dr.

**Boring No.** CV1 Elevation (ft) Station

	SAMPLE	SAMP-	N			DRY	%					STI	RENGTH T	EST		
SAMPLE	DEPTH	LER	BLOWS		W%	UW	PASS	LL	PL	PI	TEST	φ	C	φ	C	OTHERS
NO.	(ft)	TYPE	ft	GROUP		pcf	#200	%	%	%	TYPE	deg.	psi	deg.	psi	
												Pe	eak	Res	idual	
L	57.0 - 58.25	SPT		SC-SM			27.2	24	19	5						
M	67.0 - 68.5	SPT		SC			29.6	29	21	8						
N	77.0 - 78.5	SPT		SM			33.1	26	23	3						
О	87.0 - 88.5	SPT		SM			24.4									

CMS = California Modified Sampler 61mm ID

SPT = Standard Penetration 35mm ID

CS = Continuous Sample 82mm ID

RC = Rock Core

PB = Pitcher Barrel

CSS = Calif. Split Spoon 61.5mm ID

CPT = Cone Penetration Test

TP = Test Pit

P = Pushed, not driven

R = Refusal

Sh = Shelby Tube 73 mm ID

U = Unconfined Compressive

UU = Unconsolidated Undrained

CD = Consolidated Drained

CU = Consolidated Undrained

DS = Direct Shear

Friction

C = Cohesion

N = No. of blows per 0.3m, sampler

N = Field SPT  $N = (N_{css})(0.62)$ 

\* = Average of subsamples

H = Hydrometer

S = Sieve

G = Specific Gravity PI = Plasticity Index

LL = Liquid Limit

PL = Plastic Limit NP = Non-Plastic

OC = Consolidation

Ch = Chemical

RV = R - Value MD = Moisture Density CM = Compaction

E = Swell/Pressure on Expansive Soils

SL = Shrinkage Limit UW= Unit Weight W = Moisture Content

K = Permeability O = Organic Content

D = Dispersive

RQD = Rock Quality Designation

X = X-Ray Defraction

EA/Cont # 72781-1 Job Description Carson City Freeway @ Clearview Dr.

**Boring No.** CV2

Elevation (ft) 4736.95' Station "CV" 15+21 50' RT.

	SAMPLE	SAMP-	N			DRY	%					ST	RENGTH T			
SAMPLE	DEPTH	LER	BLOWS	SOIL	W%	UW	PASS	LL	PL	PI	TEST	φ	C	φ	C	OTHERS
NO.	(ft)	TYPE	ft	GROUP		pcf	#200	%	%	%	TYPE	deg.	psi eak	deg.	psi idual	
												PE	ak	Res	luuai	
Α	1.0 - 2.3	bulk		SM			14.7	15	NP	NP						Ch
B1	2.3 - 2.8	CMS		SM	3.2	114.9	13.4									
B2	2.8 - 3.3	CMS		SP-SM			11.6									
С	4.5 - 5.7	SPT		SC-SM			33.0	22	18	4						
D1	8.1 - 8.6	CMS		SM	5.5	109.1	21.6									
D2	8.6 - 8.9	CMS		SM			28.4									
Е	13.0 - 14.5	SPT		SC			20.1	25	17	8						
F1	18.1 - 18.6	CMS		SC			26.4									
F2	18.6 - 18.8	CMS		SC			27.2									
G	23.0 - 24.5	SPT		SC			30.0	24	16	8						
Н	28.0 - 29.5	SPT		SC-SM			29.3	23	16	7						
I	35.0 - 36.5	SPT		SC			25.4	26	17	9						

CMS = California Modified Sampler 61mm ID

SPT = Standard Penetration 35mm ID

CS = Continuous Sample 82mm ID

RC = Rock Core

PB = Pitcher Barrel

CSS = Calif. Split Spoon 61.5mm ID

CPT = Cone Penetration Test

TP = Test Pit

P = Pushed, not driven

R = Refusal

Sh = Shelby Tube 73 mm ID

U = Unconfined Compressive

UU = Unconsolidated Undrained

CD = Consolidated Drained

CU = Consolidated Undrained

DS = Direct Shear

 $\Phi$  = Friction

C = Cohesion

N = No. of blows per 0.3m, sampler

N = Field SPT  $N = (N_{css})(0.62)$  H = Hydrometer

S = Sieve

G = Specific Gravity

PI = Plasticity Index

LL = Liquid Limit PL = Plastic Limit

NP = Non-Plastic

OC = Consolidation

Ch = Chemical RV = R - Value

MD = Moisture Density

CM = Compaction

E = Swell/Pressure on Expansive Soils

SL = Shrinkage Limit UW= Unit Weight

W = Moisture Content K = Permeability

O = Organic Content

D = Dispersive

RQD = Rock Quality Designation

X = X-Ray Defraction

<sup>\* =</sup> Average of subsamples

EA/Cont # 72781-1 Job Description Carson City Freeway @ Clearview Dr.

**Boring No.** CV3 Elevation (ft) 4739.86' Station "CV" 15+83 44' RT.

	SAMPLE	SAMP-	N			DRY	%					STI	RENGTH T	EST		
SAMPLE	DEPTH	LER	BLOWS	SOIL	W%	UW	PASS	LL	PL	PI	TEST	φ	C	φ	C	OTHERS
NO.	(ft)	TYPE	ft	GROUP		pcf	#200	%	%	%	TYPE	deg.	psi eak	deg.	psi idual	
												PE	ak	Res	luuai	
Α	7.0 - 7.9	SPT		SC			37.3	30	19	11						
В	17.0 - 18.5	SPT		SC-SM			28.9	25	18	7						
C1	27.3 - 27.8	CMS		CL	22.15*	98.5*	55.1*	45*	22*	23*	DS	26	16.78	20	7.82	
a	1.1"				16.1	111.3										
ь	1.1"				18.6	n/a										
С	1.1"				21.9	99.4										
d	2.66"				32.0	84.8										
C2	27.8 - 28.3	CMS		sc	24.7	96.4	47.4	44	23	21						
C3	28.3 - 28.5	CMS		SC-SM			24.3	23	17	6						
D	28.5 - 29.3	SPT		SM			20.5	18	NP	NP						
E1	32.1 - 32.6	CMS		SM	8.33*	120.85*	16*	17*	NP*	NP*	DS	43	12.34	31	6.73	
a	1.1"				8.4	119.7										

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UU = Unconsolidated Undrained

CD = Consolidated Drained

CU = Consolidated Undrained

DS = Direct Shear

C = Cohesion

N = No. of blows per 0.3m, sampler

N = Field SPT

 $N = (N_{css})(0.62)$ 

H = Hydrometer

S = Sieve

G = Specific Gravity

PI = Plasticity Index

LL = Liquid Limit

PL = Plastic Limit NP = Non-Plastic

OC = Consolidation

Ch = Chemical RV = R - Value

MD = Moisture Density

CM = Compaction

E = Swell/Pressure on Expansive Soils

SL = Shrinkage Limit UW= Unit Weight W = Moisture Content

K = Permeability

O = Organic Content D = Dispersive

RQD = Rock Quality Designation

X = X-Ray Defraction

<sup>\* =</sup> Average of subsamples

EA/Cont # 72781-1 Job Description Carson City Freeway @ Clearview Dr.

**Boring No.** CV3 Elevation (ft) Station

	SAMPLE	SAMP-	N			DRY	%					STF	RENGTH T	EST		
SAMPLE	DEPTH	LER	BLOWS	SOIL	W%	UW	PASS	LL	PL	PI	TEST	φ	C	φ	C	OTHERS
NO.	(ft)	TYPE	ft	GROUP		pcf	#200	%	%	%	TYPE	deg.	psi	deg.	psi	
												Pe	ак	Res	idual	
b	1.1"				8.6	118.0										
С	1.1"				8.0	122.0										
d	2.68"				8.3	123.7										
E2	32.6 - 32.8	CMS		SM			19.0									
F	37.0 - 38.3	SPT		SM			20.8									
G	42.0 - 43.5	SPT		SM			25.7									
Н	47.0 - 48.5	SPT		SM			26.8									
I	52.0 - 52.9	SPT		SM			20.2									
J	57.0 - 58.5	SPT		SC			30.0	28	17	11						
K1	62.2 - 62.7	CMS		SC	14.4	117.8	29.9	36	17	19						
K2	62.7 - 63.2	CMS		SC	14.9*	115.7*	32*	36*	16*	20*	DS	30	13.7	34	0.71	_
a	1.1"				15.0	115.2										

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HCpot = Hydro-Collapse Potential

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EA/Cont # 72781-1 Job Description Carson City Freeway @ Clearview Dr.

**Boring No.** CV3 Elevation (ft) Station

	SAMPLE	SAMP-	N			DRY	%					STI	RENGTH T	EST		
SAMPLE	DEPTH	LER	BLOWS	SOIL	W%	UW	PASS	LL	PL	PI	TEST	φ	С	φ	C	OTHERS
NO.	(ft)	TYPE	ft	GROUP		pcf	#200	%	%	%	TYPE	deg.	psi	deg.	psi	
-												PE	ak	Res	idual	
ь	1.1"				14.6	n/a										
С	1.1"				15.0	115.0										
d	2.58"				15.0	116.9										
K3	63.2 - 63.5	CMS		SC			34.1	36	19	17						
L	67.0 - 68.5	SPT		sc			24.7	32	19	13						
M	72.0 - 73.5	SPT		sc			29.0									
N	77.0 - 78.5	SPT		SC			31.4	34	17	17						
О	82.0 - 83.5	SPT		SC			22.3									
P1	87.3 - 87.8	CMS		SC	14.0	119.8	35.0	31	18	13						
P2	87.8 - 88.3	CMS		SC	15.2	118.0	36.5	30	17	13						
Р3	88.3 - 88.5	CMS		SC			31.6									
Q	92.0 - 93.3	SPT		SC			31.7	35	17	18						

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