
GEOTECHNICAL INVESTIGATION

U.S. 95 WIDENING PROJECT

2C AND 2D RETAINING WALLS

CLARK COUNTY, NEVADA

NOVEMBER 2002



Prepared for:

PBS&J

Black Eagle Consulting, Inc. - Geotechnical & Construction Services



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November 26, 2002
Project No.: 0324-01-3

**RE: Project 2C and 2D Retaining Walls
Geotechnical Investigation**

Dear Mr. McFall:

The following report presents our geotechnical investigation for the 23 retaining walls in Project 2C and 2D U.S. 95 Widening. All design recommendations are based on soil profiles and strength characteristics determined during our field exploration and laboratory testing programs, information in the 90 percent Design Submittal by BRG Engineering, and previous investigations.

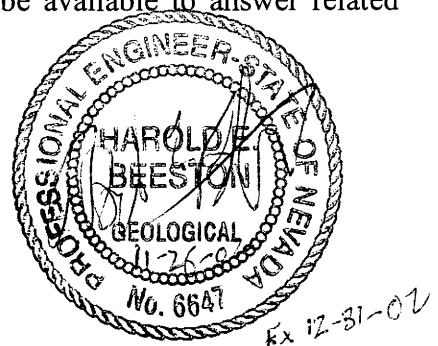
Soils encountered along the alignment are dominated by high-strength, moderately-cemented, sandy gravels. The area explored is suitable for standard spread footings to support the retaining walls.

We wish to thank you for the opportunity to provide our services and will be available to answer related questions.

Sincerely,

Black Eagle Consulting, Inc.

Larry J. Johnson
President



Harold E. Beeston, P.E.
Special Projects Manager

Enclosure: Geotechnical Investigation

LJJ:HEB:ycw

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GEOTECHNICAL INVESTIGATION

U.S. 95 WIDENING PROJECT

PROJECT 2C AND 2D RETAINING WALLS

CLARK COUNTY, NEVADA

INTRODUCTION

Presented herein is a description of the Black Eagle Consulting, Inc. (BEC) geotechnical investigation for the proposed Project 2C and 2D retaining walls that are part of the U.S. 95 Widening Project in Las Vegas, Nevada. This report presents recommendations that would be associated with the retaining wall locations shown in 90 percent submittal plans dated April 29, 2002, by BRG Engineering. The investigation itself consisted of research of existing documents, including the recent BEC reports for the Rainbow Boulevard Bridge replacement, and the R6 and R7 Bridges, and the advancement of eight additional exploration borings, laboratory analysis, and geotechnical analysis. The objectives of this study were to:

1. Determine general soil conditions pertaining to the design and construction of the proposed retaining walls.
2. Provide recommendations for design and construction of the new retaining walls, as related to these geotechnical conditions.

The services described herein were conducted in accordance with the Subcontract Addendum to PBS&J Sub-consultant Contract for *PBS&J Project 511300 with Black Eagle Consulting, Inc., with the short title, "U.S. 95 Project 2C and 2D Retaining Wall."*

PROJECT DESCRIPTION

It has been proposed to widen U.S. 95 to ten lanes in the vicinity of the Summerlin Parkway/Rainbow Boulevard/U.S. 95 Highway interchange. Twenty-three retaining walls, along with other facilities, will be constructed in the interchange to accomplish this goal. The Project 2C and 2D retaining walls (RW-1 through RW-23) characteristics are described below in Table 1.

Table 1 – Retaining Wall Characteristics

Name	Type	Length (m)	Maximum Height (m)	Minimum Height (m)	Foundation
RW-1	Cantilever	47	9.8	1.0	Spread Footing on Native Soils
RW-2	Cantilever	130	3.5	1.2	Spread Footing on Fill
RW-3	MSE	21	8.3	7.6	Footing Pad on Native Soils
RW-4	MSE	15	10.3	8.9	Footing Pad on Native Soils
RW-5	Soil Nail	38	2.4	1.4	Nails in Fill
RW-6A	Tieback/Soil Nail	50	5.4	1.1	Tiebacks and Nails in Fill
RW-6B	Cantilever	14	6.3	1.7	Spread Footing on Native Soils
RW-7	Tieback/Soil Nail	58	5.7	1.1	Tiebacks and Nails in Fill
RW-8	Cantilever	223	5.6	1.6	Spread Footing on Native Soils
RW-9	Cantilever	129	6.8	1.2	Spread Footing on Native Soils
RW-10	Cantilever	64	6.8	1.1	Spread Footing on Native Soils
RW-11	Cantilever	45	9.2	1.1	Spread Footing on Native Soils
RW-12	Cantilever	30	10.4	9.9	Spread Footing on Native Soils
RW-13	Cantilever	27	6.7	1.3	Spread Footing on Native Soils
RW-14	Cantilever	46	2.4	1.1	Spread Footing on Native Soils
RW-15	Cantilever	165	5.9	1.3	Spread Footing on Native Soils
RW-16	Tieback	67	5.8	0.8	Tiebacks in Native Soils
RW-17	Soil Nail	315	9.3	1.1	Nails in Fill
RW-18	Cantilever	103	2.4	1.1	Spread Footing on Native Soils
RW-19	Tieback	53	5.4	1.5	Tiebacks in Fill
RW-20	Cantilever	110	2.6	1.2	Spread Footing on Native Soils
RW-21	Cantilever	685	3.4	1.0?	Spread Footing on Native Soils
RW-22	Cantilever	145	3.5	2.0	Spread Footing on Native Soils
RW-23	Cantilever	94	3.8	1.7	Spread Footing on Native Soils

The Project 2C and 2D retaining wall sites extend along the U.S 95 from the Torrey Pines overpass on the east about 2,000 meters (m) to the Washington Avenue overpass on the northwest, along Summerlin Parkway about 200 meters west of the interchange, and along Rainbow Boulevard about 150 meters south of the interchange. Locations of the walls are shown in the Plot Plan in Plate 1

SITE CONDITIONS

Within the project area, there are several existing bridges that extend over U.S. 95, including the Summerlin Parkway Bridge, a steel-girder structure with seven spans and abutments; the 75-meter-long, two-span, post-tension, concrete box girder Rainbow Boulevard Bridge; the 60-meter-long, two-span, Washington Avenue Bridge that extends over U.S. 95 approximately 500 meters north of the Rainbow Bridge. The Washington Avenue Bridge consists of two parallel structures (the youngest structure was recently built to accommodate increased traffic flows), and the abutments for both structures have been placed on engineered fill.

The surface of the ground within the NDOT right-of-way, both within the main Rainbow interchange area and along the right-of-way shoulders north of the interchange, is covered mostly with sand, gravel, and low maintenance landscaping. The right-of-way east of the interchange, especially in the area of walls RW-21 and RW-23, narrows considerably where an existing retaining/sound wall separates the depressed northbound U.S. 95 traffic from private residences. Approximately 3 to 6 meters of open space, consisting of a sandy gravel soil with scattered weeds and refuse, are found between the wall and private property to the north. A 2-meter-high chain-link fence marks the actual NDOT boundary.

Various utilities, including storm drains and landscape irrigation lines associated with the right-of-way, are located throughout the project area. Communications lines and a gas pipeline, at an unknown depth, extending east-west beneath the Washington Avenue Bridge, are of specific concern.

EXPLORATION

Drilling

BEC explored the proposed retaining walls and new bridges at specific intervals in July 2001 to July 2002 by drilling a total of 42 hollow-stem auger borings to depths of up to 35 meters. The borings were drilled with 152-millimeter (-mm), outside-diameter (O.D.), 83-mm, inside-diameter (I.D.) augers. It should be noted that many of the borings utilized for the Project 2C and 2D retaining wall investigation were drilled during the exploration of the more extensive Rainbow/U.S. 95 interchange study and boring numbers are not in a continuous sequence. The existing fill, if any was identified, and native soil encountered in the borings were sampled in place every 600 mm by use of a standard, 51-mm, O.D., Split-Spoon Sampler driven with a standard 63.6-kilogram (-kg) drive hammer and a 762-mm stroke or an 89-mm O.D. Split-Spoon Sampler (ASTM D 3550).

Included in the analyses was evaluation of previously drilled borings located in close proximity to the proposed retaining walls. These included: Wallace, Inc., 1987, borings drilled for the design of the Summerlin Flyover that are adjacent to RW-2, RW-3, RW-6, and RW-7; NDOT, 1974, borings adjacent to RW-5 and

RW-19; and borings drilled by Terracon in 2000 for the Torrey Pines Bridge reconstruction that are adjacent to RW-21. The locations of all borings are shown on Plate 1.

Material Classification

An engineering geologist examined and classified all soils in the field. During drilling, representative bulk samples were placed in sealed plastic bags and returned to our Reno, Nevada, laboratory for testing. Additional soil classification was subsequently performed in accordance with ASTM 2487 (Unified Soil Classification System [USCS]) upon completion of laboratory testing as described below in the **Laboratory Testing** section. Logs of the borings, including the previous borings, are presented in Appendix I (Boring Logs).

LABORATORY TESTING

All soils testing performed in the BEC soils laboratory have been conducted in accordance with the standards and methods described in American Association of State Highway Transportation Officials (AASHTO, 1998) and Nevada Department of Transportation (NDOT, 2000) standards.

Index Testing

Samples of each significant soil type were analyzed to determine their in-situ moisture content (NDOT T 206F), grain size distribution, and plasticity index (NDOT 210E, 211E, and 212E). The results of these tests are in Appendix II (Test Results). Results of these tests were used to classify the soils according to USCS and to verify the field logs, which were updated where appropriate. Classification in this manner provides an indication of the soil's mechanical properties and can be correlated with standard penetration testing and published charts (Bowles, 1996; NAVFAC, 1982) to evaluate bearing capacity, lateral earth pressures, and settlement potential.

Direct Shear Tests

No direct shear tests were performed in this phase of exploration. Previous BEC testing for direct shear was performed on eleven samples of similar soils collected within the Rainbow interchange and reported in the Rainbow Bridge, R6, and R7 reports.

Corrosion Potential Tests

No corrosion potential tests were performed in this phase of exploration. Previous BEC testing for corrosion potential was performed on samples of similar soils. The tests for pH, soil resistivity, and soluble chloride and sulfate show that most of the soil in the interchange would not be corrosive to steel and concrete.

GEOLOGIC AND GENERAL SOIL CONDITIONS

The retaining wall sites are on soils that have been mapped by the Nevada Bureau of Mines and Geology (NBMG) (Matti, et al., 1987) as Older Alluvium of the Red Rock Fan (Pleistocene). According to the NBMG, the fan deposits consist of moderately well-consolidated and cemented, pebble to small cobble gravel with pebble-bearing sand. Previous drilling by NDOT for the overpass construction at Rainbow Boulevard (1974) and Washington Avenue (1977) encountered up to 60 feet of dense-to-very-dense, cemented sandy gravel. Drilling by BEC in 2001 and early 2002 within the US 95/Rainbow Boulevard interchange also encountered up to 30 meters of these same cemented sands and gravels. These logs are included in Appendix 1.

The native materials encountered in the main interchange and Washington Avenue, consist of very dense, moderately cemented, gravelly clayey sand and sandy gravel to depths of 7 to 30 meters. This highly competent native soil behaves very much like rock because of its cementation and density. These materials were consistent throughout the depth and lateral extent of exploration. The borings at the east end of Summerlin Parkway encountered dense clayey sand and sandy fat clay interbedded within the competent sand and gravel layers as high as 7 meters. These less competent units contained up to 55 percent medium to high plastic fines.

Variable depths of highway embankment were encountered in several of the borings. The embankment was dense-to-very-dense sand and gravel that is similar to the underlying native material. The embankment/native contact was often difficult to distinguish due to this similarity.

Ground water was not encountered during the exploration. It is, therefore, at a depth that would not affect construction.

GEOLOGIC AND SEISMIC HAZARDS

Seismicity

Much of the Western United States is a region of moderate to intense seismic activity related to movement of the crustal masses (plate tectonics). By far the most active region, outside of Alaska, centers on the San Andreas Fault system of western California. The particular area in Las Vegas, however, is not a highly active seismic area, but does have some potential for earthquakes. The AASHTO map in Division I-A of the *Standard Specifications for Highway Bridges* (1996) shows horizontal rock acceleration potential to be 0.15g for a 10 percent probability of exceeding it within 50 years in this area. For the purposes of this project, we recommend a design acceleration value of 0.15g to be used in accordance with NDOT design policy. The soils encountered during exploration have shear-wave velocities in excess of 600 meters per second. This is considered to be rock-like material for seismic evaluation purposes and is equivalent to the soil profile Type 1, as defined on page 399 of Division I-A of AASHTO *Seismic Design for Highway Bridges* (1996). However, conditions within the Las Vegas Valley are such that there is a strong potential for amplification of earthquake motion in the lower frequencies of less than three (3) hertz (Su, et al., 1996). Because of the unusual character of the Las Vegas Basin to amplify the lower frequencies and attenuate the higher frequencies, we recommend the use of a Soil Profile Type 2, which is more conservative than Type 1. This would give a Type 2 site coefficient of 1.2 for a seismic site coefficient of 0.18.

There is no potential for liquefaction at the site because the ground water is located at a depth below 30 meters.

Faults and Fissures

Area Quaternary faults have been mapped by the NBMG and are presented in the *Map of Faults and Earth Fissures in the Las Vegas Area* (DePolo and Bell, 2000). This map identifies traces of potential Quaternary age tectonic faults approximately 4 kilometers (km) west and 2 km east of the site, but there is no evidence of faulting through the site itself. Fissured areas are associated with the faults shown on this map. Fissures have been found approximately 4 km east of the site; however, there is no evidence of fissuring at the site.

Ground Subsidence

Regional land subsidence in the Las Vegas Valley related to ground water withdrawal has been monitored since 1935 (Bell and Price, 1993). A map included in that open-file report, titled *Subsidence in Las Vegas Valley 1963 Through 1986/87*, identifies three major Las Vegas subsidence centers located about 7 km north, 7 km east, and 8 km southeast of the site. The map also shows that subsidence of about 30 mm has occurred in the site vicinity between the years 1963 and 1987. This translates into a rough extrapolation of regional subsidence in the area of about 100 mm to the present day. Since this is a regional behavior and the actual settlement is slow (about 1 to 2 mm per year), there should not be any significant distress to the proposed retaining walls in the lifetime of the structures.

Dust Generation

A moderate potential for dust generation is present if grading is performed in dry weather. No other geological hazards have been identified.

RESULTS AND DISCUSSION

Retaining Wall Design

Project 2C and D will use conventional (cantilever), mechanically stabilized embankment (MSE), soil nail and tieback anchored retaining walls. The top-down constructed anchored walls will support native and/or pre-existing fill material. The cantilever and MSE walls will be backfilled with imported fill, or reworked native soil.

The native soil is very dense, weak to moderately cemented, alluvial sand and gravel. Table 2 provides the soil parameters for the native soil, pre-existing fill, and imported fill used in the soil pressure calculations. Where reworked native soil is used as backfill, after screening the plus-6-inch fraction, the material will have the same characteristics as the imported fill.

TABLE 2 – SOIL PARAMETERS TO USE FOR DESIGN

	Unit Weight (kN/m³)	Phi Angle	Cohesion
Native Soil	20.4	40	0
Pre-existing and Imported Fill	19.6	34	0

The ground water table is at depth below the current exploration levels (> 30 meters in depth) and is not a factor in the design or construction of the retaining walls. A drainage system that includes a back face

drainage system and weep holes at the base of the wall should be used behind and along the toe of all of the walls to reduce any hydrostatic pressure that could result from surface infiltration.

Conventional Reinforced Concrete Cantilever Retaining Walls

Table 3 shows the recommended static and dynamic condition bearing and lateral soil pressure parameters for cantilever retaining wall design. The values are based on Mononobe-Okabe analyses, as referenced in Federal Highway Administration (FHWA, 1998); and, the calculations are included in Appendix III. The Table 3 recommendations are for both level and sloping backfill conditions.

TABLE 3 – CANTILEVER RETAINING WALL BEARING AND PRESSURE PARAMETERS

Name	Foundation	Allowable Bearing Pressure (Mpa)	Ultimate Bearing Pressure (Mpa)	Ultimate Base Sliding Coefficient	Backfill Pressure Coefficient* K _a	Backfill Pressure Coefficient* K _{ae}	Backfill Unit Weight kN/m ³
RW-1	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-2	Spread Footing Embankment	0.190	0.570	0.5	0.28 0.42	0.33 0.58	19.6
RW-6B	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-8	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-9	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-10	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-11	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-12	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-13	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-14	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-15	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6
RW-18	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 0.42	0.33 0.58	19.6

TABLE 3 – CANTILEVER RETAINING WALL BEARING AND PRESSURE PARAMETERS

Name	Foundation	Allowable Bearing Pressure (Mpa)	Ultimate Bearing Pressure (Mpa)	Ultimate Base Sliding Coefficient	Backfill Pressure Coefficient* <i>K_a</i>	Backfill Pressure Coefficient* <i>K_{ae}</i>	Backfill Unit Weight kN/m ³
RW-20	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 <i>0.42</i>	0.33 <i>0.58</i>	19.6
RW-21	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 <i>0.42</i>	0.33 <i>0.58</i>	19.6
RW-22	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 <i>0.42</i>	0.33 <i>0.58</i>	19.6
RW-23	Spread Footing on Native Soils	1.0	3.0	0.55	0.28 <i>0.42</i>	0.33 <i>0.58</i>	19.6

*Plain text is for level backfill, *Italicized* text is for 1:2 (V:H) sloping backfill

Backfill behind cantilever retaining walls should be compacted in accordance with NDOT standard specifications (2001). Care should be exercised when compacting backfill against retaining walls. To reduce temporary construction loads on the walls, heavy equipment should not be used for placing and compacting fill within a region as determined by a 2:1 (V:H) line drawn upward from the bottom of the wall, or within 1 meter of the wall, whichever is greater. We recommend that hand-operated compaction equipment be used to compact soils adjacent to walls. Areas to receive fill, or those areas located beneath proposed structural footings, should be cleared and grubbed as to NDOT specifications (NDOT, 2001).

MSE Retaining Walls

Table 4 shows the recommended static and dynamic condition bearing and lateral soil pressure parameters for MSE retaining wall design. The values are based on Mononobe-Okabe analyses, as referenced in Federal Highway Administration (FHWA, 1998); and, the calculations are included in Appendix III.

TABLE 4 – MSE RETAINING WALL BEARING AND PRESSURE PARAMETERS

Name	Foundation	Allowable Bearing Pressure (Mpa)	Ultimate Bearing Pressure (Mpa)	Ultimate Base Sliding Coefficient	Backfill Pressure Coefficient* <i>K_a</i>	Backfill Pressure Coefficient* <i>K_{ae}</i>	External Backfill Unit Weight kN/m ³
RW-3	Footing Pad on Native Soils	1.0	3.0	0.68	0.28 <i>0.37</i>	0.43 <i>0.89</i>	19.6
RW-4	Footing Pad on Native Soils	1.0	3.0	0.68	0.28 <i>0.37</i>	0.43 <i>0.89</i>	19.6

*Plain text is for level backfill, *Italicized* text is for 1:2 (V:H) sloping backfill

Backfill behind MSE walls should be compacted in accordance with NDOT Standard Specifications (2001). To reduce temporary construction loads on the walls, heavy equipment should not be used for placing and compacting fill within a region as determined by a 2:1 (V:H) line drawn upward from the bottom of the wall,

or within 1 meter of the wall, whichever is greater. We recommend that hand-operated compaction equipment be used to compact soils adjacent to walls. Areas to receive fill, or those areas located beneath proposed structural footings, should be cleared and grubbed as to NDOT Specifications (NDOT, 2001).

Soil Nail Retaining Walls

Soil nail walls are flexible walls constructed from the top down in existing materials (both native soil and pre-existing fill) using reinforcing nails or bars placed at regular spaced intervals. A facing of shotcrete is typically applied to support face loadings during and after construction. Earth pressure is transferred from the wall face to the nails by the facing. The load transfer mechanism associated with soil nail walls is either frictional interaction between the nail and soil, or by the soil structure interaction between the soil and facing.

Table 5 shows the estimated ultimate bond stress shown in Table 8-6 (Munfakh, et al., 1998), and recommended static and dynamic parameters for soil nail retaining wall design based on Mononobe-Okabe analyses (FHWA, 1998). The calculations are included in Appendix III.

TABLE 5 – SOIL NAIL DESIGN AND PRESSURE PARAMETERS

Name	Foundation	Ultimate Bond Stress (kPa)	Phi Angle (degrees)	Cohesion (kPa)	Backfill Pressure Coefficient* K_a	Backfill Pressure Coefficient* K_{ae}	Embankment Unit Weight kN/m ³
RW-5	Nails in Fill	150	34	0*	0.28 0.42	0.33 0.58	19.6
RW-6A	Nails in Fill	150	34	0*	0.28 0.42	0.33 0.58	19.6
RW-7	Nails in Fill	150	34	0*	0.28 0.42	0.33 0.58	19.6
RW-17	Nails in Fill	150	34	0*	0.28 0.42	0.33 0.58	19.6

*Cohesion value to use for design. Actual existing material has enough cohesion for construction of soil nail walls

**Plain text is for level backfill, *Italics* is for 1:2 (*V:H*) sloping back fill

BRG Engineering will design (length, spacing, etc.) the soil nail walls. Verification and proof testing of nails should be performed. Pre-production verification tests on sacrificial test nails, as well as proof tests on production nails, should be performed at the locations specified by BRG Engineering. Verification and proof testing of nails should follow the criteria and loading schedules recommended by the FHWA (1994).

— Wall excavation should follow the regulations set forth by OSHA for sidewall excavation. Nail encapsulation using double corrosion protection (epoxy coating and encapsulation) is recommended for permanent walls. A drain system is recommended to allow water to exit the facing through small drains along the lower edge of the wall. A 400-mm-wide drainage composite strip should be placed vertically on 1.2-meter spacing between

each column of soil nails. At the base of each drainage strip, a prefabricated drain grate should be placed to connect to a 75-mm-diameter PVC pipe, day-lighted out of the face of the wall at a 2 percent slope. A wall toe drain should be constructed to capture water flow from the drain strip drainage pipes. The toe drain may be either a concrete drainage swale or a drain trench.

Tieback Anchor Retaining Walls

The anchors in these walls will be designed to offset the surcharge loads from existing bridge abutment footings. Table 6 shows the estimated ultimate transfer load shown in Table 7-6 (Munfakh, et al., 1998), and recommended maximum static and dynamic lateral pressure parameters for tieback anchor retaining wall designs. Graphs of the lateral pressures are in Plate 2. Calculations are included in Appendix III.

TABLE 6 – TIEBACK ANCHOR DESIGN AND PRESSURE PARAMETERS

Name	Foundation	Ultimate Transfer Load (kN/m)	Phi Angle (degrees)	Cohesion (kPa)	Embankment Unit Weight kN/m ³	Maximum Static Lateral Pressure (kPa)	Maximum Dynamic Lateral Pressure (kPa)
RW-6A	Tiebacks in Fill	220	34	0*	19.6	62.6	87.1
RW-7	Tiebacks in Fill	220	34	0*	19.6	55.7	83.3
RW-16	Tiebacks in Native Soil	290	40	0*	20.4	45.2	66.1
RW-19	Tiebacks in Fill	220	34	0*	19.6	67.5	88.1

*Cohesion value to use for design. Actual existing material has enough cohesion for construction of tieback walls

Wall construction should follow the regulations set forth by OSHA for excavation sidewalls. Anchor design and construction should follow the specifications found in Appendix E of Publication No. FHWA-IF-99-015 titled *Geotechnical Engineering Circular No. 4; Ground Anchors and Anchored Systems*, dated June 1999. These specifications include guidelines on the required corrosion protection and performance testing. Verification and proof testing of anchors should follow the criteria and loading schedules recommended by the Federal Highway Administration (FHWA, 1999).

RECOMMENDATION LIMITS

The above recommendations are based on the 90 percent information that BEC has submitted at this time. If the design and location of the retaining walls change, however, these recommendations are also subject to change.

STANDARD LIMITATION CLAUSE

This report has been prepared in accordance with generally accepted geotechnical practices. The analyses and recommendations submitted are based on field exploration performed at the locations shown on Plate 1 (Retaining Wall Plot Plan) and previous on-site investigations for existing structures. This report does not reflect soils variations that may become evident during the construction period, at which time re-evaluation of the recommendations may be necessary. This report has been prepared to provide information allowing the engineer to design the project. In the event of changes in the design or location of the project from the time of this report, recommendations should be reviewed and possibly modified by the geotechnical engineer. If the geotechnical engineer is not accorded the privilege of making this recommended review, he can assume no responsibility for misinterpretation or misapplication of these recommendations or their validity in the event changes have been made in the original design concept without his prior review. The geotechnical engineer makes no other warranties, expressed or implied, as to the professional recommendations provided under the terms of this agreement and included in this report.

REFERENCES

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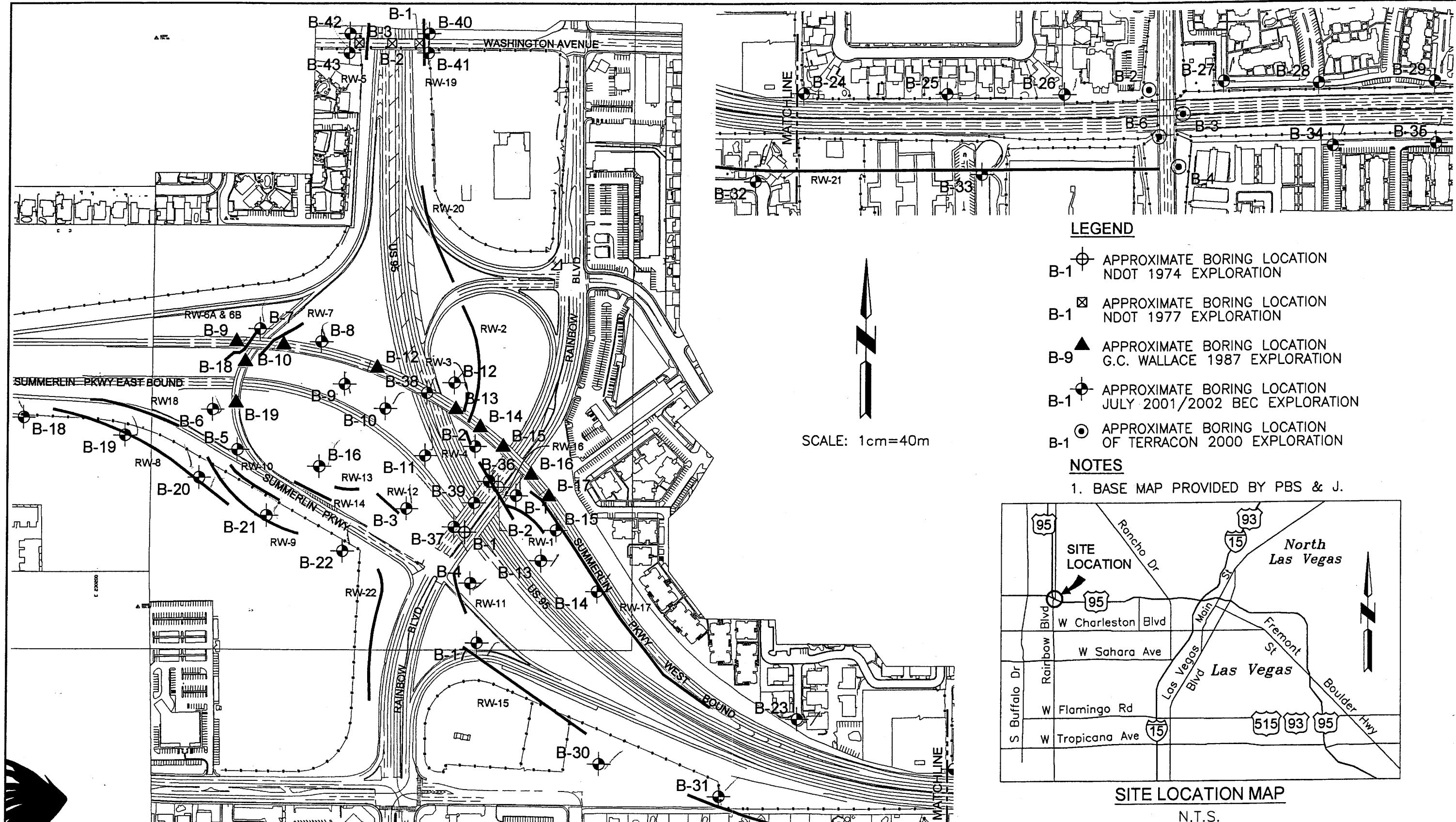
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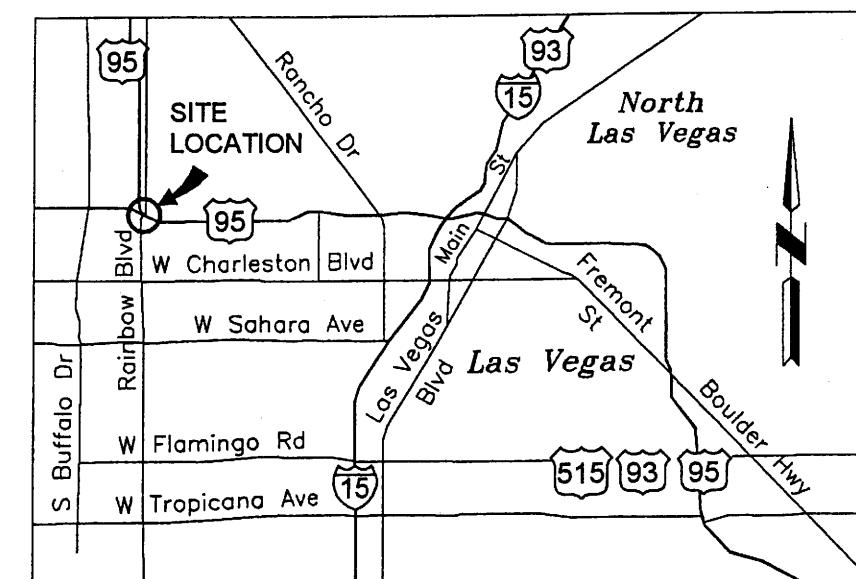
PLATES



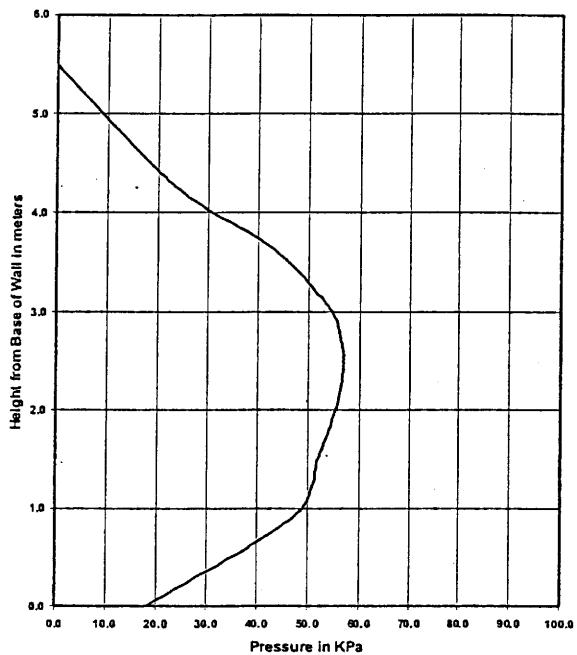
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Geotechnical & Construction Services
1345 Capital Boulevard, Suite A
Reno, Nevada 89502-7140
Telephone: 775/359-6600
Facsimile: 775/359-7766

PBS & J
PLOT PLAN
US95 PROJECT 2 C&D RETAINING WALL LOCATION
LAS VEGAS, NEVADA

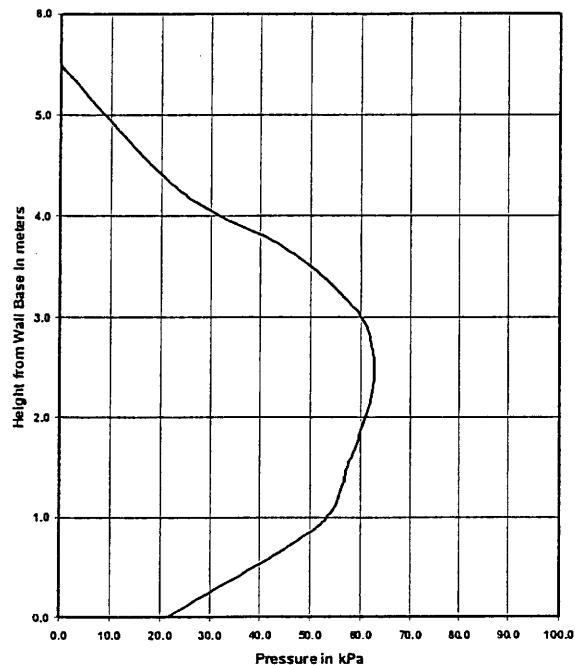
Project No.
0324-01-3
Plate 1



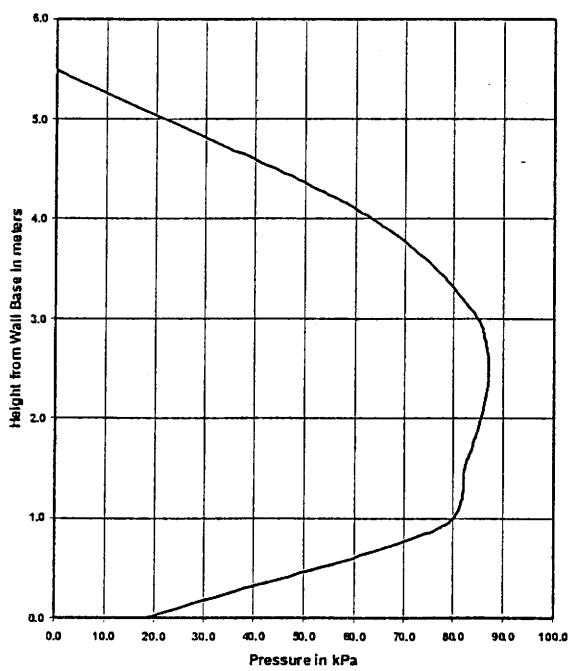
Lateral Pressure on RW-6
Dead Load Only



Lateral Pressure on RW-6
Dead Load + Live Load



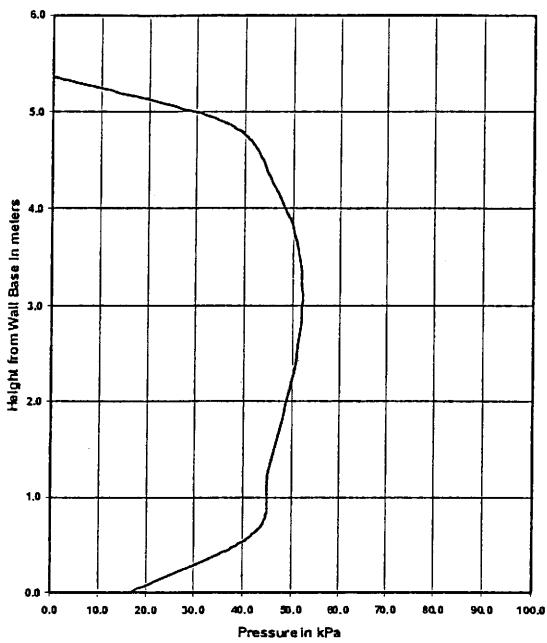
Lateral Pressure on RW-6
Dead Load + Seismic Load



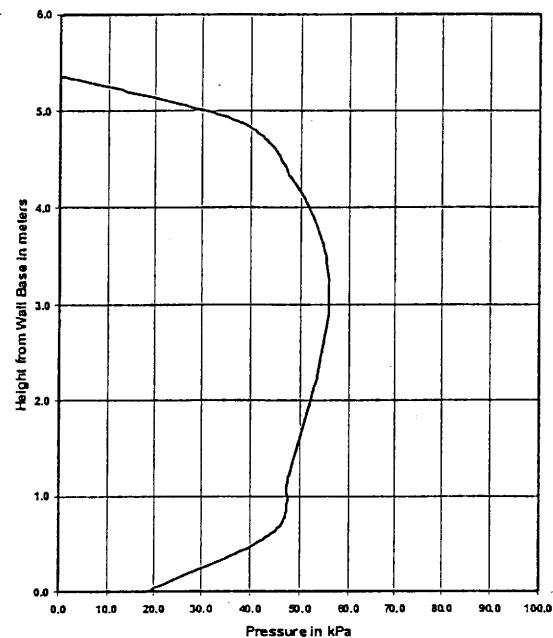
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Lateral Pressure on RW-6

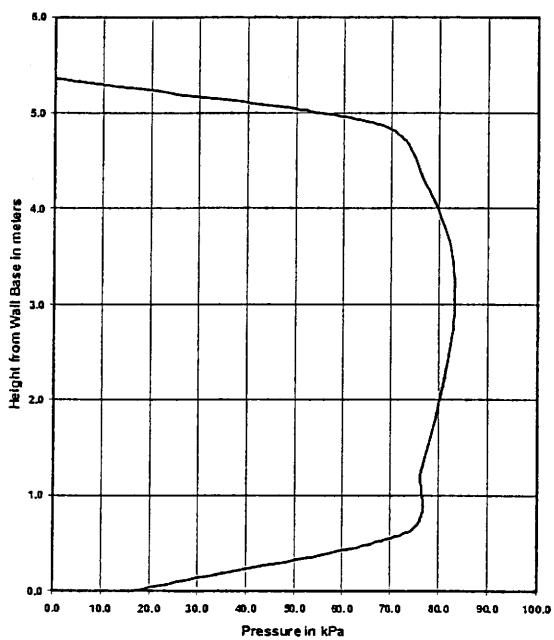
Lateral Pressure on RW-7
Dead Load Only



Lateral Pressure on RW-7
Dead Load + Live Load



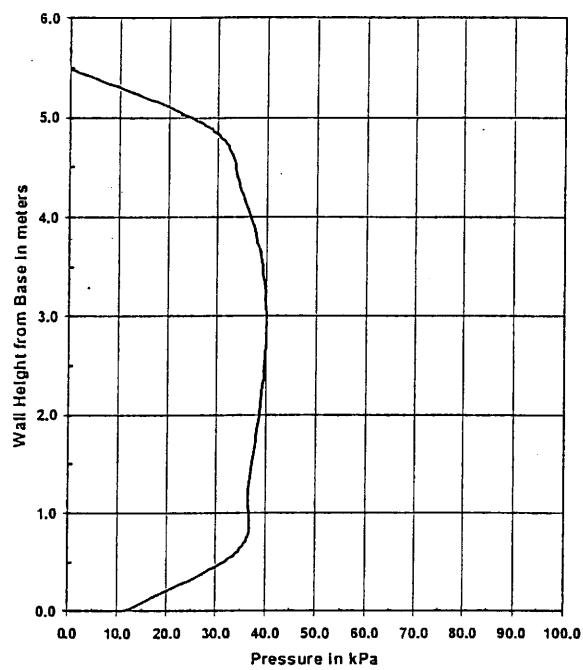
Lateral Pressure on RW-7
Dead Load + Seismic Load



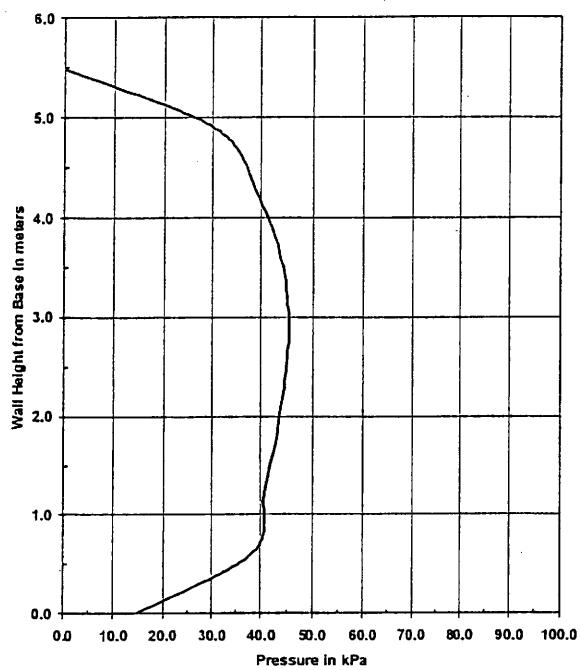
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Lateral Pressure on RW-7

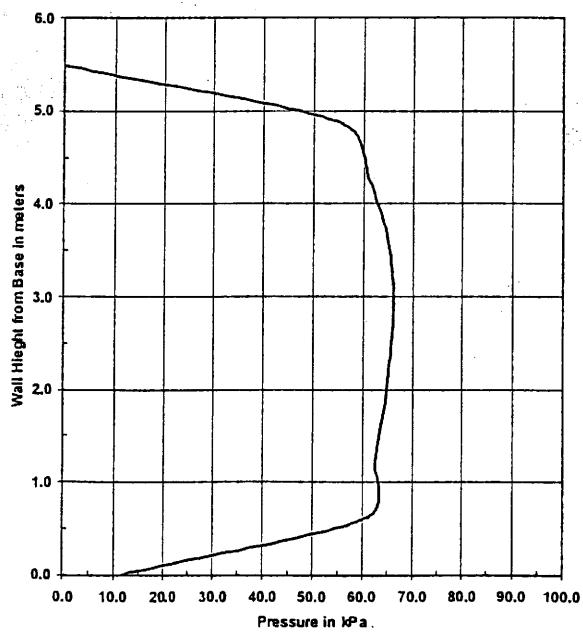
Lateral Pressure on RW-16
Dead Load Only



Lateral Pressure on RW-16
Dead Load+ Live Load



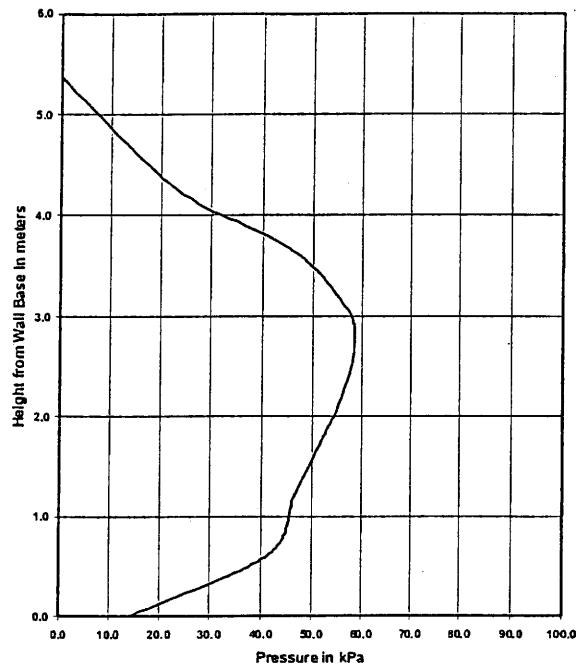
Lateral Pressure on RW-16
Dead Load + Seismic Load



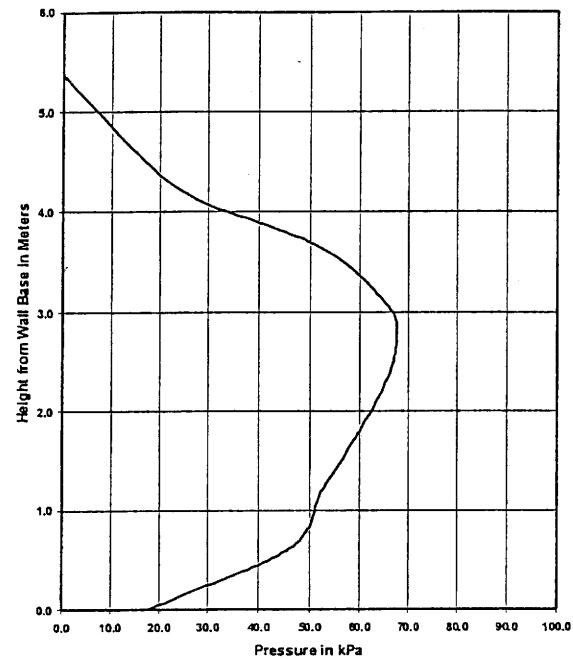
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Lateral Pressure on RW-16

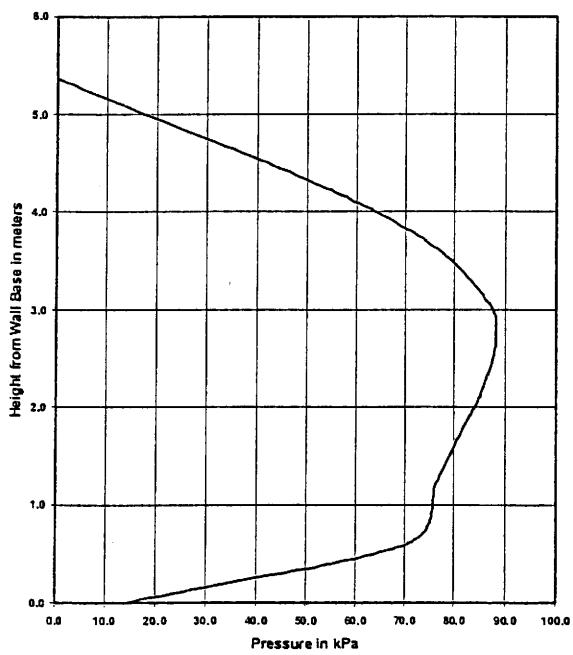
Lateral Pressure on RW-19
Dead Load Only



Lateral Pressure on RW-19
Dead Load + Live Load



Lateral Pressure on RW-19
Dead Load + Seismic Load



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Lateral Pressure on RW-19

APPENDIX I

BORING LOGS



EXPLORATION LOG

SHEET 1 OF 4

START DATE 7/20/01
 END DATE 7/20/01
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-01
 E.A. # 0324-01-1
 GROUND ELEV. 725.42 (m)
 HAMMER DROP SYSTEM Cable

STATION	<u>91+75 Q</u>	
OFFSET	<u>50 RT</u>	
ENGINEER	<u>PGT</u>	
EQUIPMENT	<u>Foremost B90</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>203 mm HS Auger</u>	
BACKFILLED	<u>Cased</u>	<u>DATE 7/20/2001</u>

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
724.42	1							GM	Silty Gravel with Sand ; light grey brown, dry, very dense, with estimated 15-20% low plastic fines, 30-35% fine to coarse sand, 50-55% subangular limestone gravel to 3". 10-15% oversize to 6". Moderately cemented.	
1.52	1A	MC	50/75	50/75	0				Poorly Graded Gravel with Clay and Sand ; light brown grey, slightly moist, very dense, with 9% low to medium plastic fines, 35% fine to coarse sand, 56% subangular to subrounded limestone gravel to 2". Moderately cemented. All size fractions, including cement, are calcareous.	
1.68									Lithology is based on auger cuttings which is likely biased toward a more coarse sample (the auger winnows out the fine material thereby increasing the apparent gravel content). Actual soil might be a cemented Silty Gravel with Sand or a Silty Sand with Gravel.	
723.42	2	1A'	GRAB			50	SV, PI, Dens		Gravel becomes progressively finer and more subrounded down hole. Predominantly <1" at base of unit.	
722.42	3	1B	SPT	50/50	50/50	0				
3.20										
3.66	1B'	GRAB				50				
721.42	4							GP		
4.57	1C	MC	50/38	50/38	100			GC		
720.42	5									
719.42	6	1D	SPT	50/25	50/25	0				
6.25										
6.71	1D'	GRAB				50	SV, PI, Dens			
718.42	7									
7.62	1E	MC	50/75	50/75	100		SV, PI, Dens	7.32	Clayey Sand with Gravel ; light grey brown, slightly moist, very dense, with 19% low to medium plastic fines, 51% fine to coarse sand, 30% subrounded limestone gravel to 1". Moderate to well cemented. Gravel is sheared into sharp fragments during augering.	
717.42	8									
716.42	9	1F	SPT	50/25	50/25	50	SV, PI, Dens	SC	Samples 1F and 1G were combined for lab analysis.	
	9.14									



START DATE 7/20/01
 END DATE 7/20/01
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-01
 E.A. # 0324-01-1
 GROUND ELEV. 725.42 (m)
 HAMMER DROP SYSTEM Cable

EXPLORATION LOG

SHEET 2 OF 4

STATION	<u>91+75 Q</u>	
OFFSET	<u>50 RT</u>	
ENGINEER	<u>PGT</u>	
EQUIPMENT	<u>Foremost B90</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>203 mm HS Auger</u>	
BACKFILLED	<u>Cased</u>	<u>DATE 7/20/2001</u>

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
	10.67	1G	MC	50/75	50/75	100	SV, PI, Dens	GC GM	11.58 Silty, Clayey Gravel with Sand ; light brown grey, slightly moist, very dense, with 13% low plastic fines, 39% fine to coarse sand, 48% subangular limestone gravel to 1". Moderate to well cemented.	
714.42	11									
713.42	12	12.19	1H	SPT	50/25	50/25	0			
	12.34									
	12.80	1H'	GRAB			50				
712.42	13									
	13.72	1I	MC	50/25	50/25	0				
711.42	14									
710.42	15	15.24	1J	SPT	50/100	50/100	100			
709.42	16							SC	Samples 1J and 1K were combined for lab analysis.	
	16.76	1K	MC	50/50	50/50	50	SV, PI, Dens			
708.42	17									
707.42	18	18.29	1L	SPT	50/25	50/25	0			
	18.44									
	18.90	1L'	GRAB			50	SV, PI, Dens	SC SM	17.83 Silty, Clayey Sand with Gravel ; light brown grey, slightly moist, very dense, with 12% low plastic fines, 50% fine to coarse sand, 38% subrounded limestone gravel to 1.25". Moderately cemented.	
706.42	19									
	19.81	1M	MC	50/75	50/75	67				



EXPLORATION LOG

SHEET 3 OF 4

START DATE 7/20/01
 END DATE 7/20/01
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-01
 E.A. # 0324-01-1
 GROUND ELEV. 725.42 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>7/21/01</u>	<u>NE</u>	

STATION 91+75 Q
 OFFSET 50 RT
 ENGINEER PGT
 EQUIPMENT Foremost B90
 OPERATOR Eagle Drilling
 DRILLING METHOD 203 mm HS Auger
 BACKFILLED Cased DATE 7/20/2001

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
704.42	21								
21.34	21.49	1N	SPT	50/12	50/12	0			
703.42	22								
22.86	23	10	MC	50/38	50/38	0			
701.42	24								
24.38	24.54	1P	SPT	50/38	50/38	0			
700.42	25								
25.91	26	1Q	MC	50/50	50/50	0			
699.42	27								
27.43	28	1R	SPT	50/50	50/50	100			
698.42	29								
28.96	29.11	1S	MC	50/88	50/88	0			
696.42	30								
29.57	31	1S'	GRAB			50	SV, PI, Dens		

20.42 Poorly Graded Gravel with Silt and Sand ; light brown, slightly moist, very dense, with 11% low plastic fines, 44% fine to coarse sand, 45% subrounded limestone gravel to 1.5". Moderate to well cemented.

23.77 Well Graded Gravel with Silty Clay and Sand ; light brown grey, slightly moist, very dense, with 11% low plastic fines, 39% fine to coarse sand, 50% subangular limestone gravel to 1.25". Moderately cemented.

26.21 Clayey Sand with Gravel ; light brown, slightly moist, very dense, with estimated 15-20% low to medium plastic fines, 45-50% fine to coarse sand, 30-35% subangular gravel to 0.75". Moderate to well cemented.

28.35 Well Graded Sand with Silt and Gravel ; light brown, slightly moist, very dense, with 12% low to medium plastic fines, 60% fine to coarse sand, 28% subangular limestone gravel to 1".



EXPLORATION LOG

SHEET 4 OF 4

START DATE 7/20/01
END DATE 7/20/01
JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
LOCATION Las Vegas, Nevada
BORING B-01
E.A. # 0324-01-1
GROUND ELEV. 725.42 (m)
HAMMER DROP SYSTEM Cable

STATION 91+75 Q
OFFSET 50 RT
ENGINEER PGT
EQUIPMENT Foremost B90
OPERATOR Eagle Drilling
DRILLING METHOD 203 mm HS Auger
BACKFILLED Cased DATE 7/20/2001

ELEV. (m)	DEPTH (m)	SAMPLE				LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
30.48	30.48	1T	SPT	50/12	50/12	0		30.48	
694.42	31								
693.42	32								
692.42	33								
691.42	34								
690.42	35								
689.42	36								
688.42	37								
687.42	38								
686.42	39								



EXPLORATION LOG

SHEET 1 OF 3

START DATE 7/21/01
 END DATE 7/21/01
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-02
 E.A. # 0324-01-1
 GROUND ELEV. 723.90 (m)
 HAMMER DROP SYSTEM Cable

STATION 92+61 Q
 OFFSET 39 RT
 ENGINEER PGT
 EQUIPMENT Foremost B90
 OPERATOR Eagle Drilling
 DRILLING METHOD 203 mm HS Auger
 BACKFILLED Yes DATE 7/21/2001

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>7/21/01</u>	<u>NE</u>	

ELEV. (m)	DEPTH (m)	SAMPLE			BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE		150 mm Increments	Last 300 mm				
722.90	1							GM	Silty Gravel with Sand ; light grey brown, dry, very dense, with estimated 15-20% low plastic fines, 35-40% fine to coarse sand, 45-50% subangular limestone gravel to 3". 10-15% oversize to 6". Moderately cemented with weak caliche coating on cobbles.	
	1.52	2A	MC	50/50	50/50	100		0.61		
	1.68							SW	Well Graded Sand with Silt and Gravel ; light grey brown, dry, very dense, with 10% low plastic fines, 47% fine to coarse sand, 43% subangular limestone gravel to 1.5". Moderate to well cemented. Gravel is sheared by the auger. Calcareous cement throughout hole.	
721.90	2	2A'	GRAB			50	SV, PI, Dens	SM		
	2.13									
	2.44									
720.90	3	2B	SPT	50/100	50/100	50		GC	Clayey Gravel with Sand ; light grey brown, dry, very dense, with 13% low to medium plastic fines, 42% fine to coarse sand, 45% subangular limestone gravel to 1.75". Moderately cemented.	
	3.05									
	3.20									
	3.66	2B'	GRAB			50	SV, PI, Dens			
719.90	4							GP		
	4.57	2C	MC	50/25	50/25	0		4.27	Poorly Graded Gravel with Sand ; light brown grey, dry, very dense, with 4% low plastic fines, 18% fine to coarse sand, 78% subrounded limestone gravel to 2.5". Moderate to well cemented.	
	4.72									
718.90	5	2C'	GRAB			50	SV, PI, Dens	GP		
	5.18									
	5.79									
717.90	6	2D	SPT	50/75	50/75	0		SC	Clayey Sand with Gravel ; light brown, dry, very dense, with 18% medium plastic fines, 55% fine to coarse sand, 27% subrounded limestone gravel to 2". Moderate to well cemented.	
	6.10									
	6.25									
	6.71	2D'	GRAB			50	SV, PI, Dens			
716.90	7									
	7.62	2E	MC	50/50	50/50	100	SV, PI, Dens			
715.90	8									
714.90	9	2F	SPT	50/12	50/12	0		9.75	Clayey Sand with Gravel ; light brown, dry,	
	9.14									



EXPLORATION LOG

SHEET 2 OF 3

START DATE	7/21/01	STATION	92+61 Q
END DATE	7/21/01	OFFSET	39 RT
JOB DESCRIPTION	US 95 Widening / Project 2D Retaining Walls	ENGINEER	PGT
LOCATION	Las Vegas, Nevada	EQUIPMENT	Foremost B90
BORING	B-02	OPERATOR	Eagle Drilling
E.A. #	0324-01-1	DRILLING METHOD	203 mm HS Auger
GROUND ELEV.	723.90 (m)	BACKFILLED	Yes DATE 7/21/2001
HAMMER DROP SYSTEM	Cable		

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
7/21/01	NE	

ELEV. (m)	DEPTH (m)	SAMPLE NO.	TYPE	BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
				150 mm Increments	Last 300 mm					
	10.67	2G	MC	50/12	50/12	0				
	10.82									
712.90	11	2G	GRAB			50	SV, PI, Dens	SC		
	11.28									
711.90	12	2H	SPT	50/38	50/38	0				
	12.19									
710.90	13									
	13.72	2I	MC	50/75	50/75	100	SV, PI, Dens	SC		
709.90	14									
708.90	15	2J	SPT	50/38	50/38	67				
	15.24									
	15.39									
	15.85	2J	GRAB			50	SV, PI, Dens	GP GC		
707.90	16									
	16.76	2K	MC	50/63	50/63	100	SV, PI, Dens			
706.90	17									
705.90	18	2L	SPT	50/25	50/25	0				
	18.29									
704.90	19									
	19.81	2M	MC	50/50	50/50	75	SV, PI, Dens	SC SM		



EXPLORATION LOG

SHEET 3 OF 3

START DATE 7/21/01
END DATE 7/21/01
JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
LOCATION Las Vegas, Nevada
BORING B-02
E.A. # 0324-01-1
GROUND ELEV. 723.90 (m)
HAMMER DROP SYSTEM Cable

STATION 92+61 Q
OFFSET 39 RT
ENGINEER PGT
EQUIPMENT Foremost B90
OPERATOR Eagle Drilling
DRILLING METHOD 203 mm HS Auger
BACKFILLED Yes DATE 7/21/2001

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>7/21/01</u>	<u>NE</u>	

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
702.90	21								
21.34	21.34	2N	SPT	50/25	50/25	0			
701.90	22								
22.86	22.86	2O	MC	50/38	50/38	67	SV, PI, Dens	22.86	
700.90	23								
699.90	24								
698.90	25								
697.90	26								
696.90	27								
695.90	28								
694.90	29								



EXPLORATION LOG

SHEET 1 OF 3

START DATE	7/21/01	STATION	92+26 Q
END DATE	7/21/01	OFFSET	65 LT
JOB DESCRIPTION	US 95 Widening / Project 2D Retaining Walls	ENGINEER	PGT
LOCATION	Las Vegas, Nevada	EQUIPMENT	Foremost B90
BORING	B-03	OPERATOR	Eagle Drilling
E.A. #	0324-01-1	DRILLING METHOD	203 mm HS Auger
GROUND ELEV.	728.47 (m)	BACKFILLED	Yes DATE 7/21/2001
HAMMER DROP SYSTEM	Cable		

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
7/21/01	NE	

ELEV. (m)	DEPTH (m)	SAMPLE						LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd					
727.47	1								GM	Silty Gravel with Sand ; light grey brown, dry, very dense, with estimated 15-20% low plastic fines, 35-40% fine to coarse sand, 45-50% subangular limestone gravel to 3". 5-10% oversize to 5". Moderately cemented with weak caliche coating on cobbles.	
	1.52	3A	MC	50/50	50/50	0			0.61	Silty Clayey Sand with Gravel ; light grey brown, dry, very dense, with 15% low plastic fines, 47% fine to coarse sand, 38% subangular limestone gravel to 2". Moderate to well cemented. Gravel is sheared by the auger. Calcareous cement throughout hole.	
726.47	2 2.13	3A'	GRAB			50	SV, PI, Dens		SC SM		
725.47	3 3.05 3.20	3B	SPT	50/38	50/38	0					
	3.66	3B'	GRAB			50	SV, PI, Dens				
724.47	4								3.96	Well Graded Gravel with Silt and Sand ; light brown grey, dry, very dense, with 12% low plastic fines, 42% fine to coarse sand, 46% subangular to subrounded limestone gravel to 1.75". Moderate to well cemented.	
	4.57	3C	MC	50/88	50/88	60	SV, PI, Dens		GW GM		
723.47	5										
722.47	6 6.10 6.25	3D	SPT	50/25	50/25	100			5.49	Silty Sand with Gravel ; light grey brown, dry, very dense, with 13% low plastic fines, 49% fine to coarse sand, 38% subangular limestone gravel to 2.5". Moderately cemented.	
	6.71	3D'	GRAB			50	SV, PI, Dens				
721.47	7								SM		
	7.62	3E	MC	50/75	50/75	0					
720.47	8										
719.47	9 9.14 9.30	3F	SPT	50/25	50/25	100			8.84	Silty, Clayey Sand with Gravel ; light brown, dry, very dense, with 15% low plastic fines, 52% fine to coarse sand, 33% subangular to subrounded limestone gravel to 1". Moderate to well cemented.	
	9.75	3F'	GRAB			50	SV, PI, Dens				



EXPLORATION LOG

SHEET 2 OF 3

START DATE 7/21/01
 END DATE 7/21/01
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-03
 E.A. # 0324-01-1
 GROUND ELEV. 728.47 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>7/21/01</u>	<u>NE</u>	

STATION 92+26 Q
 OFFSET 65 LT
 ENGINEER PGT
 EQUIPMENT Foremost B90
 OPERATOR Eagle Drilling
 DRILLING METHOD 203 mm HS Auger
 BACKFILLED Yes DATE 7/21/2001

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
	10.67	3G	MC	50/62	50/62	60			
717.47	11						SC		
716.47	12						SM		
12.19	12.34	3H	SPT	50/25	50/25	0			
12.80		3H'	GRAB			50	SV, PI, Dens		
715.47	13							13.11	
13.72	13.72	3I	MC	50/50	50/50	100	SV, PI, Dens		
714.47	14								
713.47	15								
15.24	15.39	3J	SPT	50/62	50/62	0			
15.85		3J'	GRAB			50	SV, PI, Dens		
712.47	16						SM		
16.76	16.76	3K	MC	50/25	50/25	0			
711.47	17								
710.47	18								
18.29	18.44	3L	SPT	50/25	50/25	0			
18.90		3L'	GRAB			50			
709.47	19								
19.81	19.81	3M	MC	50/38	50/38	0			

START DATE 7/21/01END DATE 7/21/01JOB DESCRIPTION US 95 Widening / Project 2D Retaining WallsLOCATION Las Vegas, NevadaBORING B-03E.A. # 0324-01-1GROUND ELEV. 728.47 (m)HAMMER DROP SYSTEM Cable**EXPLORATION LOG**

SHEET 3 OF 3

STATION	92+26 Q	
OFFSET	65 LT	
ENGINEER	PGT	
EQUIPMENT	Foremost B90	
OPERATOR	Eagle Drilling	
DRILLING METHOD	203 mm HS Auger	
BACKFILLED	Yes	DATE <u>7/21/2001</u>

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
7/21/01	NE	

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
707.47	21								
	21.34	3N	SPT	50/38	50/38	0			
	21.49								
706.47	22								
	21.95	3N'	GRAB			50			
705.47	23							22.86	
704.47	24								
703.47	25								
702.47	26								
701.47	27								
700.47	28								
699.47	29								



EXPLORATION LOG

SHEET 1 OF 3

START DATE 7/21/01
 END DATE 7/21/01
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-04
 E.A. # 0324-01-1
 GROUND ELEV. 725.12 (m)
 HAMMER DROP SYSTEM Cable

STATION 91+30 Q
 OFFSET 35 LT
 ENGINEER PGT
 EQUIPMENT Foremost B90
 OPERATOR Eagle Drilling
 DRILLING METHOD 203 mm HS Auger
 BACKFILLED Yes DATE 7/21/2001

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm					
724.12	1							GM	Silty Gravel with Sand ; light grey brown, dry, very dense, with estimated 15-20% low plastic fines, 35-40% fine to coarse sand, 45-50% subangular limestone gravel to 3". 5-10% oversize to 5". Moderately cemented with weak caliche coating on cobbles.	
	1.52	4A	MC	50/50	50/50	100		SP	Poorly Graded Sand with Silt and Gravel ; light grey brown, dry, very dense, with 10% low plastic fines, 49% fine to coarse sand, 41% subangular limestone gravel to 2". Moderate to well cemented. Gravel is sheared by the auger. Calcareous cement throughout hole.	
	1.68							SM		
723.12	2	4A'	GRAB			50	SV, PI, Dens			
	2.13									
722.12	3	3.05	4B	SPT	50/25	50/25	0	GW	Well Graded Gravel with Silt and Sand ; light grey brown, dry, very dense, with 10% low plastic fines, 43% fine to coarse sand, 48% subangular limestone gravel to 2". Moderate to well cemented.	
	3.20							GM		
	3.66	4B'	GRAB			50	SV, PI, Dens			
721.12	4									
	4.57	4C	MC	50/25	50/25	0				
720.12	5							GM	Silty Gravel with Sand ; light brown grey, dry, very dense, with estimated 15-20% low plastic fines, 35-40% fine to coarse sand, 45-50% subangular to subrounded limestone gravel to 1". Moderately cemented.	
719.12	6	6.10	4D	SPT	50/62	50/62	0			
	6.25							GM		
	6.71	4D'	GRAB			50				
718.12	7									
	7.62	4E	MC	50/50	50/50	100	SV, PI, Dens		Clayey Sand with Gravel ; light brown, dry, very dense, with 19% medium plastic fines, 51% fine to coarse sand, 30% subangular limestone gravel to 1". Moderate to well cemented.	
717.12	8									
716.12	9	9.14	4F	SPT	50/62	50/62	60	SV, PI, Dens		
									Samples 4F and 4H were combined for the lab analysis.	



EXPLORATION LOG

SHEET 2 OF 3

START DATE 7/21/01
 END DATE 7/21/01
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-04
 E.A. # 0324-01-1
 GROUND ELEV. 725.12 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>7/21/01</u>	<u>NE</u>	

STATION 91+30 Q
 OFFSET 35 LT
 ENGINEER PGT
 EQUIPMENT Foremost B90
 OPERATOR Eagle Drilling
 DRILLING METHOD 203 mm HS Auger
 BACKFILLED Yes DATE 7/21/2001

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
10.67										
10.67		4G	MC	50/25	50/25	0				
714.12	11									
713.12	12	12.19	4H	SPT	50/100	50/100	75	SV, PI, Dens		
712.12	13									
712.12	13									
13.72		4I	MC	50/88	50/88	0				
711.12	14									
710.12	15									
15.24		4J	SPT	50/62	50/62	100				
709.12	16									
16.76		4K	MC	50/62	50/62	0				
708.12	17									
707.12	18									
18.29		4L	SPT	50/50	50/50	0				
706.12	19									
19.81		4M	MC	50/75	50/75	0				



EXPLORATION LOG

SHEET 3 OF 3

START DATE 7/21/01
END DATE 7/21/01
JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
LOCATION Las Vegas, Nevada
BORING B-04
E.A. # 0324-01-1
GROUND ELEV. 725.12 (m)
HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>7/21/01</u>	<u>NE</u>	

STATION 91+30 Q
OFFSET 35 LT
ENGINEER PGT
EQUIPMENT Foremost B90
OPERATOR Eagle Drilling
DRILLING METHOD 203 mm HS Auger
BACKFILLED Yes DATE 7/21/2001

ELEV. (m)	DEPTH (m)	SAMPLE			BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd					
704.12	21										
21.34	4N	SPT	50/62	50/62	60						
703.12	22										
22.86	4O	MC	50/38	50/38	0		22.86				
702.12	23										
701.12	24										
700.12	25										
699.12	26										
698.12	27										
697.12	28										
696.12	29										



EXPLORATION LOG

SHEET 1 OF 3

START DATE 11/8/01
 END DATE 11/8/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-5
 E.A. # 0324-01-2
 GROUND ELEV. 730.61 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/8/01</u>	<u>NE</u>	

STATION 14+40 R
 OFFSET 27 LT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/8/2001

ELEV. (m)	DEPTH (m)	SAMPLE NO.	TYPE	BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
				150 mm Increments	Last 300 mm					
729.61	1.07	A	SPT	50/25	50/25	5		GP GM	POORLY GRADED GRAVEL with SILT and SAND light brown, dry, very dense, with 6% nonplastic fines, 29% fine to coarse sand and 65% fine to coarse subangular gravel to 2". Cobbles to 4" comprise an estimated 20% of the unit mass.	Previously reported as boring B-A. Poor sample return on SPT and MC samples
	1.22	A'	GRAB			50	PI, SI, MC			
	1.68									
728.61	2									
	2.59	B	MC	75/50	75/50	11				
	2.74	B'	GRAB			50	PI, SI, MC, SH, CHEM			
727.61	3									
	3.20									
726.61	4	C	ST	50/25	50/25	1				
	4.11									
	4.27	C'	GRAB			50	PI, SI, MC			
725.61	5							GP GC		
	5.64	D	MC	75/25	75/25	5				
	5.79									
724.61	6	D'	GRAB			50	PI, SI, MC			
	6.25									
723.61	7	E	ST	50/25	50/25	5		8.23		
	7.16									
722.61	8									
	8.69	F	MC	75/40	75/40	10			SILTY, CLAYEY SAND with GRAVEL light brown, slightly moist, very dense, with 2% nonplastic fines, 46% fine to coarse sand and 42% fine to coarse subrounded gravel to 3". Cobbles to 4" comprise an estimated 10% of the unit mass.	
721.61	9									



EXPLORATION LOG

SHEET 2 OF 3

START DATE 11/8/01
 END DATE 11/8/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-5
 E.A. # 0324-01-2
 GROUND ELEV. 730.61 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/8/01</u>	<u>NE</u>	

STATION 14+40 R
 OFFSET 27 LT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/8/2001

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
719.61	11	10.21	G SPT	50/50	50/50	11		SC SM	POORLY GRADED GRAVEL with SILT and SAND tan, slightly moist, very dense, with 10-20% nonplastic fines, 30% fine to coarse sand and 50-55% fine to coarse surrounded gravel to 1/2". Trace cobbles to 4".	
718.61	12	11.73	H MC	75/50	75/50	11				
718.61	12	11.89	H GRAB			50	PI, SI, MC			
717.61	13	12.34								
716.61	14	14.78	I MC	75/50	75/50	11				
715.61	15									
714.61	16									
713.61	17									
712.61	18	17.83	J SPT	50/125	50/125	28				
711.61	19									



EXPLORATION LOG

SHEET 3 OF 3

START DATE 11/8/01END DATE 11/8/01JOB DESCRIPTION US 95 - Rainbow Blvd InterchangeSTATION 14+40 RLOCATION Las Vegas, NevadaOFFSET 27 LTBORING B-5ENGINEER MAME.A. # 0324-01-2EQUIPMENT Diedrich D-50 turboGROUND ELEV. 730.61 (m)OPERATOR Eagle DrillingHAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/8/01</u>	<u>NE</u>	

DRILLING METHOD 152 mm HS AugerBACKFILLED Yes DATE 11/8/2001

ELEV. (m)	DEPTH (m)	SAMPLE					LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	BLOW COUNT		Percent Recov'd				
				150 mm Increments	Last 300 mm					
709.61	21	K	MC	75/25	75/25	5				
708.61	22	L	MC	75/50	75/50	11			22.86	
707.61	23									
706.61	24									
705.61	25									
704.61	26									
703.61	27									
702.61	28									
701.61	29									



EXPLORATION LOG

SHEET 1 OF 3

START DATE 11/8/01
 END DATE 11/8/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-6
 E.A. # 0324-01-2
 GROUND ELEV. 726.95 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/8/01</u>	<u>NE</u>	

STATION 14+50 R
 OFFSET 15 LT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/8/2001

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
725.95	1 1.07	A	SPT	50/25	50/25	5	GP	POORLY GRADED GRAVEL with SILT and SAND grey-brown, dry, medium dense, with estimated 90% fine to coarse gravel, 10% coarse sand and 90% fine to coarse subrounded gravel. Cobbles to 4" comprise an estimated 20% of the unit mass. Loose weak cementation gravels at surface.	Previously reported as boring B-B.
	1.22						GW		
	1.68	A'	GRAB			50	GM	WELL GRADED GRAVEL with SILT and SAND light brown, dry to slightly moist, very dense, with 10% nonplastic fines, 41% fine to coarse sand and 49% fine to coarse subrounded gravel to 2".	
724.95	2						1.92	POORLY GRADED GRAVEL with SILT and SAND tan, moist, very dense with 2% nonplastic fines, 42% fine to coarse sand and 47% fine subrounded gravel to 1-1/2".	
	2.59	B	MC	75/25	75/25	5	GW		
	2.74						GM		
723.95	3	B'	GRAB			50	PI, SI, MC, SH, CHEM		
	3.20								
722.95	4 4.11	C	SPT	50/25	50/25	5	GP	WELL GRADED GRAVEL with SILT and SAND light brown, dry to slightly moist, very dense with 10% nonplastic to very low plasticity fines, 41% fine to coarse sand and 49% fine to coarse subrounded gravel to 2".	
	4.27						GM		
	4.72	C'	GRAB			50	PI, SI, MC,		
721.95	5						3.66		
	5.64	D	MC	75/25	75/25	5	GW		
	5.79						GM		
720.95	6	D'	GRAB			50	PI, SI, MC,	POORLY GRADED GRAVEL with SILTY CLAY and SAND light brown, dry, very dense, with 11% nonplastic to very low plasticity fine, 52% fine to coarse gravel and 36% coarse sand and 52% fine to coarse subrounded limestone gravel to 3". Cobbles to 4" comprise an estimated 20% of the unit mass.	
	6.25						GP		
719.95	7	E	SPT	50/25	50/25	5	GC		
	7.16						4.97		
718.95	8						GP		
	8.69	F	MC	75/25	75/25	5	GC	WELL GRADED GRAVEL with SILT and SAND light brown, dry to slightly moist, very dense, with 13% nonplastic fines, 42% fine to coarse sand and 45% fine to coarse subrounded limestone gravel to 3".	
717.95	9								



EXPLORATION LOG

SHEET 2 OF 3

START DATE 11/8/01
 END DATE 11/8/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-6
 E.A. # 0324-01-2
 GROUND ELEV. 726.95 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/8/01</u>	<u>NE</u>	

STATION 14+50 R
 OFFSET 15 LT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/8/2001

ELEV. (m)	DEPTH (m)	SAMPLE					LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
10.21	G	SPT	50/60	50/60	12			GM		
715.95	11									
11.73	H	MC	75/0	75/0	0					
11.89										
714.95	12	H'	GRAB			50	PI, SI, MC,			
12.34										
713.95	13									
13.17									WELL GRADED GRAVEL with SILT and SAND tan, dry to slightly moist, very dense, with estimated 10% nonplastic fines, 40% fine to coarse sand and 50% fine to coarse subrounded gravel to 2"	
712.95	14									
14.78	I	SPT	50/25	50/25	5					
711.95	15							GP GM		
710.95	16									
709.95	17									
17.83	J	MC	75/50	75/50	11					
708.95	18									
707.95	19									



EXPLORATION LOG

SHEET 3 OF 3

START DATE 11/8/01

END DATE 11/8/01

JOB DESCRIPTION US 95 - Rainbow Blvd Interchange

LOCATION Las Vegas, Nevada

BOBING B-6

F.A. # 0324

GROUND ELEV. 726.95 (m)

HAMMER PROOF SYSTEM: Ca

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
11/8/01	NE	

STATION	14+50 R
OFFSET	15 LT
ENGINEER	MAM
EQUIPMENT	Diedrich D-50 turbo
OPERATOR	Eagle Drilling
DRILLING METHOD	152 mm HS Auger
BACKFILLED	Yes DATE 11/8/2001



EXPLORATION LOG

SHEET 1 OF 4

START DATE 11/9/01
 END DATE 11/9/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-7
 E.A. # 0324-01-2
 GROUND ELEV. 733.04 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/9/01</u>	<u>NE</u>	

STATION 14+50 R
 OFFSET 90 RT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/9/2001

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS		
		NO.	TYPE	150 mm Increments	Last 300 mm						
732.04	1 1.07	A	SPT	50/25	50/25	5	GW GC	WELL GRADED GRAVEL with SILTY CLAY and SAND tan, slightly moist, very dense, with 11% nonplastic to low plasticity fines, 42% fine to coarse sand and 47% fine subrounded gravel to 1-1/2". Moderate calcareous cementation.	Previously reported as boring B-C.		
	1.22										
	1.68	A'	GRAB			50					
	2						GC				
	2.59	B	MC	75/25	75/25	5					
	2.74										
	3 3.20	B'	GRAB			50					
	4 4.11	C	SPT	50/25	50/25	5	SC SM				
	4.27										
	4.72	C'	GRAB			50					
729.04	5						SM				
	5.64	D	MC	75/25	75/25	5					
	5.79										
	6 6.25	D'	GRAB			50					
	7 7.16	E	ST	50/25	50/25	5					
	8										
	8.69	F	MC	75/25	75/25	5					
	9										



EXPLORATION LOG

SHEET 2 OF 4

START DATE	11/9/01	STATION	14+50 R
END DATE	11/9/01	OFFSET	90 RT
JOB DESCRIPTION	US 95 - Rainbow Blvd Interchange	ENGINEER	MAM
LOCATION	Las Vegas, Nevada	EQUIPMENT	Diedrich D-50 turbo
BORING	B-7	OPERATOR	Eagle Drilling
E.A. #	0324-01-2	DRILLING METHOD	152 mm HS Auger
GROUND ELEV.	733.04 (m)	BACKFILLED	Yes DATE 11/9/2001
HAMMER DROP SYSTEM	Cable		

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
	10.21	G	SPT	50/50	50/50	11	GC GM		
722.04	11								
721.04	11.73	H	MC	75/25	75/25	5			
	12								
	12.19								
	12.65	H'	GRAB			50	PI, SI, MC,		
720.04	13								
719.04	14								
718.04	14.78	I	SPT	50/25	50/25	5			
	15								
717.04	16								
716.04	17								
715.04	17.83	J	MC	75/25	75/25	5			
	18								
	18.29								
	18.75	J'	GRAB			50	PI, SI, MC,		
714.04	19								



EXPLORATION LOG										SHEET 3 OF 4	
START DATE	11/9/01			STATION	14+50 R						
END DATE	11/9/01			OFFSET	90 RT						
JOB DESCRIPTION	US 95 - Rainbow Blvd Interchange			ENGINEER	MAM						
LOCATION	Las Vegas, Nevada			EQUIPMENT	Diedrich D-50 turbo						
BORING	B-7			OPERATOR	Eagle Drilling						
E.A. #	0324-01-2			DRILLING METHOD	152 mm HS Auger						
GROUND ELEV.	733.04 (m)			BACKFILLED	Yes DATE 11/9/2001						
HAMMER DROP SYSTEM Cable				GROUNDWATER LEVEL							
		DATE	DEPTH m	ELEV. m							
		11/9/01	NE								

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION				REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd							
712.04	21	K	SPT	50/25	50/25	5							
711.04	22												
710.04	23												
709.04	24	L	MC	75/25	75/25	5	PI, SI, MC,						
708.04	25												
707.04	26												
706.04	27	M	SPT	50/50	50/50	11		SM					
705.04	28												
704.04	29												
	30.02												



EXPLORATION LOG

SHEET 4 OF 4

START DATE 11/9/01END DATE 11/9/01JOB DESCRIPTION US 95 - Rainbow Blvd InterchangeLOCATION Las Vegas, NevadaBORING B-7E.A. # 0324-01-2GROUND ELEV. 733.04 (m)HAMMER DROP SYSTEM Cable

STATION	<u>14+50 R</u>	
OFFSET	<u>90 RT</u>	
ENGINEER	<u>MAM</u>	
EQUIPMENT	<u>Diedrich D-50 turbo</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>152 mm HS Auger</u>	
BACKFILLED	<u>Yes</u>	DATE <u>11/9/2001</u>

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/9/01</u>	<u>NE</u>	

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
702.04	31	N	MC	75-50mm	75-50mm	0			30.48	
701.04	32									
700.04	33									
699.04	34									
698.04	35									
697.04	36									
696.04	37									
695.04	38									
694.04	39									



EXPLORATION LOG

SHEET 1 OF 3

START DATE	11/6/01	STATION	93+88 Q
END DATE	11/6/01	OFFSET	103 LT
JOB DESCRIPTION	US 95 - Rainbow Blvd Interchange	ENGINEER	MAM
LOCATION	Las Vegas, Nevada	EQUIPMENT	Diedrich D-50 turbo
BORING	B-8	OPERATOR	Eagle Drilling
E.A. #	0324-01-2	DRILLING METHOD	152 mm HS Auger
GROUND ELEV.	737.62 (m)	BACKFILLED	Yes DATE 11/6/2001
HAMMER DROP SYSTEM	Cable		

ELEV. (m)	DEPTH (m)	SAMPLE						LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd					
736.62	1 1.07									SILTY, CLAYEY GRAVEL with SAND light brown, slightly moist, dense to very dense, with estimated 20% low plasticity fines, 35% fine to coarse sand and 45% fine subangular limestone gravel to 1-1/2".	Previously reported as boring B-D.
	1.22	A	SPT	46	50/50	44					
735.62	2										
	2.59										
	2.74	B	MC	75/100	75/100	0					
734.62	3										
733.62	4 4.11										
	4.27	C	SPT	49	50/75	50					
732.62	5										
	5.64										
	5.79	D	MC	50/125	50/125	28					
731.62	6										
730.62	7 7.16										
	7.32	E	SPT	50/100	50/100	22					
729.62	8										
	8.69										
	8.84	F	MC	50/100	50/100	100	PI, SI, MC,				
728.62	9										

EXPLORATION LOG

SHEET 2 OF 3



START DATE 11/6/01
 END DATE 11/6/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-8
 E.A. # 0324-01-2
 GROUND ELEV. 737.62 (m)
 HAMMER DROP SYSTEM Cable

STATION	<u>93+88 Q</u>	
OFFSET	<u>103 LT</u>	
ENGINEER	<u>MAM</u>	
EQUIPMENT	<u>Diedrich D-50 turbo</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>152 mm HS Auger</u>	
BACKFILLED	<u>Yes</u>	DATE <u>11/6/2001</u>

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS	
		NO.	TYPE	150 mm Increments	Last 300 mm					
	10.21									
	10.36	G	SPT	50/25	50/25	5				
726.62	11						GC GM	CLAYEY SAND with GRAVEL light brown, slightly moist to moist, very dense with 14% low plasticity fines, 65% fine to coarse sand and 21% fine to coarse subrounded limestone gravel to 2".		
	11.73									
	11.89	H	MC	75/40	75/40	10				
725.62	12									
	13									
724.62	14									
	14.78									
722.62	14.94	I	SPT	50/25	50/25	5				
	15									
	16						SC	16.46		
721.62	17									
	17.83									
719.62	17.98	J	MC	75/25	75/25	5		18.29	CLAYEY GRAVEL with SAND light brown, slightly moist, very dense, with estimated 20% low to medium plasticity fines, 35% fine to coarse sand and 45% fine subangular limestone gravel to 1". Moderate cementation.	
	18									
718.62	19									



EXPLORATION LOG

SHEET 3 OF 3

START DATE 11/6/01

END DATE 11/6/01

JOB DESCRIPTION US 95 - Rainbow Blvd Interchange

LOCATION Las Vegas, Nevada

BORING B-8

E.A. # 0324-01-2

GROUND ELEV. 737.62 (m)

HAMMER DROP SYSTEM Cable

STATION	93+88 Q
OFFSET	103 LT
ENGINEER	MAM
EQUIPMENT	Diedrich D-50 turbo
OPERATOR	Eagle Drilling
DRILLING METHOD	152 mm HS Auger
BACKFILLED	Yes DATE 11/6/2001

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
716.62	20.88	21.03	K ST	50/25	50/25	5		SC		
715.62	22	22.40	L MC	75/25	75/25	5				
714.62	23	22.86								
713.62	24									
712.62	25									
711.62	26									
710.62	27									
709.62	28									
708.62	29									



EXPLORATION LOG

SHEET 1 OF 3

START DATE 11/7/01
 END DATE 11/7/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-9
 E.A. # 0324-01-2
 GROUND ELEV. 723.90 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/7/01</u>	<u>NE</u>	

STATION 13+35 R
 OFFSET 15 RT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/7/2001

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
722.90	1 1.07	A	SPT	50/25	50/25	5	GP GC	POORLY GRADED GRAVEL with SILTY CLAY and SAND light brown, slightly moist, dense to very dense, with 10% low to medium plasticity fines, 35% fine to coarse sand and 55% fine to coarse limestone gravel to 3". Cobbles to 4" comprise an estimated 15% of the unit mass. Moderate cementation.	Previously reported as boring B-E.
	1.22								
	1.68	A'	GRAB			50	PI, SI, MC		
721.90	2						GW GC	WELL GRADED GRAVEL with CLAY and SAND light brown, slightly moist, very dense, with 11% low plasticity fines, 43% fine to coarse sand and 46% fine subangular limestone gravel to 3/4". Moderate cementation.	
	2.59	B	MC	75/100	75/100	11			
720.90	3 3.20	B'	GRAB			50	PI, SI, MC, SH, CHEM	3.05	CLAYEY SAND with GRAVEL light brown-grey, slightly moist, very dense, with estimated 14% medium to high plasticity fines, 43% fine to coarse sand and 42% fine to coarse subangular limestone gravel to 3". Unit contains an estimated 10% subangular cobbles to 4". Moderate cementation.
719.90	4 4.11	C	SPT	50/15	50/15	3	SC	5.18	
	4.27								
	4.72	C'	GRAB			50	PI, SI, MC		
718.90	5						SC SM	SILTY, CLAYEY SAND with GRAVEL tan-light brown, slightly moist to moist, very dense, with 13% low plasticity fines, 60% fine to coarse sand and 27% fine to coarse subrounded limestone gravel to 2". Moderate calcareous cementation.	
	5.64	D	MC	50/25	50/25	5			
717.90	6 6.25	D'	GRAB			50	PI, SI, MC	6.40	CLAYEY SAND with GRAVEL light brown-tan, slightly moist to moist, very dense, with 17-21% medium plasticity fines, 49-50% fine to coarse sand and 29-33% fine to coarse gravel to 3". Moderate cementation.
716.90	7 7.16	E	SPT	50/125	50/125	28	SC		
715.90	8								
	8.69	F	MC	75/50	75/50	11			
714.90	9								



EXPLORATION LOG

SHEET 2 OF 3

START DATE 11/7/01

END DATE 11/7/01

JOB DESCRIPTION US 95 - Rainbow Blvd Interchange

LOCATION Las Vegas, Nevada

BORING B-9

FA # 0324-01-2

GROUND ELEV 723.90 (m)

HAMMER DROP SYSTEM

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
11/7/01	NE	

13+35 R

15 RT

ENGINEER MAM

EQUIPMENT Diedrich D-50 turbo

OPERATOR Eagle Drilling

**DRILLING
METHOD** 152 mm HS Auger

RECEIVED BY: Yes DATE: 11/7/2001



EXPLORATION LOG

SHEET 3 OF 3

START DATE 11/7/01

END DATE 11/7/01

JOB DESCRIPTION US 95 - Rainbow Blvd Interchange

LOCATION Las Vegas, Nevada

BORING B-9

E A # 0324-01-2

GROUND ELEV. 723.90 (m)

HAMMER DROP SYSTEM Cable

HAMMER DROF SYSTEM

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
11/7/01	NE	

STATION

13+35 R

OFFSET

15 RT

ENGINEER

MAM

EQUIPMENT

Diedrich D-50

OPERATOR

Eagle Drilling

DRILLING METHOD

152 mm HS A

METHOD

Yes _____ 11/1

BACK TEELE

750 DATE 7/7



EXPLORATION LOG

SHEET 1 OF 3

START DATE 11/6/01
 END DATE 11/6/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-10
 E.A. # 0324-01-2
 GROUND ELEV. 729.39 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/6/01</u>	<u>NE</u>	

STATION 12+55 R
 OFFSET 33 RT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/6/2001

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
728.39	0.00	A	MC	75/50	75/50	11	SC SM	SILTY, CLAYEY SAND with GRAVEL light brown, slightly moist, very dense, with 14% low plasticity fines, 50% fine to coarse sand and 36% fine to coarse subangular limestone gravels to 1-1/2". Moderate calcareous cementation.	Previously reported as boring B-F.
	0.30								
	0.76	A'	GRAB			50			
	1.07	B	SPT	50/25	50/25	5			
	1.22								
	1.68	B'	GRAB			50			
	2								
	2.59	C	MC	75/50	75/50	11			
	2.74								
	3	C'	GRAB			50			
726.39	3.20								
	4	D	SPT	50/50	50/50	11	SW SC	WELL GRADED SAND with CLAY and GRAVEL light brown, slightly moist, very dense, with 9% low to medium plasticity fines, 71% fine to coarse sand and 30% fine to coarse subangular limestone gravels to 1-1/2". Well cemented; difficult drilling.	Previously reported as boring B-F.
	4.11								
	4.27	D'	GRAB			50			
	4.72								
	5								
	5.64	E	MC	75/75	75/75	17			
	5.79								
	6	E'	GRAB			50			
	6.25								
724.39	7	F	ST	50/15	50/15	2	GW GM	WELL GRADED GRAVEL with SILT and SAND tan, slightly moist, very dense, with 10% low plasticity fines, 42% fine to coarse sand and 48% fine to coarse subangular limestone gravels to 2". Well cemented; difficult drilling.	Previously reported as boring B-F.
	7.16								
	8								
	8.69	G	MC	75/15	75/15	2			
	9								



EXPLORATION LOG

SHEET 2 OF 3

START DATE 11/6/01
 END DATE 11/6/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-10
 E.A. # 0324-01-2
 GROUND ELEV. 729.39 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/6/01</u>	<u>NE</u>	

STATION 12+55 R
 OFFSET 33 RT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/6/2001

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
	10.21	H	ST	50/25	50/25	5			
718.39	11						GP GM		
	11.73	I	MC	75/25	75/25	5			
717.39	12								
716.39	13								
715.39	14								
	14.78	J	SPT	50/50	50/50	11			
714.39	15								
713.39	16								
712.39	17								
	17.83	K	MC	75/50	75/50	11		CLAYEY SAND with GRAVEL light brown, moist, very dense, with 13-16% low to medium plasticity fines, 54-60% fine to coarse sand and 24-33% fine to coarse subrounded limestone gravel to 1". Moderate cementation.	
711.39	18						SC		
710.39	19								



EXPLORATION LOG

SHEET 3 OF 3

START DATE	11/6/01	EXPLORATION LOG		
END DATE	11/6/01			
JOB DESCRIPTION	US 95 - Rainbow Blvd Interchange			
LOCATION	Las Vegas, Nevada			
BORING	B-10			
E.A. #	0324-01-2			
GROUND ELEV.	729.39 (m)			
HAMMER DROP SYSTEM	Cable			
GROUNDWATER LEVEL				
DATE	DEPTH m	ELEV. m		
11/6/01	NE			

STATION	12+55 R
OFFSET	33 RT
ENGINEER	MAM
EQUIPMENT	Diedrich D-50 turbo
OPERATOR	Eagle Drilling
DRILLING METHOD	152 mm HS Auger
BACKFILLED	Yes DATE 11/6/2001



EXPLORATION LOG

SHEET 1 OF 3

START DATE 11/7/01
 END DATE 11/7/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-11
 E.A. # 0324-01-2
 GROUND ELEV. 723.90 (m)
 HAMMER DROP SYSTEM Cable

STATION	<u>91+68 Q</u>	
OFFSET	<u>31 RT</u>	
ENGINEER	<u>MAM</u>	
EQUIPMENT	<u>Diedrich D-50 turbo</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>152 mm HS Auger</u>	
BACKFILLED	<u>Yes</u>	DATE <u>11/7/2001</u>

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
722.90	1.07	A	ST	50/25	50/25	5	GM	POORLY GRADED GRAVEL with SILT and SAND light brown-tan, slightly moist, very dense, with 7% nonplastic fines, 43% fine to coarse sand and 50% fine subangular limestone gravel to 1". Moderate cementation.	Previously reported as boring B-G.
	1.22	A'	GRAB			50			
	1.68					PI, SI, MC			
721.90	2						SW SC	WELL GRADED SAND with SILTY CLAY and SAND light brown, slightly moist, very dense with 11% low plasticity fines, 54% fine to coarse sand and 35% fine surrounded limestone gravel to 3/4". Moderate calcareous cementation.	
	2.59	B	MC	75/25	75/25	5			
	2.74	B'	GRAB			50			
720.90	3					PI, SI, MC, SH, CHEM	GW GC	WELL GRADED GRAVEL with SILTY CLAY and SAND light tan, moist, very dense, with 10% low plasticity fines, 39% fine to coarse sand and 51% fine subangular limestone gravel to 1/2". Moderate cementation.	
	3.20								
	4.11	C	ST	50/50	50/50	11			
719.90	4.27	C'	GRAB			50	SW SC	WELL GRADED SAND with CLAY and GRAVEL light brown, moist, very dense with estimated 20% low plasticity fines, 35-40% fine to coarse sand and 40-45% fine subangular limestone gravel to 3/4". Moderate cementation.	
	4.72					PI, SI, MC			
	5								
718.90	5.64	D	MC	75/38	75/38	10	GW GC	CLAYEY SAND with GRAVEL light brown, moist, very dense, with 14-21% low plasticity fines, 44-65% fine to coarse sand and 18-42% fine surrounded limestone gravel to 1". Moderate cementation.	
	5.79	D'	GRAB			50			
	6.25					PI, SI, MC			
717.90	6						SW SC		
	7.16	E	ST	50/100	50/100	22			
	8					PI, SI, MC			
716.90	8.69	F	MC	75/125	75/125	28	GW GC		
	9					PI, SI, MC			



EXPLORATION LOG

SHEET 2 OF 3

START DATE	11/7/01
END DATE	11/7/01
JOB DESCRIPTION	US 95 - Rainbow Blv
LOCATION	Las Vegas, Nevada
BORING	B-11
E.A. #	0324-01-2
GROUND ELEV.	723.90 (m)
HAMMER DROP SYSTEM	Cable

STATION	91+68 Q
OFFSET	31 RT
ENGINEER	MAM
EQUIPMENT	Diedrich D-50 turbo
OPERATOR	Eagle Drilling
DRILLING METHOD	152 mm HS Auger
BACKFILLED	Yes DATE 11/7/2001



EXPLORATION LOG

SHEET 3 OF 3

START DATE 11/7/01END DATE 11/7/01JOB DESCRIPTION US 95 - Rainbow Blvd InterchangeLOCATION Las Vegas, NevadaBORING B-11E.A. # 0324-01-2GROUND ELEV. 723.90 (m)HAMMER DROP SYSTEM Cable

STATION	<u>91+68 Q</u>	
OFFSET	<u>31 RT</u>	
ENGINEER	<u>MAM</u>	
EQUIPMENT	<u>Diedrich D-50 turbo</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>152 mm HS Auger</u>	
BACKFILLED	<u>Yes</u>	DATE <u>11/7/2001</u>

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/7/01</u>	<u>NE</u>	

ELEV. (m)	DEPTH (m)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
				150 mm Increments	Last 300 mm	Percent Recov'd				
702.90	20.88	K	ST	50/25	50/25	5			moist, very dense, with 23% low plasticity fines, 67% fine to coarse sand and 10% fine to coarse subangular gravel to 2". Moderate calcareous cementation.	
	21									
	21.34									
	21.79	K'	GRAB			50				
701.90	22									
	22.40	L	MC	75/50	75/50	11				
	22.86									
700.90	23									
699.90	24									
698.90	25									
697.90	26									
696.90	27									
695.90	28									
694.90	29									



EXPLORATION LOG

SHEET 1 OF 3

START DATE 11/7/01
 END DATE 11/7/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-12
 E.A. # 0324-01-2
 GROUND ELEV. 723.90 (m)
 HAMMER DROP SYSTEM Cable

STATION	<u>93+15 Q</u>	
OFFSET	<u>60 RT</u>	
ENGINEER	<u>MAM</u>	
EQUIPMENT	<u>Diedrich D-50 turbo</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>152 mm HS Auger</u>	
BACKFILLED	<u>Yes</u>	DATE <u>11/7/2001</u>

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			Percent Reco'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm						
722.90	1 1.07	A	ST	50/50	50/50	11			GP GM	<p>CLAYEY GRAVEL with SAND light brown, lightly moist, very dense, with estimated 15% low plasticity and nonplastic fines, 35% fine to coarse sand and 50% fine subangular limestone gravel to 3/4". Moderate cementation.</p> <p>2.44</p> <p>WELL GRADED GRAVEL with SILT and SAND light brown, slightly moist, very dense, with 9-10% nonplastic fines, 40-44% fine to coarse sand and 47-51% fine subrounded limestone gravel to 1". Moderate calcareous cementation.</p>	Previously reported as boring B-H.
	1.22	A'	GRAB			50	PI, SI, MC, SH, CHEM				
	1.68										
	2										
	2.59	B	MC	75/50	75/50	11					
	2.74	B'	GRAB			50	PI, SI, MC				
	3										
	3.20										
	4 4.11	C	SPT	50/25	50/25	5					
	4.27	C'	GRAB			50	PI, SI, MC				
718.90	5								GW GM	<p>6.10</p> <p>WELL GRADED GRAVEL with SILTY CLAY and SAND tan, slightly moist to moist, very dense, with 12% low plasticity fines, 42% fine to coarse sand and 47% fine to coarse subrounded limestone gravel to 2". Moderate cementation.</p>	
	5.64	D	MC	75/25	75/25	5					
	5.79	D'	GRAB			50	PI, SI, MC				
	6										
	6.25										
	7 7.16	E	SPT	50/25	50/25	5					
	8										
	8.69	F	MC	75/63	75/63	12					
	9										

JOB : GDT : GPU : DOT



EXPLORATION LOG

SHEET 2 OF 3

START DATE 11/7/01
 END DATE 11/7/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-12
 E.A. # 0324-01-2
 GROUND ELEV. 723.90 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/7/01</u>	<u>NE</u>	

STATION 93+15 Q
 OFFSET 60 RT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/7/2001

ELEV. (m)	DEPTH (m)	SAMPLE				LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
	10.21	G	SPT	50/50	50/50	11	GC	POORLY GRADED GRAVEL with SILT and SAND light brown, slightly moist to moist, very dense, with estimated 10% nonplastic fines, 35% fine to coarse sand and 55% fine surrounded limestone gravel to 2". Moderate cementation.	
712.90	11								
	11.73	H	MC	75/50	75/50	11			
711.90	11.89								
	12	H'	GRAB			40			
	12.34								
710.90	13								
	14								
709.90	14								
	14.78	I	SPT	50/25	50/25	5			
708.90	15						GP GM		
707.90	16								
706.90	17								
	17.83	J	MC	75/75	75/75	17			
705.90	18								
704.90	19								



EXPLORATION LOG

SHEET 3 OF 3

START DATE 11/7/01END DATE 11/7/01JOB DESCRIPTION US 95 - Rainbow Blvd InterchangeSTATION 93+15 QOFFSET 60 RTENGINEER MAMEQUIPMENT Diedrich D-50 turboOPERATOR Eagle DrillingDRILLING METHOD 152 mm HS AugerBACKFILLED Yes DATE 11/7/2001LOCATION Las Vegas, NevadaBORING B-12E.A. # 0324-01-2GROUND ELEV. 723.90 (m)HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL

DATE 11/7/01 DEPTH m NE ELEV. m

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd						
702.90	21	K	SPT	50/50	50/50	11				
701.90	22									
700.90	23	L	MC	75/75	75/75	17				
699.90	24									
698.90	25									
697.90	26									
696.90	27									
695.90	28									
694.90	29									



EXPLORATION LOG

SHEET 1 OF 3

START DATE 11/7/01
 END DATE 11/7/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-13
 E.A. # 0324-01-2
 GROUND ELEV. 720.24 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/7/01</u>	<u>NE</u>	

STATION 93+15 Q
 OFFSET 60 RT
 ENGINEER MAM
 EQUIPMENT Diedrich D-50 turbo
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 11/7/2001

ELEV. (m)	DEPTH (m)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT 150 mm Increments	BLOW COUNT Last 300 mm	Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS	
719.24	1.07	A	SPT	50/75	50/75	16		SC SM	SILTY, CLAYEY SAND with GRAVEL light brown, dry to slightly moist, very dense, with 13-15% low plasticity fines, 52% fine to coarse sand and 34-36% fine to coarse subrounded limestone gravel to 3/4". Strong calcareous cementation.	Previously reported as boring B-I.	
	1.22	A'	GRAB			50	PI, SI, MC				
	1.68										
	2										
	2.59	B	MC	75/25	75/25	5					
	2.74										
	3	B'	GRAB			50	PI, SI, MC, SH, CHEM				
	3.20										
	4	4.11	C	SPT	50/25	50/25	5		3.35	CLAYEY SAND with GRAVEL light brown, slightly moist, very dense, with 15% low plasticity fines, 51% fine to coarse sand and 34% fine subangular limestone gravel to 1-1/2". Strong calcareous cementation.	
	4.27	4.72	C'	GRAB			50	PI, SI, MC			
	5										
718.24	5							SC	CLAYEY SAND with GRAVEL tan, slightly moist, very dense, with 15% low plasticity fines, 51% fine to coarse sand and 34% fine to coarse subangular limestone gravel to 2-1/2". Moderate calcareous cementation.	4.27	
	5.64	D	MC	75/0	75/0	0					
	5.79										
	6	D'	GRAB			50	PI, SI, MC				
	6.25										
717.24	7	7.16	E	SPT	50/100	50/100	22	PI, SI, MC	GC	SILTY, CLAYEY SAND with GRAVEL light brown, slightly moist, very dense, with 14% low plasticity to nonplastic fines, 49% fine to coarse sand and 37% fine subangular limestone gravel to 1-1/2". Moderate calcareous cementation.	5.18
	8										
	8.69	F	MC	75/75	75/75	17	PI, SI, MC				
	9										



EXPLORATION LOG

SHEET 2 OF 3

START DATE 11/7/01
 END DATE 11/7/01
 JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
 LOCATION Las Vegas, Nevada
 BORING B-13
 E.A. # 0324-01-2
 GROUND ELEV. 720.24 (m)
 HAMMER DROP SYSTEM Cable

STATION	<u>93+15 Q</u>
OFFSET	<u>60 RT</u>
ENGINEER	<u>MAM</u>
EQUIPMENT	<u>Diedrich D-50 turbo</u>
OPERATOR	<u>Eagle Drilling</u>
DRILLING METHOD	<u>152 mm HS Auger</u>
BACKFILLED	<u>Yes</u> DATE <u>11/7/2001</u>

ELEV. (m)	DEPTH (m)	SAMPLE				LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	BLOW COUNT 150 mm Increments	Last 300 mm				
	10.21	G	SPT	50/25	50/25	5			
709.24	11								
	11.73	H	MC	75/50	75/50	11			
708.24	12	H'	GRAB			50	PI, SI, MC		
	12.34								
707.24	13								
706.24	14								
	14.78	I	SPT	50/25	50/25	5			
705.24	15								
704.24	16								
703.24	17								
	17.83	J	MC	75/38	75/38	4			
702.24	18								
701.24	19								



EXPLORATION LOG

SHEET 3 OF 3

START DATE 11/7/01
END DATE 11/7/01
JOB DESCRIPTION US 95 - Rainbow Blvd Interchange
LOCATION Las Vegas, Nevada
BORING B-13
E.A. # 0324-01-2
GROUND ELEV. 720.24 (m)
HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>11/7/01</u>	<u>NE</u>	

STATION 93+15 Q
OFFSET 60 RT
ENGINEER MAM
EQUIPMENT Diedrich D-50 turbo
OPERATOR Eagle Drilling
DRILLING METHOD 152 mm HS Auger
BACKFILLED Yes DATE 11/7/2001

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
699.24	21	K	SPT	50/25	50/25	5				
698.24	22									
697.24	23	L	MC	75/63	75/63	12			22.86	
696.24	24									
695.24	25									
694.24	26									
693.24	27									
692.24	28									
691.24	29									

EXPLORATION LOG

SHEET 1 OF 2



START DATE	1/14/02	STATION	R1 11+50
END DATE	1/14/02	OFFSET	5 RT
JOB DESCRIPTION	US 95 - Rainbow Blvd Retaining Walls	ENGINEER	PGT
LOCATION	Las Vegas, Nevada	EQUIPMENT	Diedrich D-50
BORING	B-14	OPERATOR	Eagle Drilling
E.A. #	0324-01-3	DRILLING METHOD	152 mm HS Auger
GROUND ELEV.	725.42 (m)	BACKFILLED	Yes DATE 1/14/2002
HAMMER DROP SYSTEM	Cable		

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm					
724.42	1	0.76	14A	SPT	50/125	50/125	20			
		0.91								
		1.22	14A'	GRAB			50	SV, PI		
		1.52	14B	MC	50/75	50/75	85	SV, PI		
723.42	2									
722.42	3	3.05	14C	SPT	50/50	50/50	100	SV, PI		
721.42	4									
720.42	5	4.57	14D	MC	50/75	50/75	100	SV, PI		
719.42	6	6.10	14E	SPT	50/75	50/75	0			
		6.25								
		6.55	14E'	GRAB			50	SV, PI, SH		
718.42	7									
717.42	8	7.62	14F	MC	50/25	50/25	0			
		7.77								
		8.08	14F'	GRAB			50	SV, PI		
716.42	9	9.14	14G	SPT	50/25	50/25	100	SV, PI		

NV DUE 03240135 NV DUE 01/17/2002

EXPLORATION LOG

SHEET 2 OF 2



START DATE 1/14/02
 END DATE 1/14/02
 JOB DESCRIPTION US 95 - Rainbow Blvd Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-14
 E.A. # 0324-01-3
 GROUND ELEV. 725.42 (m)
 HAMMER DROP SYSTEM Cable

STATION	<u>R1 11+50</u>	
OFFSET	<u>5 RT</u>	
ENGINEER	<u>PGT</u>	
EQUIPMENT	<u>Diedrich D-50</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>152 mm HS Auger</u>	
BACKFILLED	<u>Yes</u>	DATE <u>1/14/2002</u>

ELEV. (m)	DEPTH (m)	SAMPLE			BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE		150 mm Increments	Last 300 mm	Percent Recov'd				
706.42	19										
707.42	18										
708.42	17										
709.42	16										
710.42	15										
711.42	14										
712.42	13										
713.42	12	12.19	14I	SPT	50/50	50/50	0			12.19	
714.42	11										
714.42	10.67	14H	MC		50/100	50/100	100	SV, PI	SC		



EXPLORATION LOG

SHEET 1 OF 2

START DATE	1/14/02	STATION	R1 12+75
END DATE	1/14/02	OFFSET	8 RT
JOB DESCRIPTION	US 95 - Rainbow Blvd Retaining Walls		
LOCATION	Las Vegas, Nevada		
BORING	B-15	EQUIPMENT	Diedrich D-50
E.A. #	0324-01-3	OPERATOR	Eagle Drilling
GROUND ELEV.	730.91 (m)	DRILLING METHOD	152 mm HS Auger
HAMMER DROP SYSTEM	Cable	BACKFILLED	Yes DATE 1/14/2002

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
729.91	1	0.76	15A MC	50/50	50/50	100	SC	Clayey Sand with Gravel ; light grey brown, dry, very dense, with 10-20% low plastic fines, 45-55% fine to coarse sand, 30-40% subangular limestone gravel to 3". Cobbles to 6-inch-diameter comprise 15% of the total mass at the surface. Moderately cemented with weak caliche coating on cobbles within upper 10 feet.	Boring located at east end of Summerlin Westbound flyover.
728.91	2	1.52	15B SPT	50/100	50/100	100		The SPT and MC samples are small and have not adequately collected the larger gravel fraction.	Grab samples are from auger cuttings at surface. They are much larger in volume than the limited volume SPT and MC samples.
727.91	3 3.05	15C MC	50/75	50/75	100				
726.91	4	4.57	15D SPT	50/130	50/130	90			
725.91	5								
724.91	6 6.10	15E MC	50/50	50/50	100				
723.91	7								
722.91	8	7.62	15F SPT	50/35	50/35	33			
721.91	9 9.14	15G MC	50/25	50/25	0	GP GC	Poorly Graded Gravel with Clay and Sand ; light brown grey, dry, very dense, with 10-15% low to medium plastic fines, 30-35% fine to coarse sand, 55-60% subangular to subrounded limestone gravel to >2.5". Moderate to well cemented.		
	9.30	GRAB			50				
	9.60	15G GRAB							



EXPLORATION LOG

SHEET 2 OF 2

START DATE	1/14/02	STATION	R1 12+75			
END DATE	1/14/02	OFFSET	8 RT			
JOB DESCRIPTION	US 95 - Rainbow Blvd Retaining Walls					
LOCATION	Las Vegas, Nevada					
BORING	B-15					
E.A. #	0324-01-3					
GROUND ELEV.	730.91 (m)					
HAMMER DROP SYSTEM	Cable					
GROUNDWATER LEVEL						
	DATE	DEPTH m	ELEV. m			
	1/14/02	NE				
BACKFILLED	Yes	DATE 1/14/2002				

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
719.91	10.67							SC	Clayey Sand with Gravel ; light grey brown, dry, very dense, with 15-20% low to medium plastic fines, 50-55% fine to coarse sand, 25-30% subangular to subrounded limestone gravel to >2". Moderate to well cemented.	
	10.82	15H	SPT	50/75	50/75	0				
	11.13	15H	GRAB			50	SV, PI			
	11.58									
718.91	12.04	15I	GRAB			50	SV, PI		12.19	
	12.19	15I	MC	50/75	50/75	0				
717.91	13									
716.91	14									
715.91	15									
714.91	16									
713.91	17									
712.91	18									
711.91	19									



EXPLORATION LOG

SHEET 1 OF 1

START DATE 1/14/02
 END DATE 1/14/02
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-16
 E.A. # 0324-01-1
 GROUND ELEV. 725.42 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
1/14/02	NE	

STATION 13+25 R7
 OFFSET 15 RT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 1/14/2002

ELEV. (m)	DEPTH (m)	SAMPLE			BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE		150 mm Increments	Last 300 mm					
724.42	0.76								GP GC	Poorly Graded Gravel with Silty Clay and Sand ; light grey brown, dry, very dense, with 5-10% low plastic fines, 30-45% fine to coarse sand, 45-65% subangular limestone gravel to 3". Cobbles to 6-inch-diameter comprise 15% of the total mass at the surface. Moderately cemented with weak caliche coating on cobbles.	Boring located in median west of Rainbow Boulevard. Grab samples are from auger cuttings at surface. They are much larger in volume than the limited volume SPT and MC samples.
	0.91	16A	SPT	50/25	50/25	0					
	1.22	16A'	GRAB			50	SV, PI				
	1.52										
	1.68	16B	MC	50/50	50/50	85					
	1.98	16B'	GRAB			50	SV, PI				
723.42	2								SC	Clayey Sand with Gravel ; light grey brown, dry, very dense, with 15-20% medium plastic fines, 60-65% fine to coarse sand, 15-20% subangular to subrounded limestone gravel to >2". Moderate to well cemented.	Hard, cemented gravel throughout hole. Auger bit produces angular sand and fine gravel fragments from originally larger gravel and possibly cobble clasts.
	2.44										
	3	3.05	16C	SPT	50/50	50/50	100	SV, PI			
721.42	4								GC	Clayey Gravel with Sand ; light brown grey, dry, very dense, with 10-15% medium plastic fines, 40-45% fine to coarse sand, 40-45% subangular to subrounded limestone gravel to >2.5". Moderate to well cemented.	Hard, cemented gravel throughout hole. Auger bit produces angular sand and fine gravel fragments from originally larger gravel and possibly cobble clasts.
	4.57	4.72	16D	MC	50/25	50/25	0				
	5	5.18	16D'	GRAB			50	SV, PI			
	6	6.10	16E	SPT	50/100	50/100	33	SV, PI			
719.42	7	7.01							7.62		
	7.32	16F	GRAB				50	SV, PI			
	7.62	16F	MC	50/25	50/25	0					
717.42	8										
716.42	9										



EXPLORATION LOG

SHEET 1 OF 1

START DATE 1/15/02
 END DATE 1/15/02

JOB DESCRIPTION US 95 Widening / Project 2D Retaining WallsLOCATION Las Vegas, NevadaBORING B-17E.A. # 0324-01-1GROUND ELEV. 727.86 (m)HAMMER DROP SYSTEM CableSTATION 10+90 R4OFFSET 5 RTENGINEER PGTEQUIPMENT Diedrich D-50OPERATOR Eagle DrillingDRILLING METHOD 152 mm HS AugerBACKFILLED Yes DATE 1/14/2002

GROUNDWATER LEVEL

DATE 1/14/02DEPTH m NE

ELEV. m

ELEV. (m)	DEPTH (m)	SAMPLE NO.	TYPE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
				150 mm Increments	Last 300 mm	Percent Recov'd				
726.86	0.76							GP GC	Poorly Graded Gravel with Sand ; light grey, dry, very dense, with estimated <5% low plastic fines, 20-25% fine to coarse sand, 75-80% subangular to subrounded limestone gravel to 3". Cobbles to 6-inch-diameter comprise 15-20% of the total mass at the surface.	Boring located at southeast corner of Rainbow/US95 interchange. Grab samples are from auger cuttings at surface. They are much larger in volume than the limited volume SPT and MC samples.
	0.91	17A	SPT	50/25	50/25	0				
	1.22	17A'	GRAB			50	SV, PI			
	1.52									
	1.68	17B	MC	50/15	50/15	0				
	1.98	17B'	GRAB			50	SV, PI			
	2									
	3 3.05									
	3.20	17C	SPT	50/50	50/50	0				
	3.51	17C'	GRAB			50	SV, PI			
723.86	4							GW GC	Well Graded Gravel with Silty Clay and Sand ; light brown grey, dry, very dense, with 10% low plastic fines, 35-40% fine to coarse sand, 50-55% subangular to subrounded limestone gravel to >2.5". Moderate to well cemented.	Hard, cemented gravel throughout hole. Auger bit produces angular sand and fine gravel fragments from originally larger gravel and possibly cobble clasts.
	4.57									
	4.72	17D	MC	50/25	50/25	0				
	5	17D'	GRAB			50	SV, PI			
	5.18									
721.86	6 6.10							SP SM	Poorly Graded Sand with Silt and Gravel ; light grey brown, dry, very dense, with 10-15% low plastic fines, 45-50% fine to coarse sand, 40-45% subangular limestone gravel to 3". Moderately to well cemented.	7.62
	6.25	17E	SPT	50/50	50/50	25				
	6.71	17E'	GRAB			50	SV, PI			
	7	7.01								
	7.47	17F	GRAB			50	SV, PI			
720.86	7.62	17F	MC	50/25	50/25	0				
	8									
	9									



EXPLORATION LOG

SHEET 1 OF 1

EXPLORATION LOG

END DATE 1/15/02

JOB DESCRIPTION US 95 Wi

JOB DESCRIPTION SS-00-Widening Project ZB Retaining Walls

LOCATION Las Vegas, Nevada

BORING B-18

EA # 0324-01-1

E.A. # _____

GROUND ELEV. 730.40 (m)

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
1/14/02	NE	

STATION 13+90 R5

OFFSET 20 RT

ENGINEER **PGT**

ENGINEER EQUIPMENT Diedrich D-50

EQUIPMENT OPERATOR Eagle Drilling

OPERATOR Logic Driving

**DRILLING
METHOD** **152 mm HS Auger**

BACKFILLED Yes DATE 1/14/2002

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
735.40	0.76							SC SM	Silty, Clayey Sand with Gravel ; light grey brown, dry, very dense, with 15-20% low plastic fines, 45-50% fine to coarse sand, 30-35% subangular limestone gravel to 3". Cobbles to 6-inch-diameter comprise 15% of the total mass at the surface. Moderately cemented with weak caliche coating on cobbles.	Boring located in field south of NDOT right-of-way at west end of Summerlin eastbound off-ramp. The westernmost of five holes.
	0.91	18A	MC	50/25	50/25	100				
	1.22	18A'	GRAB			50	SV, PI		1.22	
	1.52									
	1.68	18B	SPT	50/25	50/25	0				
	1.98	18B'	GRAB			50	SV, PI			
	3.05									
	4.57									
	4.72	18D	SPT	50/100	50/100	0				
	5.18	18D'	GRAB			50	SV, PI			
734.40	6.10							GP GC		Grab samples are from auger cuttings at surface. They are much larger in volume than the limited volume SPT and MC samples.
	6.10	18E	MC	50/25	50/25	100	SV, PI		2.74	
	7.01									
	7.47									
	7.62	18F	GRAB			50	SV, PI			
732.40	7.62	18F	SPT	50/50	50/50	0		SW SC		Hard, cemented gravel throughout hole. Auger bit produces angular sand and fine gravel fragments from originally larger gravel and possibly cobble clasts.
	7.62									
	8									
	9									



EXPLORATION LOG

SHEET 1 OF 2

START DATE 1/15/02
END DATE 1/15/02
JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
LOCATION Las Vegas, Nevada
BORING B-19
E.A. # 0324-01-1
GROUND ELEV. 735.48 (m)
HAMMER DROP SYSTEM Cable

STATION 12+90 R5
OFFSET 10 RT
ENGINEER PGT
EQUIPMENT Diedrich D-50
OPERATOR Eagle Drilling
DRILLING METHOD 152 mm HS Auger
BACKFILLED Yes DATE 1/14/2002

ELEV. (m)	DEPTH (m)	SAMPLE NO.	TYPE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
				150 mm Increments	Last 300 mm	Percent Recov'd				
734.48	0.76	19A	SPT	50/15	50/15	0		GW GM	<p>Well Graded Gravel with Silt and Sand ; light grey brown, dry, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand, 40-50% subangular limestone gravel to 3". Cobbles to 6-inch-diameter comprise 15% of the total mass at the surface. Moderately cemented with weak caliche coating on cobbles.</p> <p>Grab samples are from auger cuttings at surface. They are much larger in volume than the limited volume SPT and MC samples.</p>	<p>Boring located in field south of NDOT right-of-way at west end of Summerlin eastbound off-ramp.</p> <p>Hard, cemented gravel throughout hole. Auger bit produces angular sand and fine gravel fragments from originally larger gravel and possibly cobble clasts.</p>
	0.91									
	1.22	19A	GRAB			50	SV, PI			
	1.52	19B	MC	50/10	50/10	0				
	1.68	19B	GRAB			50	SV, PI			
	1.98	19B	GRAB			50	SV, PI			
	2									
	3 3.05	19C	SPT	50/75	50/75	100	SV, PI			
	4									
	4.57	19D	MC	50/75	50/75	67	SV, PI			
730.48	4.72	19D	GRAB			50	SV, PI			
	5									
	5.18	19D	GRAB			50	SV, PI			
	6 6.10	19E	SPT	50/75	50/75	67	SV, PI			
	6.25	19E	GRAB			50	SV, PI			
728.48	6.71	19E	GRAB			50	SV, PI			
	7									
	7.62	19F	MC	50/25	50/25	100	SV, PI			
	8									
726.48	9 9.14	19G	SPT	50/50	50/50	50		SC	<p>Clayey Sand with Gravel ; light grey brown, dry, very dense, with 10-15% low to medium plastic fines, 50-55% fine to coarse sand, 35-45% subangular limestone gravel to 3". Moderately cemented with weak caliche coating on cobbles.</p>	
	9.30	19G	GRAB			50	SV, PI			
	9.75	19G	GRAB			50	SV, PI			



EXPLORATION LOG

SHEET 2 OF 2

START DATE 1/15/02END DATE 1/15/02JOB DESCRIPTION US 95 Widening / Project 2D Retaining WallsSTATION 12+90 R5OFFSET 10 RTENGINEER PGTEQUIPMENT Diedrich D-50OPERATOR Eagle DrillingDRILLING METHOD 152 mm HS AugerBACKFILLED Yes DATE 1/14/2002LOCATION Las Vegas, NevadaBORING B-19E.A. # 0324-01-1

GROUNDWATER LEVEL

GROUND ELEV. 735.48 (m)DATE 1/14/02DEPTH m NEELEV. m HAMMER DROP SYSTEM Cable

ELEV. (m)	DEPTH (m)	SAMPLE NO.	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
			Type	150 mm Increments	Last 300 mm				
724.48	10.67	19H	MC	50/75	50/75	100	SV, PI		
723.48	11								
722.48	12	19I	SPT	50/25	50/25	0			
721.48	12.19					12.19	GP GC	Poorly Graded Gravel with Silty Clay and Sand ; light grey brown, dry, very dense, with 10% low plastic fines, 35% fine to coarse sand, 55% subangular limestone gravel to 3". Moderately to well cemented.	
720.48	13	19J	MC	50/25	50/25	0			
719.48	13.72								
718.48	13.87	19J	GRAB			50	SV, PI		
717.48	14								
716.48	14.33								
715.48	15	19K	SPT	50/125	50/125	40	SV, PI	15.24	
714.48	15.24								
713.48	16								
712.48	17								
711.48	18								
710.48	19								



EXPLORATION LOG

SHEET 1 OF 1

START DATE	1/15/02
END DATE	1/15/02
JOB DESCRIPTION	US 95 Widening / Pr
LOCATION	Las Vegas, Nevada
BORING	B-20
E.A. #	0324-01-1
GROUND ELEV.	733.96 (m)
HAMMER DROP SYSTEM	Cable

STATION	11+95 R5
OFFSET	8 RT
ENGINEER	PGT
EQUIPMENT	Diehrich D-50
OPERATOR	Eagle Drilling
DRILLING METHOD	152 mm HS Auger
BACKFILLED	Yes DATE 1/14/2002

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
1/14/02	NE	
.		

START DATE 1/15/02END DATE 1/15/02JOB DESCRIPTION US 95 Widening / Project 2D Retaining WallsLOCATION Las Vegas, NevadaBORING B-21E.A. # 0324-01-1GROUND ELEV. 733.04 (m)HAMMER DROP SYSTEM Cable**EXPLORATION LOG**

SHEET 1 OF 2

STATION 11+10 R5OFFSET 8 RTENGINEER PGTEQUIPMENT Diedrich D-50OPERATOR Eagle DrillingDRILLING METHOD 152 mm HS AugerBACKFILLED Yes DATE 1/14/2002

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
1/14/02	NE	

ELEV. (m)	DEPTH (m)	SAMPLE NO.	TYPE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
				150 mm Increments	Last 300 mm	Percent Recov'd				
732.04	0.76	21A	SPT	50/10	50/10	0		SP SM	Poorly Graded Sand with Silt and Gravel ; light grey brown, dry, very dense, with 10-15% low plastic fines, 50-55% fine to coarse sand, 35-40% subangular limestone gravel to 3". Cobbles to 6-inch-diameter comprise 15% of the total mass at the surface. Moderately cemented with weak caliche coating on cobbles.	Boring located in field south of NDOT right-of-way at Summerlin eastbound off-ramp.
	0.91									
	1.22	21A'	GRAB			50	SV, PI			
	1.52	21B	MC	50/25	50/25	100				
	1.68									
	1.98	21B'	GRAB			50	SV, PI			
731.04	2							GP GC	2.44 Poorly Graded Gravel with Silty Clay and Sand ; light brown grey, dry, very dense, with 5-10% low plastic fines, 30-35% fine to coarse sand, 55-60% subangular to subrounded limestone gravel to >2.5". Moderate to well cemented.	Grab samples are from auger cuttings at surface. They are much larger in volume than the limited volume SPT and MC samples.
	3.05	21C	SPT	50/25	50/25	0				
	3.20									
	3.51	21C'	GRAB			50	SV, PI			
	4									
	4.57	21D	MC	50/25	50/25	0				
	4.72									
728.04	5	21D'	GRAB			50	SV, PI	GP GC	Hard, cemented gravel throughout hole. Auger bit produces angular sand and fine gravel fragments from originally larger gravel and possibly cobble clasts.	
	5.18									
	6	21E	SPT	50/50	50/50	25				
	6.10									
	6.25	21E'	GRAB			50	SV, PI			
	6.71									
726.04	7							SW SM	8.53 Well Graded Sand with Silt and Gravel ; light grey brown, dry, very dense, with 10-15% low plastic fines, 50-55% fine to coarse sand, 35-40% subangular limestone gravel to 3". Moderately to well cemented.	
	7.62	21F	MC	50/10	50/10	0				
	7.77									
	8	21F'	GRAB			50	SV, PI			
	8.23									
	9	21G	SPT	50/75	50/75	100	SV, PI			
	9.14									



EXPLORATION LOG

SHEET 2 OF 2

START DATE 1/15/02END DATE 1/15/02JOB DESCRIPTION US 95 Widening / Project 2D Retaining WallsLOCATION Las Vegas, NevadaBORING B-21E.A. # 0324-01-1GROUND ELEV. 733.04 (m)HAMMER DROP SYSTEM CableSTATION 11+10 R5OFFSET 8 RTENGINEER PGTEQUIPMENT Diedrich D-50OPERATOR Eagle DrillingDRILLING METHOD 152 mm HS AugerBACKFILLED Yes DATE 1/14/2002

GROUNDWATER LEVEL

DATE 1/14/02DEPTH m NEELEV. m

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
	70.06									
	70.52	21H	GRAB			50	SV, PI			
	70.67	21H	MC	50/25	50/25	0			10.67	
722.04	11									
721.04	12									
720.04	13									
719.04	14									
718.04	15									
717.04	16									
716.04	17									
715.04	18									
714.04	19									



EXPLORATION LOG

SHEET 1 OF 1

START DATE 1/16/02
 END DATE 1/16/02
 JOB DESCRIPTION US 95 Widening / Project 2D Retaining Walls
 LOCATION Las Vegas, Nevada
 BORING B-22
 E.A. # 0324-01-1
 GROUND ELEV. 730.91 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
1/14/02	NE	

STATION 10+15 R5
 OFFSET 8 RT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 1/14/2002

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
729.91	0.76						GW GM SC SM	<p>Well Graded Gravel with Silt and Sand; light grey brown, dry, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand, 45-50% subangular limestone gravel to 3". Cobbles and boulders to 1.25-foot-diameter comprise 5-10% of the total mass at the surface. Moderately cemented with weak caliche coating on cobbles.</p> <p>Silty, Clayey Sand with Gravel; light grey brown, dry, very dense, with 15-20% low plastic fines, 56-60% fine to coarse sand, 25-30% subangular limestone gravel to 3". Moderately cemented with weak caliche coating on cobbles.</p> <p>Well Graded Gravel with Silt and Sand; light grey brown, dry, very dense, with 10% low plastic fines, 40-45% fine to coarse sand, 45-50% subangular limestone gravel to 3". Moderately to well cemented.</p>	<p>Boring located in field south of NDOT right-of-way at Summerlin eastbound off-ramp. Easternmost of five holes.</p> <p>Grab samples are from auger cuttings at surface. They are much larger in volume than the limited volume SPT and MC samples.</p> <p>Hard, cemented gravel throughout hole. Auger bit produces angular sand and fine gravel fragments from originally larger gravel and possibly cobble clasts.</p>
	0.91	22A	SPT	50/25	50/25	0			
	1.22	22A'	GRAB			50			
	1.52	22B	MC	50/40	50/40	100			
	2								
	3 3.05	22C	SPT	50/50	50/50	50			
	3.20	22C'	GRAB			50			
	3.51								
	4								
	4.57	22D	MC	50/25	50/25	100			
725.91	5 5.18	22D'	GRAB			50			
	6 6.10	22E	SPT	50/50	50/50	0	GW GM		<p>Hard, cemented gravel throughout hole. Auger bit produces angular sand and fine gravel fragments from originally larger gravel and possibly cobble clasts.</p>
	6.25	22E'	GRAB			50			
	6.71								
723.91	7								
	7.62	22F	MC	50/25	50/25	100			
	7.77	22F'	GRAB						
722.91	8 8.23	22G	GRAB	50/25	50/25	50			
	9 9.14	22G	SPT	50/25	50/25	100			



EXPLORATION LOG

SHEET 1 OF 2

START DATE 3/5/02
 END DATE 3/5/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-23
 E.A. # 0324-01-4
 GROUND ELEV. 722.07 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/5/02</u>	<u>NE</u>	

STATION 87+30 "95-N"
 OFFSET 48 m RT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 3/5/2002

ELEV. (m)	DEPTH (m)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
				150 mm Increments	Last 300 mm					
721.07	1									
	1.52	A	SPT	50/50	50/50	100				
	1.68									
720.07	2	A'	AC			50	SV, PI			
	2.13									
719.07	3	3.05	B	MC	50/75	50/75	0			
	3.20									
	3.66	B'	AC			50	SV, PI			
718.07	4									
	4.57	C	SPT	50/75	50/75	0				
	4.72									
717.07	5	5.18	C'	AC			50	SV, PI		
716.07	6	6.10	D	MC	50/50	50/50	0			
	6.25									
	6.71	D'	AC			50	SV, PI			
715.07	7									
	7.62	E	SPT	50/38	50/38	67				
	7.77									
714.07	8	8.23	E'	AC			50	SV, PI		
713.07	9	9.14	F	MC	50/50	50/50	0			
	9.30									
	9.75	F'	AC			50	SV, PI			



EXPLORATION LOG

SHEET 2 OF 2

START DATE 3/5/02
 END DATE 3/5/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-23
 E.A. # 0324-01-4
 GROUND ELEV. 722.07 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/5/02</u>	<u>NE</u>	

STATION 87+30 "95-N"
 OFFSET 48 m RT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 3/5/2002

ELEV. (m)	DEPTH (m)	SAMPLE					LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	BLOW COUNT		Percent Recov'd				
				150 mm Increments	Last 300 mm					
	10.67							GC	<p>Clayey Sand with Gravel ; light grey brown, slightly moist, very dense, with 30% medium plastic fines, 56% fine to coarse sand and 14% subangular to subrounded gravel to >38 mm. Weak cementation.</p>	
	10.82	G	SPT	50/50	50/50	0				
711.07	11	G'	AC			50	SV, PI			
	11.28									
710.07	12									
	12.19	H	MC	50/38	50/38	0				
	12.34									
	12.80	H'	AC			50	SV, PI			
709.07	13									
	13.72	I	SPT	50/75	50/75	100	SV, PI			
708.07	14							SC	<p>15.30</p>	
707.07	15									
	15.24	J	MC	50/38	50/38	0				
706.07	16									
705.07	17									
704.07	18									
703.07	19									



EXPLORATION LOG

SHEET 1 OF 1

START DATE 3/6/02
 END DATE 3/6/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-24
 E.A. # 0324-01-4
 GROUND ELEV. 718.11 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/6/02</u>	<u>NE</u>	

STATION 85+15 "95-N"
 OFFSET 33 m RT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 3/6/2002

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
717.11	1							SP SC	Poorly Graded Sand with Clay and Gravel ; light brown, slightly moist, very dense, with 12% low plastic fines, 46% fine to coarse sand, 42% subangular to subrounded gravel to >50 mm.	Boring located at west end of narrow NDOT right-of-way on north side of US 95.
	1.52	A	MC	50/75	50/75	0				
	1.68	A'	AC			50	SV, PI			
716.11	2	2.13								
	3.05	B	SPT	50/125	50/125	40				
	3.20	B'	AC			50	SV, PI			
715.11	3	3.66								
	3.05	C	MC	50/100	50/100	100	SV, PI			
714.11	4									
	4.57	D	AC			50	SV, PI			
713.11	5							GP GC		Poorly Graded Gravel with Clay and Sand ; light grey brown, slightly moist, very dense, with 9-11% low to medium plastic fines, 35-41% fine to coarse sand and 48-56% subangular to subrounded gravel to >38 mm.
	5.64									
712.11	6	5.94								
	6.10	D	SPT	50/25	50/25	0				
711.11	7									
710.11	8									
709.11	9									

EXPLORATION LOG

SHEET 1 OF 1



START DATE 3/6/02
 END DATE 3/6/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-25
 E.A. # 0324-01-4
 GROUND ELEV. 716.89 (m)
 HAMMER DROP SYSTEM Cable

STATION	<u>83+85 "95-N"</u>	
OFFSET	<u>37 m RT</u>	
ENGINEER	<u>PGT</u>	
EQUIPMENT	<u>Diedrich D-50</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>152 mm HS Auger</u>	
BACKFILLED	<u>Yes</u>	<u>DATE 3/6/2002</u>

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION			REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm						
715.89	1						GM	Silty Gravel with Sand ; light grey brown, slightly moist, very dense, with estimated 15-20% low plastic fines, 35-40% fine to coarse sand and 45-50% subangular to subrounded gravel to 180 mm. Weak to moderate cementation.	0.61		
							SC	Clayey Sand with Gravel ; light brown, slightly moist, very dense, with 21% medium plastic fines, 40% fine to coarse sand and 39% subangular to subrounded gravel to >38 mm. Weak cementation.	2.44		
714.89	2	1.52	A SPT	50/88	50/88	50	SV, PI				
		1.68									
713.89	3	2.13	A' AC			50	SV, PI				
		3.05									
		3.20									
712.89	4										
711.89	5	4.57	C SPT	50/50	50/50	100					
		4.72									
		5.18	C' AC			50	SV, PI				
		5.64									
710.89	6	5.94	D' AC			50	SV, PI				
		6.10	D MC	50/50	50/50	0					
709.89	7										
708.89	8										
707.89	9										



EXPLORATION LOG

SHEET 1 OF 2

START DATE	3/5/02	STATION	82+50 "95-N"
END DATE	3/5/02	OFFSET	35 m RT
JOB DESCRIPTION	US 95 Widening Project / Retaining-Sound Walls		
LOCATION	Las Vegas, Nevada		
BORING	B-26	EQUIPMENT	Diedrich D-50
E.A. #	0324-01-4	OPERATOR	Eagle Drilling
GROUND ELEV.	715.06 (m)	DRILLING METHOD	152 mm HS Auger
HAMMER DROP SYSTEM	Cable	BACKFILLED	Yes DATE 3/5/2002

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
3/5/02	NE	

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS	
		NO.	TYPE	150 mm Increments	Last 300 mm					
714.06	1						GP GC	<p>Poorly Graded Gravel with Clay and Sand ; light grey brown, dry, very dense, with 11% low plastic fines, 34% fine to coarse sand and 55% subangular to subrounded gravel to >50 mm. Weak to moderate cementation.</p> <p>Clayey Gravel with Sand ; light grey brown, slightly moist, very dense, with 12-17% medium plastic fines, 26-36% fine to coarse sand and 49-57% subangular to subrounded gravel to >38 mm.</p> <p>Clayey Sand with Gravel ; light brown, slightly moist, very dense, with 34% high plastic fines, 47% fine to coarse sand and 20% subangular gravel to >38 mm. Weak cementation.</p> <p>Clayey Sand ; light brown, slightly moist, very dense, with 17% medium plastic fines, 72% fine to coarse sand and 11% subangular gravel to >38 mm. Weak cementation.</p> <p>Sandy Fat Clay ; light brown, moist, hard, with</p>	Boring located at east end of narrow NDOT right-of-way on north side of US 95.	
1.52		A	SPT	50/75	50/75	0				
1.68		A'	AC			50				
2.13										
713.06	2									
3.05		B	MC	50/75	50/75	0				
3.20		B'	AC			50				
3.66										
711.06	4									
4.57		C	SPT	50/25	50/25	0				
4.72		C'	AC			50				
5.18										
709.06	6	D	MC	50/75	50/75	100	SC	<p>Clayey Sand with Gravel ; light brown, slightly moist, very dense, with 34% high plastic fines, 47% fine to coarse sand and 20% subangular gravel to >38 mm. Weak cementation.</p> <p>Clayey Sand ; light brown, slightly moist, very dense, with 17% medium plastic fines, 72% fine to coarse sand and 11% subangular gravel to >38 mm. Weak cementation.</p> <p>Sandy Fat Clay ; light brown, moist, hard, with</p>	5/17 0324C NV C	
6.10										
708.06	7									
7.62		E	SPT	50/100	50/100	100				
707.06	8						SC	<p>Clayey Sand ; light brown, slightly moist, very dense, with 17% medium plastic fines, 72% fine to coarse sand and 11% subangular gravel to >38 mm. Weak cementation.</p> <p>Sandy Fat Clay ; light brown, moist, hard, with</p>		
706.06	9	F	MC	50/113	50/113	100				
9.14										



EXPLORATION LOG

SHEET 2 OF 2

START DATE 3/5/02
END DATE 3/5/02
JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
LOCATION Las Vegas, Nevada
BORING B-26
E.A. # 0324-01-4
GROUND ELEV. 715.06 (m)
HAMMER DROP SYSTEM Cable

STATION 82+50 "95-N"
OFFSET 35 m RT
ENGINEER PGT
EQUIPMENT Diedrich D-50
OPERATOR Eagle Drilling
DRILLING METHOD 152 mm HS Auger
BACKFILLED Yes DATE 3/5/2002

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/5/02</u>	<u>NE</u>	

ELEV. (m)	DEPTH (m)	SAMPLE				LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	BLOW COUNT					
				150 mm Increments	Last 300 mm	Percent Recov'd			
10.67	G	SPT	50/100	50/100	100	SV, PI	CH	51% high plastic fines, 46% fine to coarse sand and 3% subangular gravel to >20 mm. The limited sample penetration is a result of coarse gravel clogging the sample tube. The majority clay soil is very stiff to hard.	
704.06	11								
703.06	12								
702.06	13								
701.06	14								
700.06	15								
699.06	16								
698.06	17								
697.06	18								
696.06	19								



EXPLORATION LOG

SHEET 1 OF 1

START DATE 3/7/02END DATE 3/5/02JOB DESCRIPTION US 95 Widening Project / Retaining-Sound WallsLOCATION Las Vegas, NevadaBORING B-27E.A. # 0324-01-4GROUND ELEV. 711.10 (m)HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/7/02</u>	<u>NE</u>	

STATION	<u>80+65 "95-N"</u>
OFFSET	<u>35 m RT</u>
ENGINEER	<u>PGT</u>
EQUIPMENT	<u>Foremost B90</u>
OPERATOR	<u>Eagle Drilling</u>
DRILLING METHOD	<u>203 mm HS Auger</u>
BACKFILLED	<u>Yes</u> DATE <u>3/7/2002</u>

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
710.10	1									Boring located within parking area in SW corner of Catalina Apartments.
709.10	2									
708.10	3									
707.10	4									
706.10	5									
705.10	6									
704.10	7									
703.10	8									
702.10	9									



EXPLORATION LOG

SHEET 1 OF 1

START DATE	3/7/02	STATION	79+70 "95-N"
END DATE	3/7/02	OFFSET	25 m RT
JOB DESCRIPTION	US 95 Widening Project / Retaining-Sound Walls	ENGINEER	PGT
LOCATION	Las Vegas, Nevada	EQUIPMENT	Foremost B90
BORING	B-28	OPERATOR	Eagle Drilling
E.A. #	0324-01-4	DRILLING METHOD	203 mm HS Auger
GROUND ELEV.	708.96 (m)	BACKFILLED	Yes DATE 3/7/2002
HAMMER DROP SYSTEM	Cable		

ELEV. (m)	DEPTH (m)	SAMPLE			BLOW COUNT		LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
707.96	1								0.09 Asphalt Concrete Clayey Gravel with Sand ; light brown, dry, very dense, with 15% medium plastic fines, 39% fine to coarse sand and 46% subangular to subrounded gravel to >50 mm. Weak to moderate cementation.	Boring located within parking area along southwest side of Catalina Apartments.
	1.52	A	SPT	50/75	50/75	67				
	1.68									
706.96	2	A'	AC			50	SV, PI		2.44 Clayey Sand with Gravel ; light brown, slightly moist, very dense, with 24% medium plastic fines, 58% fine to coarse sand and 18% subangular to subrounded gravel to >25 mm. Weak to moderate cementation.	Patch was installed in asphalt concrete surface upon completion of boring.
	2.13									
705.96	3	3.05	B	MC	50/75	50/75	67	SV, PI		
704.96	4								3.96 Poorly Graded Gravel with Clay and Sand ; grey brown, slightly moist, very dense, with estimated 10-15% low plastic fines, 35-40% fine to coarse sand and 50-55% subangular to subrounded gravel to >50 mm. Moderately cemented.	
	4.57	C	SPT	50/50	50/50	100				
	4.72									
703.96	5	5.18	C'	AC			50	SV, PI		
702.96	6	6.10								
	6.55	D	MC	14 10 12	22	85	SV, PI			
701.96	7									
700.96	8									
699.96	9									



EXPLORATION LOG

SHEET 1 OF 2

START DATE 3/6/02
 END DATE 3/6/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-29
 E.A. # 0324-01-4
 GROUND ELEV. 707.14 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/6/02</u>	<u>NE</u>	

STATION 78+40 "95-N"
 OFFSET
 ENGINEER
 EQUIPMENT
 OPERATOR
 DRILLING METHOD
 BACKFILLED Yes DATE 3/6/2002

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
706.14	1						GP GC	<p>-0.09 Asphalt Concrete Poorly Graded Gravel with Clay and Sand ; light grey brown, dry, very dense, with 9% low plastic fines, 31% fine to coarse sand and 60% subangular to subrounded gravel to >50 mm. Weak to moderate cementation.</p> <p>1.52</p> <p>1.68 A SPT 50/138 50/138 40</p> <p>2.13 A' AC 50 SV, PI</p> <p>3.05</p> <p>3.20 B MC 50/50 50/50 50</p> <p>3.66 B' AC 50 SV, PI</p> <p>3.96</p> <p>4.57</p> <p>4.72 C SPT 50/75 50/75 0</p> <p>5.18 C' AC 50 SV, PI</p> <p>5.49</p> <p>6.10 D MC 32 50/125 50/125 100 SV, PI</p> <p>6.37</p> <p>7.01 E SPT 50/50 50/50 100</p> <p>7.62</p> <p>7.77 E' AC 50 SV, PI</p> <p>8.23</p> <p>9.14 F MC 50 50/75 50/75 100 SV, PI</p> <p>9.35</p>	<p>Boring located within parking area along south side of Catalina Apartments.</p> <p>Patch was installed in asphalt concrete surface upon completion of boring.</p> <p>Drill penetration is slowing. Boring is tight.</p>
705.14	2					50			
704.14	3								
703.14	4								
702.14	5					50			
701.14	6								
700.14	7								
699.14	8								
698.14	9								



EXPLORATION LOG

SHEET 2 OF 2

START DATE 3/6/02
 END DATE 3/6/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-29
 E.A. # 0324-01-4
 GROUND ELEV. 707.14 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/6/02</u>	<u>NE</u>	

STATION 78+40 "95-N"
 OFFSET 10 m RT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 3/6/2002

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
	10.67									
696.14	11.13	G	SPT	45 26 43	69	60	SV, PI	GC	T0.06 Clayey Gravel with Sand ; light brown, moist, very dense, with 25% high plastic fines, 32% fine to coarse sand and 43% subangular to subrounded gravel to >50 mm. Weak cemented.	
695.14	12.19	H	MC	50/50	50/50	100	SV, PI	SC	11.58 Clayey Sand with Gravel ; light brown, moist, very dense, with 42% medium plastic fines, 33% fine to coarse sand and 25% subangular gravel to >38 mm.	
694.14	13								12.95	
693.14	14									
692.14	15									
691.14	16									
690.14	17									
689.14	18									
688.14	19									



EXPLORATION LOG

SHEET 1 OF 1

START DATE 3/5/02
 END DATE 3/5/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-30
 E.A. # 0324-01-4
 GROUND ELEV. 726.03 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/5/02</u>	<u>NE</u>	

STATION 89+10 "95-S"
 OFFSET 55 m LT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 3/5/2002

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION		REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				MATERIAL DESCRIPTION	REMARKS	
725.03	1								Poorly Graded Gravel with Silt and Sand ; light brown grey, dry, very dense, with 7-8% low plastic fines, 25-35% fine to coarse sand and 57-68% subangular to subrounded gravel to >60 mm.		Boring located in wide NDOT right-of-way on south side of US 95.
	1.52	A	SPT	50/25	50/25	0					
	1.68										
724.03	2	A'	AC			50	SV, PI				
	2.13										
723.03	3	B	MC	50/75	50/75	100					
	3.05										
	3.20										
	3.66	B'	AC			50	SV, PI				
722.03	4										
	4.57	C	SPT	50/100	50/100	50					
	4.72										
721.03	5	C'	AC			50	SV, PI				
	5.18										
	5.49	D	MC	50/75	50/75	100	SV, PI				
720.03	6										
719.03	7										
718.03	8										
717.03	9										



START DATE 3/5/02

END DATE 3/5/02

JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls

LOCATION Las Vegas, Nevada

BORING B-31

FA # 0324-01-4

GROUND FL FV 723.90 (m)

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
3/5/02	NE	

SHEET 1 OF 2

87+90 "95-S"

30 m LT

PGT

Diedrich D-50

Eagle Drilling

152 mm HS Auger

Page 2 of 2

BACKFILLED



EXPLORATION LOG

SHEET 2 OF 2

START DATE 3/5/02

END DATE 3/5/02

JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls

LOCATION Las Vegas, Nevada

BORING B-31

EA # 0324-01-4

GROUND ELEV. 723.90 (m)

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
3/5/02	NE	

STATION 87+90 "95-S"

30 m LT

ENGINEER PGT

EQUIPMENT Diedrich D-50

OPERATOR Eagle Drilling

DRILLING METHODS 152 mm HS Auger

Method Yes Date 3/5/2002



EXPLORATION LOG

SHEET 1 OF 1

START DATE 3/21/02
 END DATE 3/21/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-32
 E.A. # 0324-01-4
 GROUND ELEV. 720.85 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/21/02</u>	<u>NE</u>	

STATION 85+90 "95-S"
 OFFSET 30 m LT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 3/21/2002

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm				
719.85	1						GP GM	Poorly Graded Gravel with Silt and Sand ; light brown grey, slightly moist, very dense, with estimated 10-15% low plastic fines, 30-35% fine to coarse sand and 50-55% subangular to subrounded gravel to >65 mm.	
1.52		A	SPT	50/38	50/38	67			
1.68							0.91		
718.85	2	A'	AC			50	SV, PI	Silty, Clayey Gravel with Sand ; light grey brown, dry, very dense, with 14% low plastic fines, 39% fine to coarse sand and 47% subangular to subrounded gravel to >50 mm. Weak to moderate cementation.	
2.13							GC GM		
717.85	3	B	MC	50/50	50/50	0			
3.05							2.44		
3.20							GC	Clayey Gravel with Sand ; light brown grey, dry, very dense, with 13% medium plastic fines, 30% fine to coarse sand and 57% subangular to subrounded gravel to >50 mm.	
3.66		B'	AC			50	SV, PI		
716.85	4								
4.57		C	SPT	50/50	50/50	100		3.96	
4.72							GP GC	Poorly Graded Gravel with Clay and Sand ; light grey brown, slightly moist, very dense, with 8-11% low to medium plastic fines, 31-35% fine to coarse sand and 54-61% subangular to subrounded gravel to >65 mm. Weak cementation.	
5.18		C'	AC			50	SV, PI		
714.85	6	D	MC	50/100	50/100	100	SV, PI	6.20	
6.10									
713.85	7								
712.85	8								
711.85	9								



START DATE 3/5/02
 END DATE 3/5/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-33
 E.A. # 0324-01-4
 GROUND ELEV. 715.98 (m)
 HAMMER DROP SYSTEM Cable

EXPLORATION LOG

SHEET 1 OF 2

STATION	<u>83+00 "95-S"</u>	
OFFSET	<u>20 m LT</u>	
ENGINEER	<u>PGT</u>	
EQUIPMENT	<u>Diedrich D-50</u>	
OPERATOR	<u>Eagle Drilling</u>	
DRILLING METHOD	<u>152 mm HS Auger</u>	
BACKFILLED	<u>Yes</u>	DATE <u>3/5/2002</u>

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd			
714.98	1						GM	Silty Gravel with Sand ; light grey brown, dry, very dense, with estimated 15-20% low plastic fines, 35-40% fine to coarse sand and 45-50% subangular to subrounded gravel to 5". Weak to moderate cementation.	
1.52		A	SPT	50/75	50/75	33	GP	Poorly Graded Gravel with Clay and Sand ; light grey brown, slightly moist, very dense, with 12% low plastic fines, 38% fine to coarse sand and 50% subangular to subrounded gravel to >50 mm. Weak cementation.	
1.68		A'	AC			50	GC		
713.98	2	2.13					SC	Clayey Sand with Gravel ; light grey brown, slightly moist, very dense, with 15-19% medium plastic fines, 52-54% fine to coarse sand and 27-33% subangular to subrounded gravel to >50 mm. Weak cementation.	
712.98	3	3.05	B	MC	50/88	50/88	100	SV, PI	
711.98	4						SC		
4.57		C	SPT	50/88	50/88	100	SV, PI		
710.98	5						GP		
709.98	6	6.10	D	MC	50/75	50/75	67	GC	Poorly Graded Gravel with Clay and Sand ; light grey brown, slightly moist, very dense, with 10-12% medium plastic fines, 31-33% fine to coarse sand and 54-57% subangular to subrounded gravel to >50 mm. Weak cementation.
6.25		D'	AC			50	SC		
708.98	7						GP		
7.62		E	SPT	50/50	50/50	67	GC		
7.77		E'	AC			50	SC	Clayey Sand with Gravel ; light brown, slightly moist, very dense, with 15% high plastic fines, 56% fine to coarse sand and 29% subangular to subrounded gravel to >50 mm.	
707.98	8	8.23					GP		
706.98	9	9.14	F	MC	50/75	50/75	100	DOT	Clayey Sand with Gravel ; light brown, slightly



EXPLORATION LOG

SHEET 2 OF 2

START DATE 3/5/02

END DATE 3/5/02

JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls

LOCATION Las Vegas, Nevada

BORING B-33

E A # 0324-

GROUND ELEV. 715.98 (m)

GROUND ELEV.: _____ ()

HAMMER DROP SYSTEM

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
3/5/02	NE	

STATION	83+00 "95-S"	
OFFSET	20 m LT	
ENGINEER	PGT	
EQUIPMENT	Diedrich D-50	
OPERATOR	Eagle Drilling	
DRILLING METHOD	152 mm HS Auger	
BACKFILLED	Yes	DATE 3/5/2002



EXPLORATION LOG

SHEET 1 OF 2

START DATE 3/21/02
END DATE 3/21/02
JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
LOCATION Las Vegas, Nevada
BORING B-34
E.A. # 0324-01-4
GROUND ELEV. 709.88 (m)
HAMMER DROP SYSTEM Cable

STATION 79+80 "95-S"
OFFSET 15 m LT
ENGINEER PGT
EQUIPMENT Diedrich D-50
OPERATOR Eagle Drilling
DRILLING METHOD 152 mm HS Auger
BACKFILLED Yes DATE 3/21/2002

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd				
708.88	1							GC	0.06 Asphalt Concrete: thin AC pavement on bike path.	
	1.52	A	SPT	50/50	50/50	0			Clayey Gravel with Sand ; light brown, slightly moist, very dense, with 14% low to medium plastic fines, 40% fine to coarse sand and 47% subangular to subrounded gravel to >50 mm. Weak to moderate cementation.	
707.88	2	1.68	A'	AC		50	SV, PI	SC	2.44 Clayey Sand with Gravel ; light brown, moist, very dense, with 28% medium plastic fines, 51% fine to coarse sand, 21% subangular to subrounded gravel to >35 mm. Weak cemented.	
	2.13								3.66 Poorly Graded Sand with Silt and Gravel ; light brown, moist, very dense, with 12% nonplastic fines, 55% fine to coarse sand, 34% subangular to subrounded gravel to >35 mm. Weak cemented.	
706.88	3	3.05						SP SM		
	3.28	B	MC	50 50/75	50/75	80	SV, PI			
705.88	4	4.57						SC		
	4.86	C	SPT	38 50/138	50/138	80	SV, PI			
704.88	5							CL	5.49 Clayey Sand ; light brown, moist, very dense, with 44% medium plastic fines, 55% fine to coarse sand and 3% subangular to subrounded gravel to 25 mm.	
703.88	6	6.10							7.01 Sandy Lean Clay ; light brown, moist, very hard, with 50% high plastic fines, 42% fine to coarse sand and 8% subangular to subrounded gravel to >25 mm.	
	6.55	D	MC	32 50 50	100	67	SV, PI	SC		
702.88	7									
	7.62							SC		
701.88	8	8.05	E	SPT	25 35 50/125	50/125	55	SV, PI		
700.88	9	9.14						SC	8.53 Clayey Sand ; light brown, moist, very dense, with 48% medium plastic fines, 52% fine to coarse sand and trace subangular to subrounded gravel to >38 mm. Weak cemented.	
	9.43	F	MC	65 75/138	75/138	65	SV, PI		9.75 Sandy Fat Clay ; light brown, moist, very hard,	



EXPLORATION LOG

SHEET 2 OF 2

START DATE 3/21/02
 END DATE 3/21/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-34
 E.A. # 0324-01-4
 GROUND ELEV. 709.88 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/21/02</u>	<u>NE</u>	

STATION 79+80 "95-S"
 OFFSET
 ENGINEER
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 3/21/2002

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		Percent Reco'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm					
	10.67									
698.88	10.93	G	SPT	40 50/100	50/100	100	SV, PI	CH	with 52% high plastic fines, 48% fine to coarse sand and trace subangular gravel to 15 mm.	
	11									
697.88	12.19							SC	11.58	Clayey Sand ; light orange brown, moist, very dense, with 33% medium plastic fines and 67% fine to coarse sand.
	12.34	H	MC	75/138	75/138	100	SV, PI			
696.88	13							SC	13.11	Clayey Sand with Gravel ; light brown, moist, very dense, with 29% medium plastic fines, 54% fine to coarse sand and 17% subangular to subrounded gravel to >35 mm.
	13.72									
695.88	14 14.17	I	SPT	32 45 50	95	60	SV, PI	SC		
	15									
694.88	15.24	J	MC	75/50	75/50	0			15.30	
693.88	16									
692.88	17									
691.88	18									
690.88	19									

JDT 02
GDT
GPJ
DOT



EXPLORATION LOG

SHEET 1 OF 1

START DATE 3/21/02
 END DATE 3/21/02
 JOB DESCRIPTION US 95 Widening Project / Retaining-Sound Walls
 LOCATION Las Vegas, Nevada
 BORING B-35
 E.A. # 0324-01-4
 GROUND ELEV. 707.44 (m)
 HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>3/21/02</u>	<u>NE</u>	

STATION 78+40 "95-S"
 OFFSET 30 m LT
 ENGINEER PGT
 EQUIPMENT Diedrich D-50
 OPERATOR Eagle Drilling
 DRILLING METHOD 152 mm HS Auger
 BACKFILLED Yes DATE 3/21/2002

ELEV. (m)	DEPTH (m)	SAMPLE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
			NO.	TYPE	150 mm Increments	Last 300 mm	Percent Recov'd		
706.44	1								
1.52									
1.68	A	SPT	50/50	50/50	0				
705.44	2	A'	AC			50	SV, PI		
704.44	3	3.05	B	MC	75/75	75/75	100	SV, PI	
703.44	4								
4.57									
4.72	C	SPT	50/50	50/50	0				
702.44	5	5.18	C'	AC			50	SV, PI	
701.44	6	6.10							
6.37	D	MC	50 75/113	75/113	100		SV, PI		
700.44	7								
699.44	8								
698.44	9								



EXPLORATION LOG

SHEET 1 OF 1

START DATE 2/22/02END DATE 2/22/02JOB DESCRIPTION US 95 Widening Project / Rainbow BridgeSTATION 91+74 QN-2COFFSET 37 m LTENGINEER PGTEQUIPMENT Diedrich D-50OPERATOR Eagle DrillingDRILLING METHOD 152 mm HS AugerBACKFILLED Yes DATE 2/22/2002LOCATION Las Vegas, NevadaBORING B-36E.A. # GROUND ELEV. 728.78 (m)

GROUNDWATER LEVEL

DATE 2/22/02DEPTH m NEELEV. m HAMMER DROP SYSTEM Cable

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm					
727.78	0.76							SC	0.06 Asphalt Concrete Concrete ; thick approach slab with internal 0.43 15-mm-diameter rebar. Rebar occurs in at least 4 layers.	Hole located on southbound shoulder 3 feet south of bridge abutment on south side of Rainbow bridge.
	1.22	A	MC	34 31 34	65	33				
	1.52									
	1.98	B	SPT	18 24 19	43	60	SV, PI			
	2.29									
	2.74	C	MC	14 24 32	56	33				
	3.05									
	3.23	C	SPT	50 50/25	50/25	100				
	3.81									
	3.96	D	MC	80/125	80/125	80				
724.78	4									
	5									
	6									
	7									
	8									
	9									



EXPLORATION LOG

SHEET 1 OF 1

START DATE 2/22/02

END DATE 2/22/02

JOB DESCRIPTION US 95 Widening Project / Rainbow Bridge

LOCATION Las Vegas, Nevada

BOILING

BORING

E.A. #

GROUND ELEV. 727.00 (M)

HAMMER DROP SYSTEM Cable

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
2/22/02	NE	

STATION	92+02 QN-2C
OFFSET	27 m RT
ENGINEER	PGT
EQUIPMENT	Diedrich D-50
OPERATOR	Eagle Drilling
DRILLING METHOD	152 mm HS Auger
BACKFILLED	Yes DATE 2/22/2002



EXPLORATION LOG

SHEET 1 OF 1

START DATE	2/21/02	STATION	91+90 QN-2C	
END DATE	2/21/02	OFFSET	3 m LT	
JOB DESCRIPTION	US 95 Widening Project / Rainbow Bridge	ENGINEER	PGT	
LOCATION	Las Vegas, Nevada	EQUIPMENT	Diedrich D-50	
BORING	B-39	OPERATOR	Eagle Drilling	
E.A. #		DRILLING METHOD	152 mm HS Auger	
GROUND ELEV.	721.77 (m)	BACKFILLED	Yes DATE 2/22/2002	
HAMMER DROP SYSTEM	Cable	GROUNDWATER LEVEL		
		DATE	DEPTH m	ELEV. m
		2/22/02	NE	

ELEV. (m)	DEPTH (m)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT			LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
				150 mm Increments	Last 300 mm	Percent Recov'd				
720.77	1							GP GM	-0.11 Asphalt Concrete Poorly Graded Gravel with Silt and Sand Fill ; light grey brown, slightly moist, dense, with estimated 10% low plastic fines, 35-40% fine to coarse sand and 50-55% subrounded gravel to 50 mm. Encountered top of Rainbow bridge base footing at 1.98 meters. According to plans supplied by PBS&J, this wider base footing is 1.22 meters (4 feet) thick. A smaller 0.914 (3-foot) thick footing sits on top of the base footing. Accordingly, the top of the footing complex is at a depth 1.07 meters below the <u>existing grade</u> .	Hole located on inside shoulder of northbound US 95 beneath west side of Rainbow bridge. Site is about 9 feet NW of westernmost column and targets NW corner of base footing. The footing extends 11 feet to west and 7 feet to north of column.
719.77	2									
718.77	3									
717.77	4									
716.77	5									
715.77	6									
714.77	7									
713.77	8									
712.77	9									



EXPLORATION LOG

SHEET 1 OF 1

START DATE	4/12/02	STATION	
END DATE	4/12/02	OFFSET	
JOB DESCRIPTION	US 95 Widening Project / Washington Avenue Bridge		
LOCATION	Las Vegas, Nevada		
BORING	B-40		
E.A. #	0324-01-6		
GROUND ELEV.	(m)	GROUNDWATER LEVEL	
		DATE	DEPTH m
		4/12/02	NE
HAMMER DROP SYSTEM		ELEV. m	
Cable			

ELEV. (m)	DEPTH (m)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT 150 mm Increments	Last 300 mm	Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
	0.76	A	MC	75/75	75/75	100	SV, PI		Clayey Sand with Gravel Fill ; light grey brown, slightly moist, very dense, with 25-30% medium plastic fines, 50-55% fine to coarse sand and 15-25% subangular gravel to >50 mm.	Boring Site on the North Side of the East Embankment.
	1							SC		
	1.52	B	MC	60 75/100	75/100	40	SV, PI			
	2									
	2.29	C	MC	75/125	75/125	80	SV, PI			
	3 3.05									
	3.51	D	MC	59 63 60	123	67	SV, PI		Clayey Gravel with Sand Gravel Fill ; light grey brown, slightly moist, very dense, with 15-20% medium plastic fines, 40-45% fine to coarse sand and 40-45% subangular gravel to >50 mm.	
	3.81	E	MC	75/100	75/100	80	SV, PI			
	4									
	4.57	F	MC	75/125	75/125	0				
	5									
	5.33	G	MC	75/125	75/125	0	SV, PI			
	6 6.10									
	6.36	H	MC	70 75/75	75/75	60	SV, PI			
	6.86	I	MC	75/75	75/75	0	SV, PI			
	7									
	7.62	J	MC	75/50	75/50	0	SV, PI			
	8									
	8.38	K	MC	75/50	75/50	0	SV, PI			
	9 9.14	L	MC	75/75	75/75	0				
									9.22	



EXPLORATION LOG

SHEET 1 OF 1

START DATE 4/12/02
 END DATE 4/12/02

JOB DESCRIPTION US 95 Widening Project / Washington Avenue BridgeLOCATION Las Vegas, NevadaBORING B-41E.A. # 0324-01-6GROUND ELEV. (m)HAMMER DROP SYSTEM CableSTATION
OFFSET

PGT

Diedrich D-50

Eagle Drilling

ENGINEER

EQUIPMENT

OPERATOR

DRILLING

METHOD

152 mm HS Auger

BACKFILLED

Yes DATE 4/12/2002

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
<u>4/12/02</u>	<u>NE</u>	

ELEV. (m)	DEPTH (m)	SAMPLE NO.	SAMPLE TYPE	BLOW COUNT 150 mm Increments	BLOW COUNT Last 300 mm	Percent Reco'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
	0.76									
-1	1.22	A	MC	26 41 62	103	45	SV, PI	SC	Silty, Clayey Sand with Gravel Fill ; light grey brown, slightly moist, dense to very dense, with 10-15% low plastic fines, 45-50% fine to coarse sand and 40-45% subangular gravel to >75 mm.	
	1.52							SM		
-1	1.80	B	MC	41 75/125	75/125	55	SV, PI			
	2									
-1	2.29									
-1	2.55	C	MC	61 75/100	75/100	60	SV, PI			
	3.05									
-1	3.31	D	MC	67 75/50	75/50	65	SV, PI	GP	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 5-10% low plastic fines, 30-35% fine to coarse sand and 60-65% subangular gravel to >75 mm.	
	3.81							GC		
-1	4.08	E	MC	34 75/125	75/125	90	SV, PI			
	4.57									
-1	5.00	F	MC	30 62 75/125	75/125	85	SV, PI	GC	Silty, Clayey Gravel with Sand Fill ; light grey brown, slightly moist, very dense, with estimated 15-20% low plastic fines, 30-35% fine to coarse sand and 55-60% subangular gravel to >75 mm.	
	5.33	G	MC	75/100	75/100	100	SV, PI			
	6.10									
-1	6.37	H	MC	66 75/125	75/125	80	SV, PI	SC	Clayey Sand with Gravel Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 45-50% fine to coarse sand and 40-45% subangular gravel to >35 mm.	
	7									
	8									
	9									



EXPLORATION LOG

SHEET 1 OF 1

START DATE	4/12/02	STATION	97+15 QN-2C		
END DATE	4/12/02	OFFSET	43 m LT		
JOB DESCRIPTION	US 95 Widening / Project 2D Retaining Walls	ENGINEER	PGT		
LOCATION	Las Vegas, Nevada	EQUIPMENT	Diedrich D-50		
BORING	B-42	OPERATOR	Eagle Drilling		
E.A. #	0324-01-1	DRILLING METHOD	152 mm HS Auger		
GROUND ELEV. (m)		BACKFILLED	Yes DATE 4/12/2002		
HAMMER DROP SYSTEM	Cable	GROUNDWATER LEVEL			
		DATE	DEPTH m	ELEV. m	
		4/12/02	NE		

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION		REMARKS	
		NO.	TYPE	150 mm Increments	Last 300 mm							
	0.76	A	MC	75/50	75/50	0	SV, PI	GC	Clayey Gravel with Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low to medium plastic fines, 35-40% fine to coarse sand and 50-55% subangular gravel to 75 mm.		Boring Site on the North Side of the West Embankment. Sampled auger cuttings from 15-30 feet.	
	1											
	1.52	B	MC	75/75	75/75	100	SV, PI					
	2							SC				
	2.29	C	MC	75/75	75/75	67	SV, PI		2.44 Clayey Sand with Gravel Fill ; light grey brown, slightly moist, very dense, with 20-25% medium plastic fines, 45-50% fine to coarse sand and 25-30% subangular gravel to >35 mm.			
	3 3.05	D	MC	75/125	75/125	100	SV, PI					
	3.81	E	MC	75/75	75/75	0		GC	3.66 Clayey Gravel with Sand Fill ; light grey brown, slightly moist, very dense, with 15-20% medium plastic fines, 35-40% fine to coarse sand and 45-50% subangular gravel to >50 mm.			
	4 4.11	F	MC	75/125	75/125	60	SV, PI					
	4.57	G	MC	75/50	75/50	0	SV, PI		4.88 Clayey Gravel with Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low to medium plastic fines, 30-35% fine to coarse sand and 50-55% subangular gravel to 75 mm.			
	5							SC				
	5.33	H	MC	75/75	75/75	0	SV, PI					
	6 6.10	I	MC	75/75	75/75	0						
	6.86	J	MC	75/12.5	75/12.5	0		GC	6.71 Clayey Sand with Gravel ; light grey brown, slightly moist, very dense, with 15-20% medium plastic fines, 45-50% fine to coarse sand and 35-40% subangular gravel to >35 mm.			
	7											
	7.62	K	MC	75/100	75/100	0	SV, PI					
	8							SC				
	8.38	L	MC	75/75	75/75	33	SV, PI					
	9 9.14	M	MC	75/75	75/75	100	SV, PI		9.22			



EXPLORATION LOG

SHEET 1 OF 1

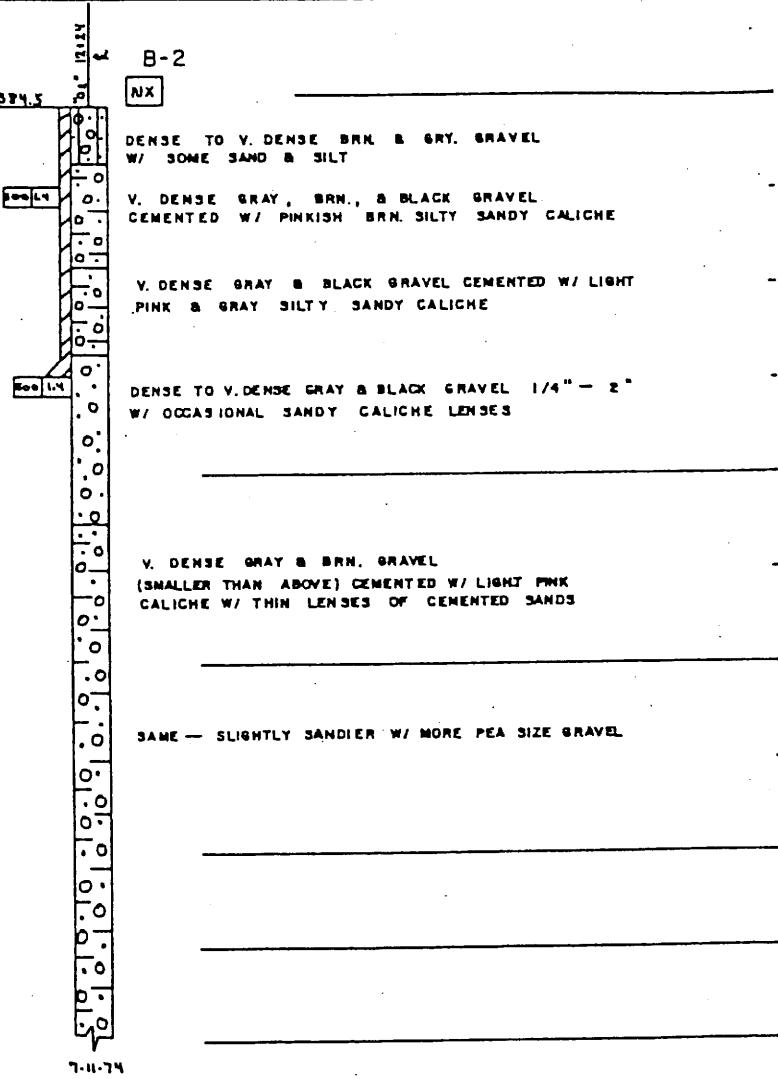
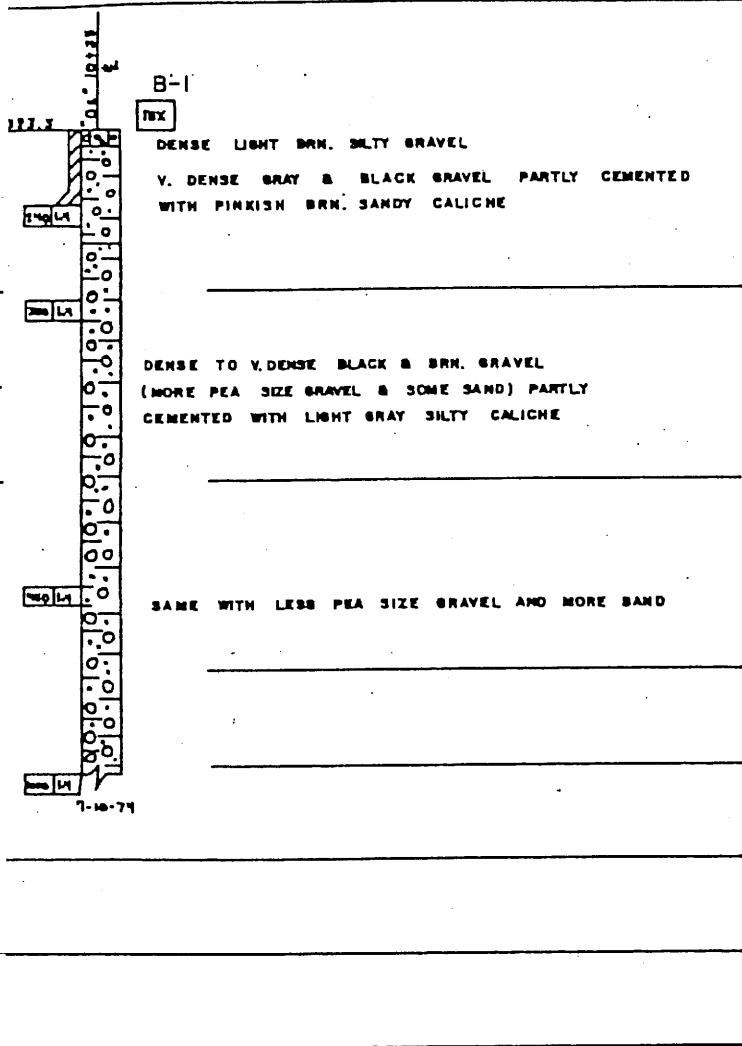
START DATE 4/12/02END DATE 4/12/02JOB DESCRIPTION US 95 Widening / Project 2D Retaining WallsLOCATION Las Vegas, NevadaBORING B-43E.A. # 0324-01-1GROUND ELEV. (m)HAMMER DROP SYSTEM CableSTATION 96+95 QN-2COFFSET 43 m LTENGINEER PGTEQUIPMENT Diedrich D-50OPERATOR Eagle DrillingDRILLING METHOD 152 mm HS AugerBACKFILLED Yes DATE 4/12/2002

GROUNDWATER LEVEL		
DATE	DEPTH m	ELEV. m
4/12/02	NE	

ELEV. (m)	DEPTH (m)	SAMPLE		BLOW COUNT		Percent Recov'd	LAB TESTS	USCS Group	MATERIAL DESCRIPTION	REMARKS
		NO.	TYPE	150 mm Increments	Last 300 mm					
	0.76									
-1	1.04	A	MC	64 75/125	75/125	35	SV, PI	GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 5-10% low plastic fines, 25-30% fine to coarse sand and 60-65% subangular gravel to >70 mm.	Boring Site on the South Side of the West Embankment.
	1.52									
-1	1.80	B	MC	38 75/125	75/125	75	SV, PI	SC	Clayey Sand with Gravel Fill ; light grey brown, slightly moist, very dense, with 15-20% low to medium plastic fines, 50-55% fine to coarse sand and 30-35% subangular gravel to >70 mm.	
	2							GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	2.29							SC	Clayey Sand with Gravel Fill ; light grey brown, slightly moist, very dense, with 15-20% medium plastic fines, 45-50% fine to coarse sand and 30-35% subangular gravel to >70 mm.	
-1	2.74	C	MC	36 64 73	137	85	SV, PI	GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	3.05							SC	Clayey Sand with Gravel Fill ; light grey brown, slightly moist, very dense, with 15-20% medium plastic fines, 45-50% fine to coarse sand and 30-35% subangular gravel to >70 mm.	
-1	3.51	D	MC	71 71 64	135	95	SV, PI	GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	3.81							SC	Clayey Sand with Gravel Fill ; light grey brown, slightly moist, very dense, with 15-20% medium plastic fines, 45-50% fine to coarse sand and 30-35% subangular gravel to >70 mm.	
-1	4.08	E	MC	49 75/125	75/125	90	SV, PI	GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	4.57	F	MC	75/75	75/75	0		SC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	5							GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
-1	5.33	G	MC	75/125	75/125	80	SV, PI	SC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	6							GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
-1	6.10	H	MC	75/75	75/75	100	SV, PI	SC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	7							GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	8							SC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	
	9							GP GC	Poorly Graded Gravel with Silt, Clay and Sand Fill ; light grey brown, slightly moist, very dense, with 10-15% low plastic fines, 40-45% fine to coarse sand and 45-50% subangular gravel to >70 mm.	

NDOT 1974 Boring

B-2



ROTARY BORING		PENETRATION BORING		NA. DIV. L
B- NO.	Top Hole Elev.	B- NO.	Top Hole Elev.	
Top Hole Elev. inches	Size	Sample Number	Pushed	P
Foot (Using a meter with a 30° Noted)		Unit Weight Wet (lb/ft³)		
Bed Compressive Strength (ft²)		Water Content	No Count Recorded	NC
(T/ft²)		○ Consolidation	Blows Per Foot	14
(T/ft²)		○ Direct Shear		25
		○ Triaxial Compression		37
		○ Atterberg Limits		54
		Conformable Material Change	Average Skin Friction above this point	68
		Estimated Material Change	(T/ft²)	90
		Description of Material		158
		Unconformable Material Change		50 100 150 200
			Blows Per Foot	

● PLAN OF ANY BORING
PENETROMETER
(FLUSH-COUPLED)

● 2" CONE PENETROMETER

■ SAMPLER BORING (DRY)

● ROTARY BORING (WET)

□ AUGER BORING (DRY)

JET BORING

◆ DIAMOND CORE
BORING.

TEST PIT.

BIT SIZES: (0,0,1) "A"=1-1/16", "B"=2-9/16",
"C"=2-7/8", "D"=1-1/2".

CASING SIZES: (0,0,1) "B"=2-7/8", "H"=1-1/2".

DNW Q.Q.Q.

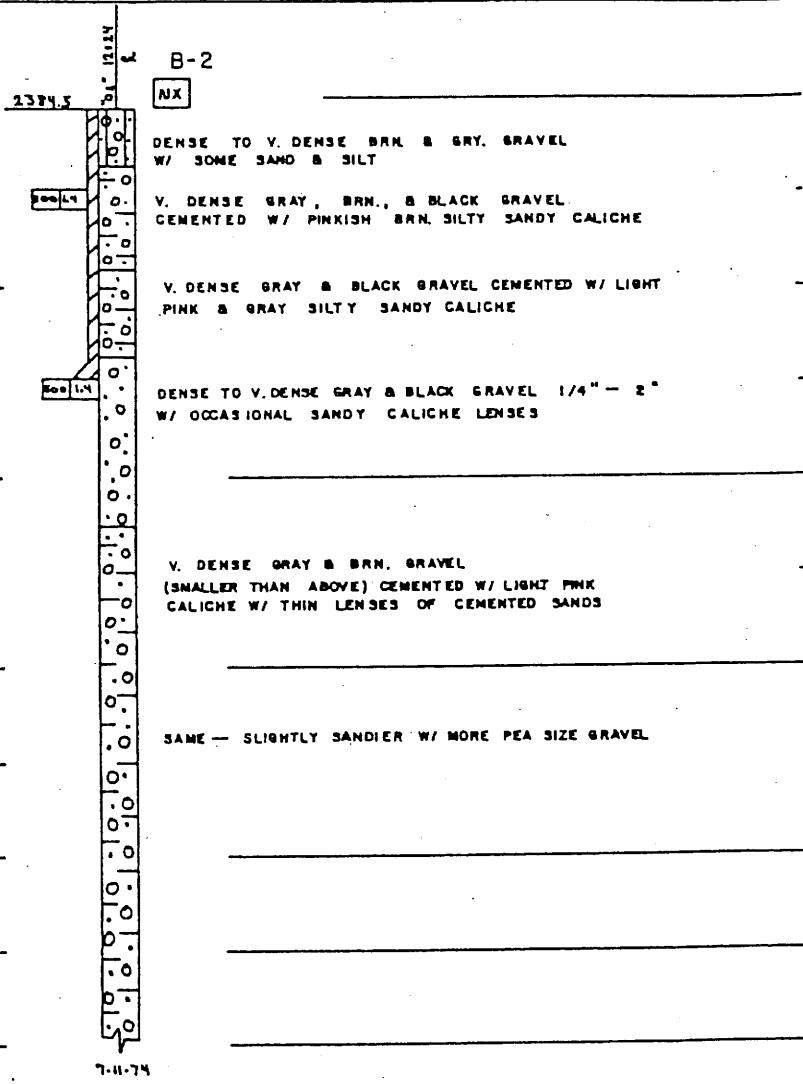
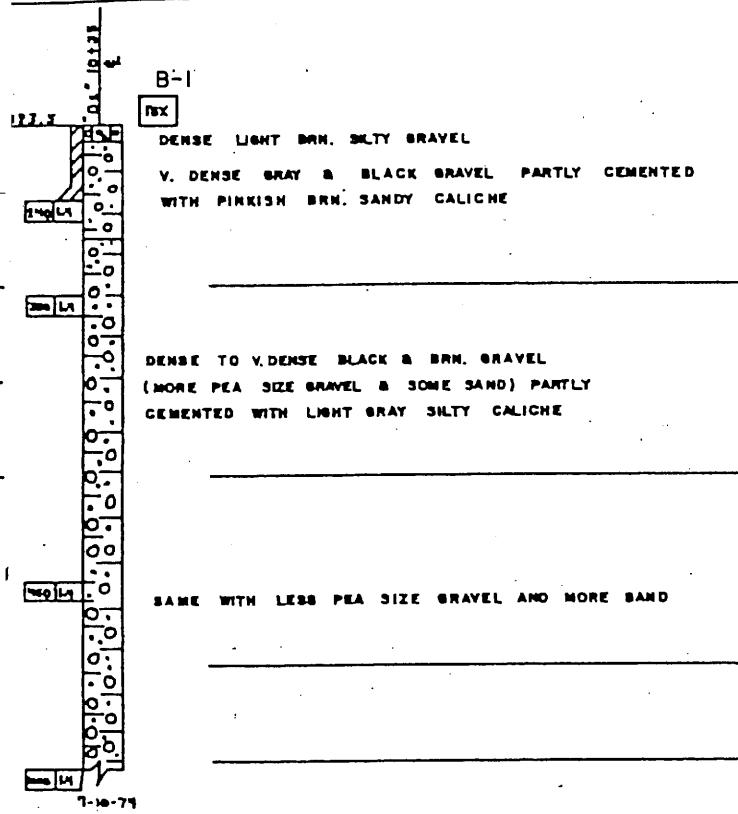
CNR. JEPK X.

DATE 0-7-74

NEVADA HIGHWAY DEPART
FOUNDATIONS A

NDOT 1974 Boring

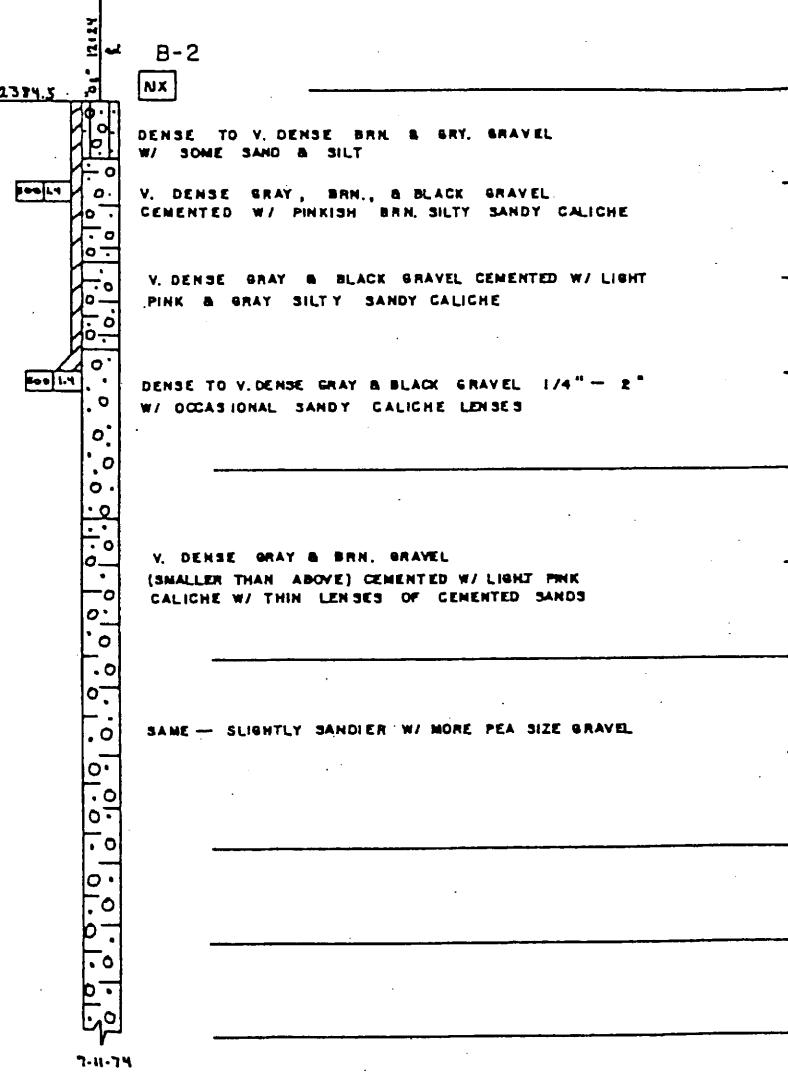
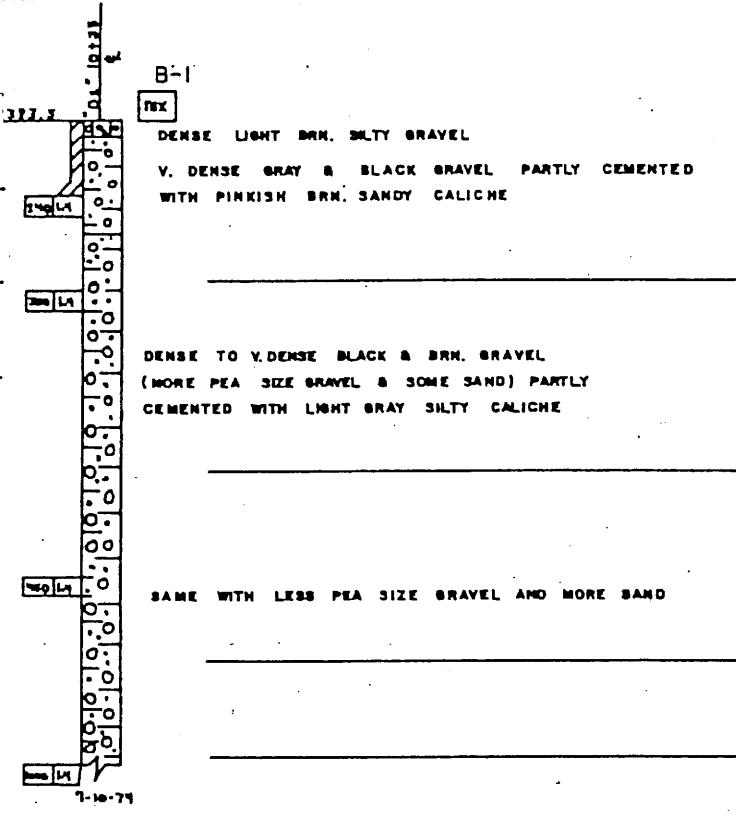
B-2



ROTARY BORING		PENETRATION BORING		AUGER BORING (DRY)	
Top Hole Elev. en Foot (Using a mer with a 30° Noted)	B- NO.	Top Hole Elev. Pushed Size	B-NO. Size	PLAN OF ANY BORING PENETROMETER (FLUSH-COUPLED) 2" CONE PENETROMETER SAMPLER BORING (DRY) ROTARY BORING (WET)	
ed Compressive T/ft^2	Sample Number Unit Weight Wet (lb/ft^3) Water Content ① Consolidation ② Direct Shear ③ Triaxial Compression ④ Atterberg Limits Conformable Material Change Estimated Material Change Description of Material Unconformable Material Change	No Count Recorded Blows Per Foot	G.W.S. (Water) ▼ Elev. Date Measured Graphic Presentation of Penetration.	JET BORING DIAMOND CORE BORING, TEST PIT.	
T/ft^2	Average Skin Friction above this point T/ft^2	25 37 54 68 90 158	25 37 54 68 90 158	BIT SIZES: (D.D.I) "A"=1-13/16", "B"=2-9/12", "C"=2-29/32" CASING SIZES: (D.D.I) "B"=2-7/8", "H"=3-1/2"	
		50 100 150 200	Blows Per Foot	CORE GRAINED Material Sand and Silty Soil Gravel and Gravelly Soil	
				DATE 0-7-74	
				NEVADA HIGHWAY DEPART. FOUNDATIONS A	

NDOT 1974 Boring

B-2



ROTARY BORING		PENETRATION BORING		AUGER BORING (DRY)	
<p>B - NO.</p> <p>Top Hole Elev. [ft]</p> <p>pler (Inches) _____</p> <p>Foot (Using a 30° Summer with a 30° Noted)</p> <p>ed Compressive (ft²) _____</p> <p>T/f² _____</p> <p>(T/f²) _____</p>		<p>B - NO.</p> <p>Top Hole Elev. [ft]</p> <p>Pushed _____</p> <p>Sample Number _____</p> <p>Unit Weight Wet (lb/ft³) _____</p> <p>Water Content _____</p> <p>Consolidation _____</p> <p>Direct Shear _____</p> <p>Triaxial Compression _____</p> <p>Atterberg Limits _____</p> <p>Conformable Material Change _____</p> <p>Estimated Material Change _____</p> <p>Description of Material _____</p> <p>Unconformable Material Change _____</p>		<p>PLAN OF ANY BORING</p> <p>PENETROMETER (FLUSH-COUPLED)</p> <p>2" CONE PENETROMETER</p> <p>SAMPLER BORING (DRT)</p> <p>ROTARY BORING (WET)</p> <p>JET BORING</p> <p>DIAMOND CORE BORING</p> <p>TEST PIT</p> <p>BIT SIZES: (I.D.) "A"=1-1/16", "B"=2-9/16", "H"=2-29/32"</p> <p>CASING SIZES: (I.D.) "B"=2-7/8", "H"=3-1/2"</p>	
				<p>NEVADA HIGHWAY DEPART FOUNDATIONS A</p>	

NORTH
BOUND
EXPRESSWAY

B-1
EAST
A.R.T.

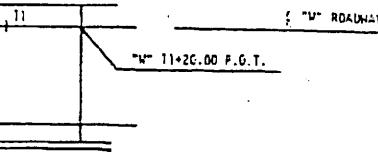
FED ED REG NC	STATE	PROJECT NO.	COUNTY	SHEET
9	NEVADA	I-80-2(1)	CLARK	B-24

NOTE: FOUNDATION REPORT AVAILABLE FOR CONTRACTORS STUDY
IN DISTRICT OFFICE AND MATERIALS & TESTING DIVISION

B-24

E" 556+76.12 P.O.T.
W" 10+00.00 P.O.T.

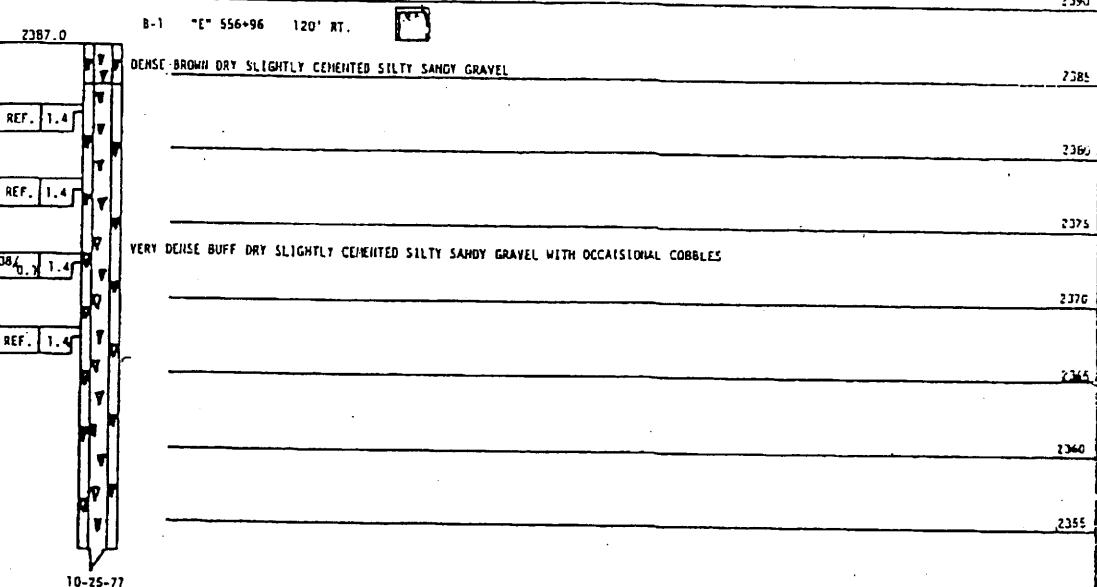
AVE. →



120' 0"

NDOT 1977 Boring

B - 1



THE UNIFIED SOIL CLASSIFICATION SYSTEM		STANDARD PENETRATION CLASSIFICATION		
LAYER	STN.	DESCRIPTION	GRANULAR SOIL	CLAYEY SOIL
GW		WELL-GRADED GRAVEL OR GRAVEL-SAND MIXTURES. LITTLE OR NO FINES.	ML	INORGANIC SILT AND VERY FINE SAND. ROCK FLUO. SILTY OR CLAYEY FINE SAND OR COARSE SILT WITH SLIGHT PLASTICITY.
GP		POORLY-GRADED GRAVEL OR GRAVEL-SAND MIXTURES. LITTLE OR NO FINES.	CL	INORGANIC SILT OF HIGH TO MEDIUM PLASTICITY. CLAYEY CLAY. SANDY CLAY.
GM		SILTY GRAVEL, GRAVEL-SAND-SILT MIXTURES.	OL	ORGANIC SILT AND INORGANIC SILTY-CLAY OF LOW PLASTICITY.
GC		GRAVEL GRAVEL, GRAVEL-SAND-CLAY MIXTURES.	MH	INORGANIC SILT, MICACEOUS OR DIATOMACEOUS FINE SAND OR SILTY SOILS. ELASTIC SILT.
SH		WELL-GRADED SAND OR GRAVELLY SAND, LITTLE OR NO FINES.	CH	INORGANIC CLAY OF HIGH PLASTICITY. FAT CLAY.
SP		POORLY-GRADED SAND OR GRAVELLY SAND. LITTLE OR NO FINES.	OM	ORGANIC CLAY OF MEDIUM TO HIGH PLASTICITY. ORGANIC SILT.
SH		SILTY SAND, SAND-SILT MIXTURES.	PT	PEAT AND OTHER HIGHLY ORGANIC SOILS.
SC		CLAYEY SAND, SAND-CLAY MIXTURES.		
MENT MATERIALS AND TESTING DIVISION AND ENGINEERING GEOLOGY SECTION		WASHINGTON AV. G.S.-L.V. EXPRESSWAY H-1211 US 95-CL 82.05		DWG. NO. 1

BORING 9

DATE DRILLED: 05-20-86
LOCATION: SEE KEY PLAN

ELEVATION: 2401.4

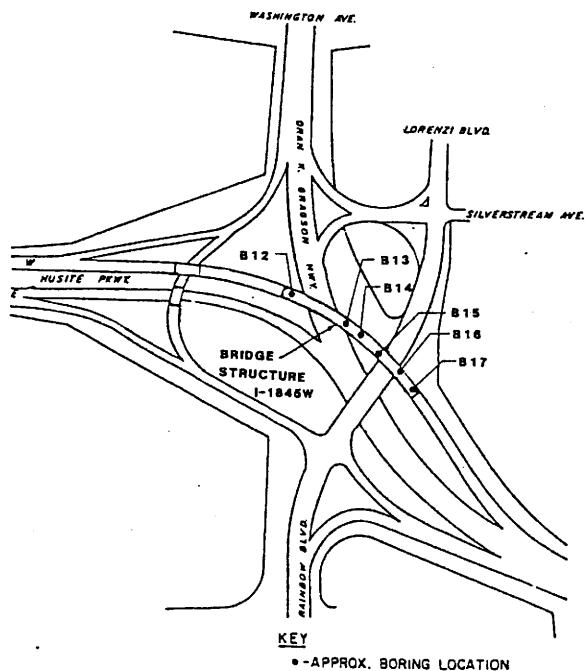
BORING 10

DATE DRAILED : 05-20-86
LOCATION: SEE KEY PLAN

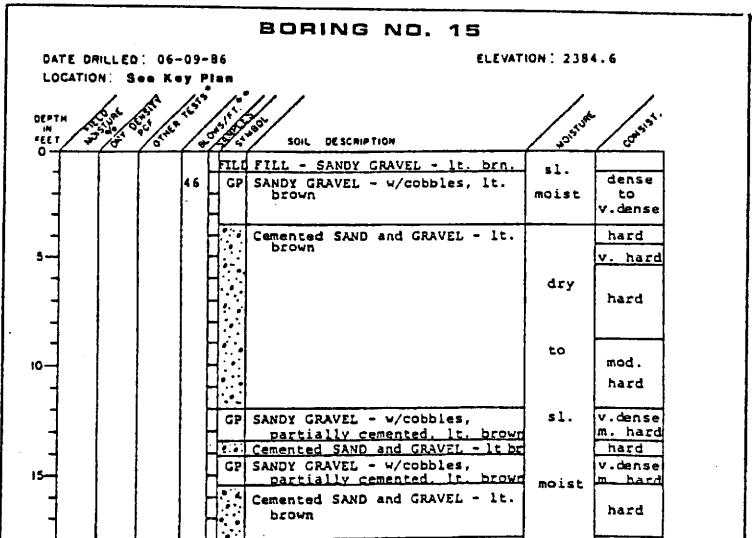
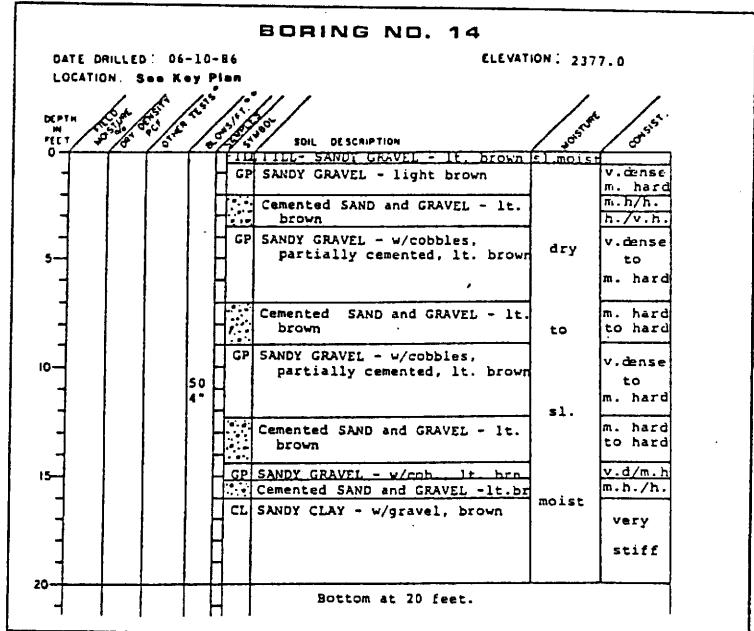
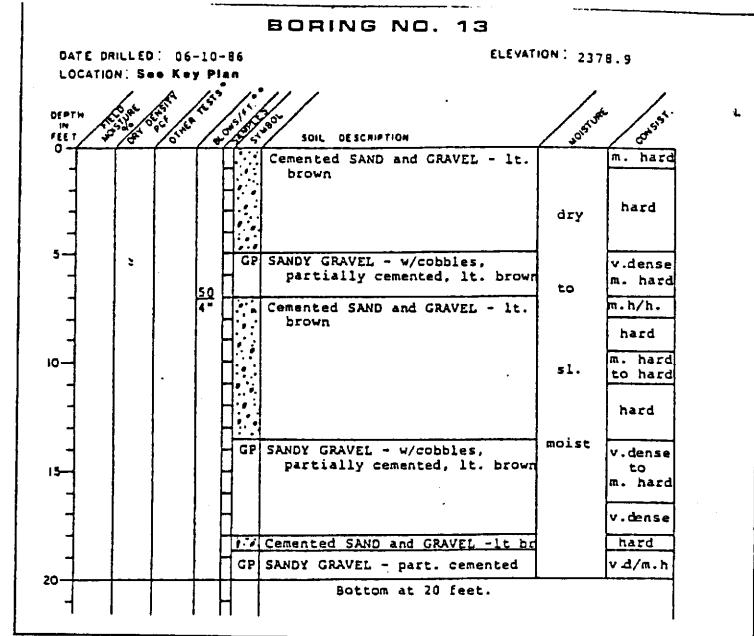
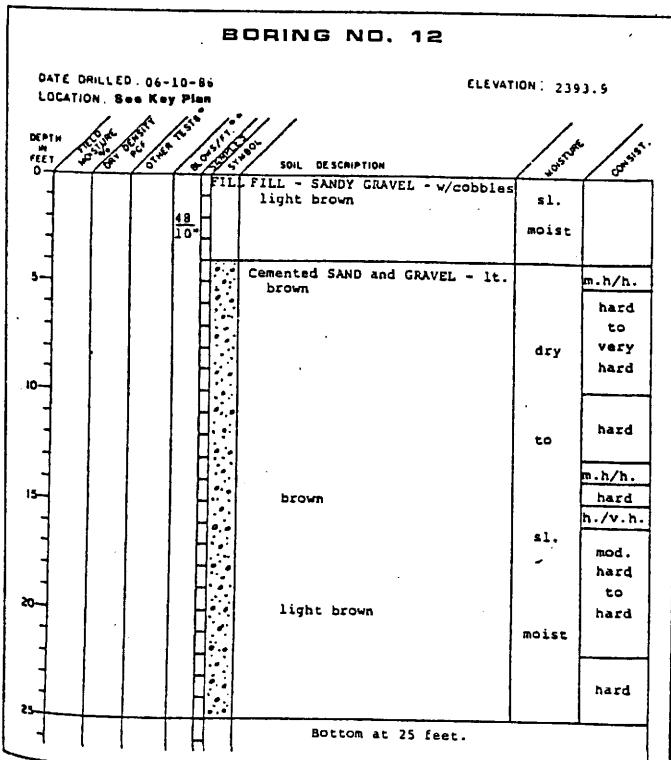
ELEVATION : 2398.6

Bottom at 20 feet.

SHEET B56, OMITTED



KEY PLAN



BORING NO. 16

DATE DRILLED: 06-09-86
LOCATION See Key Plan

ELEVATION: 2384.6

FLW. NO. REG. NO.	STATE	PROJECT NO.	COUNTY
9	NEV.	SPS-095-2(4)	CLARK

ACCOMPLISHED	DESCRIPTION	
	REV	DATE
GEORGE C. WALLACE	1015	July 1967
	N.E. NO.	DALE

RECOMMENDED
GEORGE C. WALL

EXPLANATION OF
MATERIAL CLASSIFICATIONS

BORING NO. 17

ELEVATION: 2380.8

MAJOR	DIVISIONS	Group symbols	TYPICAL NAMES	
			GW	GL
COURSE GRAINED SOILS			Well graded gravels, gravel-sand mixtures, little or no fines.	
	CLEAN GRAVELS Little or no fines	GM	Poorly graded gravels or gravel-sand mixtures, little or no fines.	
	GRAVELS More than 50% of coarse part is larger than the No. 200 sieve.	GC	Silty gravels, gravel-sand-silt mixtures.	
	GRAVELS WITH FINES Appreciable amount of fines	SW	Clayey gravels, gravel-sand-clay mixtures.	
	CLEAN SANDS Little or no fines	SP	Well graded sands, gravelly sands, little or no fines.	
	SANDS More than 50% of coarse part is smaller than the No. 200 sieve.	SM	Poorly graded sands or gravelly sands, little or no fines.	
	SANDS WITH FINES Appreciable amount of fines	SC	Silty sands, sand-silt mixtures.	
FINE GRAINED SOILS		M L	Inorganic silts & very fine sands, rock flour, silt or clayey fine sands or clayey silts with slight plasticity.	
	SILTS AND CLAYS Liquid limit LESS than 50	CL	Inorganic silts of low to med. plasticity, gravelly silty sand, sandy clays, silty clays, lean clays.	
		OL	Organic silts and organic silty clays of low plasticity.	
		MH	Inorganic silts, micaceous or diatomaceous fine sand or silty soils, elastic silts.	
	SILTS AND CLAYS Liquid limit GREATER than 50	CH	Inorganic clays of high plasticity, for clays.	
		OH	Organic clays of medium to high plasticity, organic silts.	
HIGHLY ORGANIC SOILS		PT	Pest and other highly organic soils.	

BOUNDARY CLASSIFICATIONS: Soils possessing characteristics of two groups are designated by combinations of group symbols.

PARTICLE SIZE LIMITS							
soil or clay	sand			gravel		cobbles	boulders
	fine	medium	coarse	fine	coarse		
silt or clay							

No. 100	No. 40	No. 0	No. 4	3/4"	3"	12"
U. S. STANDARD SIEVE SIZE						

DESCRIPTIVE TERMS USED WITH SOILS	
CONSISTENCY	MOISTURE CONTENT

	Soils and Geol.	Spatial Soil Groups	Wetness	Soil
Strongest ↑	very stiff	very dense		very moist moist

Soil **Moisture**
 firm medium dense moist
 soft loose slightly moist
 wet dry

DESCRIPTIVE TERMS USED WITH CALICHE AND CEMENTED SOILS

	CALICHE	SAND AND GRAVEL	STANDARD GEOLOGIST'S HAMMER
strong	very hard	very hard	Difficult to scratch or break.

hard hard Scratches leave only dust, requires many hammer blows to break.

moderately hard	moderately hard	Can be readily cut with hand and crumbles with several hammer blows.
extremely indurated	extremely compacted	Crushes easily with hands and crumbles

partially cemented partially cemented Cements easily with lime and cements readily with a few blows of a hammer

10. The following table shows the number of hours worked by each employee.

OTHER TESTS: C-CONSOLIDATION,

A-ATTERBERG, S-SHEAR, G-GRAIN SIZE,

E-EXPANSION, CH-CHEMICAL

UNLOAD SPEED, BRINING WEIGHT, AND ROLL

* OTHER TESTS: C-CONSOLIDATION,
A-ATTERBERG, S-SHEAR, G-GRAIN SIZE,
E-EXPANSION, CH-CHEMICAL

**** USING 370 LB. DRIVING WEIGHT AND 2.625 INCH. (I.D.) DIAMETER SAMPLER**

NOTE: WATER NOT ENCOUNTERED

LOG OF BORINGS

BORING 18DATE DRILLED: 05-20-86
LOCATION: See Plate NO. 1

ELEVATION: 2400.5

DEPTH IN FEET	TEST NO.	TEST NAME	TEST NO.	TEST NAME	TEST NO.	TEST NAME	TEST NO.	TEST NAME	SOIL DESCRIPTION	WATER LEVEL	CONSIST.
0									SM SILTY SAND - w/grv. and cobbles	sl. moist	loose/m.
									GP SANDY GRAVEL - w/cobbles, brown	dense	dense
									Cemented SAND and GRAVEL - lt. brown	m.h./h.	m.h./h.
5										hard	hard
										mod.	mod.
										hard	hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dense	very dense
10									Cemented SAND and GRAVEL - lt. br.	m. hard	mod. hard
										m.h./h.	to hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dense	mod. hard
15									Cemented SAND and GRAVEL - lt br	m. hard	mod. hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dense	mod. hard
									Cemented SAND and GRAVEL - lt br	m. hard	mod. hard
20									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	m. hard	mod. hard
									Cemented SAND and GRAVEL - lt br	hard	mod. hard
									Bottom at 20 feet.		

BORING 19DATE DRILLED: 05-28-86
LOCATION: See Plate NO. 1

ELEVATION: 2401.6

DEPTH IN FEET	TEST NO.	TEST NAME	TEST NO.	TEST NAME	TEST NO.	TEST NAME	TEST NO.	TEST NAME	SOIL DESCRIPTION	WATER LEVEL	CONSIST.
0									SM SILTY SAND - w/grv. and cobbles	sl. moist	loose
									GP SANDY GRAVEL - w/silt and cob.	dense	dense
									GP SANDY GRAVEL - w/cob., lt. brn.	v.d/m.h.	v.d/m.h.
5									Cemented SAND and GRAVEL - lt. brown	m.h./h.	mod. hard
										hard	mod. hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dense	mod. hard
10									Cemented SAND and GRAVEL - lt br	m. hard	mod. hard
										hard	mod. hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dense	mod. hard
15									Cemented SAND and GRAVEL - lt br	m. hard	mod. hard
										hard	mod. hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dens.	mod. hard
20									Cemented SAND and GRAVEL - lt br	m. hard	mod. hard
										hard	mod. hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dens.	mod. hard
25									Cemented SAND and GRAVEL - lt. brown	sl.	mod. hard
										hard	mod. hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dens.	mod. hard
30									Cemented SAND and GRAVEL - lt br	m. hard	mod. hard
										hard	mod. hard
									GP SANDY GRAVEL - w/cob., lt. brn.	v.d/m.h.	mod. hard
35									Cemented SAND and GRAVEL - lt. brown	sl.	mod. hard
										hard	mod. hard
									GP SANDY GRAVEL - w/cobbles, partially cemented, lt. brown	v. dens.	mod. hard
40									Bottom at 40 feet.		



FED. RD. REC. NO.	STATE	PROJECT NO.	COUNTY	SHEET NO.
9	NEVADA	EB-NH-095-2(029)	CLARK	BL-5

ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE NOTED. ALL STATIONS AND OFFSETS ARE IN METERS.

LOG OF BORING NO. 2

CLIENT: Parsons Transportation Group	BORING LOCATION: See Alignment Plan	ELEVATION (m): 713.64	PROJECT: Terrey Pines Drive Bridge	SITE: Terrey Pines and US 95	SAMPLES		TESTS						
					CONSISTENCY	GRAPHIC	USCS SYMBOL	DEPTH (m)	SAMPLE	TYPE*	MOISTURE %	DRY DENSITY kg/m³	ATTERBERG LIMITS
SOIL DESCRIPTION													
CLAYEY SAND w/trace silt, trace gravel, sl. moist, lt. green					very dense		SC	14					
white to lt. green								15					
lt. green to lt. red brown					very dense			16					
partially cemented, dry to sl. moist, lt. brown					hard			17					
SANDY GRAVEL w/lt. partially cemented, dry to sl. moist, lt. brown							GC	18					
SILTY SAND w/clay, dry to sl. moist, white to lt. brown					very dense		SM	19					
w/clayey sand lenses								19.5	971 0.23	R	13.1	1490	
partially cemented					very dense to mod. hard			20		SPT			
Continued Next Page													
THE GENERALIZATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES OR WITH THE TRANSITION MATER GRADUAL.				SAMPLE TYPE: D = Drilled, L = Liquid SPT = Standard Penetration Test C = Cone									
NOTES: Groundwater not encountered. Logged by Rick Erickson													
DATE DRILLED: 5-8-00													
PROJECT NO.: 64005007A													
PLATE: A-7													
DRIVING WEIGHT (kg): 63.5													
Terracon													

(CONTINUED)

THIS SURVEY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.



FED. RD. REG. NO.	STATE	PROJECT NO.	COUNTY	SHEET NO.
9	NEVADA	EB-NH-095-2(029)	CLARK	BL-5

ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE NOTED. ALL STATIONS AND OFFSETS ARE IN METERS.

LOG OF BORING NO. 2

CLIENT: Parsons Transportation Group	PROJECT: Terrace Pines Drive Bridge													
BORING LOCATION: See Alignment Plan	ELEVATION (m): 713.64	SITE: Terrace Pines and US 95												
SOIL DESCRIPTION		CONSISTENCY	GRAPHIC	USCS SYMBOL	DEPTH (m)	SAMPLE	BLOWS/0.3m	TYPE*	MOISTURE %	DRY DENSITY kg/m³	ATTERBERG LIMITS			
CLAYEY SAND - white silt, trace gravel, sl. moist, lt. green		very dense		SC	14			57	R	5.8	1618			
white to lt. green								53	SPT					
lt. green to lt. red brown		very dense to hard		GC	15			50/0.15	R	6.4	1682			
partially cemented, dry to sl. moist, lt. brown								50/0.10	SPT					
SANDY GRAVEL w/lt; partially cemented, dry to sl. moist, lt. brown		very dense		SM	17			97/0.23	R	13.1	1490			
w/clayey sand lenses								50/0.10	SPT					
partially cemented		very dense to mod. hard			18									
Continued Next Page														
THE BORING LOCATION LIES NEARLY ON THE APPROXIMATE BOUNDARY LINE BETWEEN SOIL AND ROCK. TYPE IS IN SITU, THE TRANSITION MAY BE GRADUAL.				SAMPLE TYPE: B = Dray, L = Liquid DPI = Standard Penetration Test C = Compaction										
NOTES: Groundwater not encountered. Logged by Rick Erickson				DATE DRILLED: 5-8-00		PAGE NUMBER: Page 4 of 7								
DRIVING WEIGHT & G: 63.5		Terracon		PROJECT NO.: 64005007A		PLATE: A-7								

(CONTINUED)

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.



FED. RD. REG. NO.	STATE	PROJECT NO.	COUNTY	SHEET NO.
9	NEVADA	EB-NH-095-2(028)	CLARK	BL-6

ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE NOTED. ALL STATIONS AND OFFSETS ARE IN METERS.

LOG OF BORING NO. 2

CLIENT: Parsons Transportation Group	PROJECT: Talley Pines Drive Bridge	
BORING LOCATION: See Alignment Plan	ELEVATION (ft): 713.64	SITE: Talley Pines and US 95
SOIL DESCRIPTION		
CONSISTENCY	GRAPHIC	USCS SYMBOL
stiff	A	ST
very stiff to mod-hard		SM
dense		SC
very dense to mod-hard		GC
DEPTH (m)	SAMPLE	BLOWS/3m
23		
		68/0.25
24		38
		SPT
26		
		50/0.08
		50/0.10
27		
		50/0.05
		50/0.09
SAMPLES	TESTS	
TYPE*	MOISTURE %	DRY DENSITY kg/m³
		ATTERBERG LIMITS

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.

Continued Next Page

LINER STABILIZATION LINE REPLICATES APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES. IN-SITU TESTS ARE SHOWN. MATTER GRADUAL.

*SAMPLE TYPE: B = Bag, L = Ring
SPT = Standard Penetration Test C = Cone

NOTES: Groundwater not encountered. Logged by Rick Erickson	DATE DRILLED: 5-8-00	PAGE NUMBER: Page 6 of 7
DRIVING WEIGHT (kN): 63.5	PROJECT NO.: 64005007A	PLATE: A-9

(CONTINUED)



FED. RD. REG. NO.	STATE	PROJECT NO.	COUNTY	SHEET NO.
9	NEVADA	EB-NH-095-2(029)	CLARK	BL-5

ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE NOTED. ALL STATIONS AND OFFSETS ARE IN METERS.

LOG OF BORING NO. 2

CLIENT: Parsons Transportation Group	BORING LOCATION: See Alignment Plan	ELEVATION (m): 713.64	PROJECT: Terrey Pines Drive Bridge	SITE: Terrey Pines and US 95	SAMPLES		TESTS			
					DEPTH (m)	SAMPLE	BLOWS/0.3m	TYPE*	MOISTURE %	DRY DENSITY kg/m³
SOIL DESCRIPTION										
CLAYEY SAND -w/trace silt, trace gravel, sl. moist, lt. green					14					
white to lt. green							57	R	5.8	1618
lt. green to lt. red brown					15		53	SPT		
partially cemented, dry to sl. moist, lt. brown					16		50/0.15	R	6.4	1682
SANDY GRAVEL -w/silt, partially cemented, dry to sl. moist, lt. brown					17		50/0.10	SPT		
SILTY SAND -w/clay, dry to sl. moist, white to lt. brown					18		97/0.23	R	13.1	1490
w/clayey sand lenses										
partially cemented										
Continued Next Page										
THE BORING LOG LINES EXPERTISE THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES. IN-SITE, THE DISTINCTION MAY BE GRADUAL.				SAMPLE TYPE: B = BAG, L = LIQUEFIED DPI = Standard Penetration Test C = CORER						
NOTES: Groundwater not encountered. Logged by Rick Erickson				DATE DRILLED:				PAGE NUMBER:		
DRIVING WEIGHT (kN): 63.5				5-8-00				Page 4 of 7		
				PROJECT NO.:				PLATE:	A-7	
				64005007A						

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.

(CONTINUED)

Terracon

LOG OF BORING NO. 2

CLIENT: Parsons Transportation Group	ELEVATION (m) 713.64	PROJECT: Torrey Pines Drive Bridge	SITE: Torrey Pines and US 95			SAMPLES	TESTS					
				SOIL DESCRIPTION	CONSISTENCY	GRAPHIC	USCS SYMBOL	DEPTH (m)	BLOWS/1.3m	TYPE *	MOISTURE %	DRY DENSITY kg/m³
THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.												
SILTY SAND -w/clay, sl. moist, lt. red brown w/sec. partially cemented lenses	very dense	SM		10	61	R	11.7	1842				
CLAYEY SAND -w/ilt, sl. moist, lt. red brown	very dense	SC		15	41	SPT						
SILTY CLAY -w/trace sand, sl. moist, lt. red brown	very stiff	CL		20								
CLAYEY SAND -w/ilt, sl. moist, lt. red brown	very dense	SC		20	58	R	7.6	1698				
SILTY SAND -w/trace clay, sl. moist, lt. red brown w/sec. partially cemented lenses	dense	SM		21	35	SPT						
CLAYEY SAND -partially cemented, sl. moist, lt. red brown	very dense to mod-hard	SC		22	50f 0.14 50f 0.13	R SPT	3.8	1634				
SANDY GRAVEL -w/clay, sl. moist, lt. brown	very dense	GC										
Continued Next Page				SAMPLE TYPE: B = B-4 L = L-4 SPT = Standard Penetration Test C = Com								
THE HATCHED LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES IN SITE. THE TRANSITION MAY BE GRADUAL.				DATE DRILLED: 5-8-00								
NOTES: Groundwater not encountered. Logged by Rick Erickson				PAGE NUMBER: Page 5 of 7								
DRIVING WEIGHT (kN) 63.5	Terracon			PROJECT NO.: 64005007A								
				PLATE A-8								

LOG OF BORING NO.

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.

LOG OF BORING NO. 2										
CLIENT: Parsons Transportation Group		PROJECT: Torrey Pines Drive Bridge								
BORING LOCATION: See Alignment Plan	ELEVATION (ft) 713.64	SITE: Torrey Pines and US 95								
SOIL DESCRIPTION		SAMPLES								
		CONSISTENCY	GRAPHIC	USCS SYMBOL	DEPTH (in)	SAMPLE	BLOWS/0.3m	TYPE*	MOISTURE %	
FILL SANDY GRAVEL -w/lt, trace cobbles, dry, lt brown		sl. moist	FILL		1	20	R	2.8	5.3	1602
-sl. moist					2	9	SPT			
SANDY GRAVEL -w/lt, trace cobbles, partially cemented, dry to sl. moist, lt brown		very dense to mod. hard	GM		3	50/0.10	R			
-sl. moist, white to lt brown					4	50/0.05	SPT			
SILTY SAND -sl. moist, lt brown		very dense	SM		45	R	4.1	1810		
SANDY GRAVEL -w/lt, occ. cobbles, sl. moist, white to lt brown			GM		47	SPT				
Continued Next Page										
THE GENERAL LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES; IN FACT, THE TRANSITION MAY BE GRADUAL.					SAMPLE TYPES: B = B-rod, R = R-rod SPT = Standard Penetration Test C = Cone					
NOTES: Groundwater not encountered. Logged by Rick Erickson		Terracon			DATE DRILLED: 5-8-00		PAGE NUMBER: Page 1 of 7			
DRIVING WEIGHT (kN) 635		PROJECT NO.: 64005007A			PLATE: A-4					

LOG OF BORING

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.

LOG OF BORING NO. 2									
CLIENT:		PROJECT:							
Parsons Transportation Group		Torrey Pines Drive Bridge							
BORING LOCATION:	ELEVATION (ft)	SITE:				Torrey Pines and US 95			
See Alignment Plan	713.64	Torrey Pines and US 95				SAMPLES			
SOIL DESCRIPTION					TESTS		TESTS		
					BLOWS/0.3m		TYPE *	MOISTURE %	DRY DENSITY kg/m³
					SAMPLE	DEPTH (m)			ATTERBERG LIMITS
FILL-SANDY GRAVEL -w/lt, trace cobbles, dry, lt brown					FILL			5.3	
-sl. moist						1	20	R	2.8
						9		SPT	
						2			
SANDY GRAVEL -w/lt, trace cobbles, partially rounded, dry to sl. moist, lt brown					GM	SD/0.10 SD/0.05	R	SPT	
-sl. moist, white to lt brown						3			
SILTY SAND -sl. moist, lt brown					SM				
SANDY GRAVEL -w/lt, occ. cobbles, sl. moist, white to lt brown					GM				
						4	45	R	4.1
						47		SPT	1810
Continued Next Page									
THE INTERSECTION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES IN-SITE. THE TRANSITION MAY BE GRADUAL.					SAMPLE TYPES: B = Bore, R = Ram SPT = Standard Penetration Test C = Core				
NOTES: Groundwater not encountered. Logged by Rick Erickson		DATE DRILLED: 5-8-00				PAGE NUMBER: Page 1 of 7			
DRIVING WEIGHT (kN) 63.5		PROJECT NO.: 64005007A				PLATE: A-4			

LOG OF BORING

THIS FORMULARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.



FED. RD. REC. NO.	STATE	PROJECT NO.	COUNTY	SHEET NO.
9	NEVADA	EB-NH-095-2(029)	CLARK	BL-4

ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE NOTED. ALL STATIONS AND OFFSETS ARE IN METERS.

LOG OF BORING NO. 2

CLIENT: Parsons Transportation Group	BORING LOCATION: See Alignment Plan	ELEVATION (m) 713.64	PROJECT: Terry Pines Drive Bridge	SITE: Terry Pines and US 95	SAMPLES		TESTS						
					CONSISTENCY	GRAPHIC	USCS SYMBOL	DEPTH (m)	BLOWS/0.3m	TYPE *	MOISTURE %	DRY DENSITY kg/m³	ATTERBERG LIMITS
SOIL DESCRIPTION													
SANDY GRAVEL -w/lt, trace cobbles, sl. moist, white to lt. brown			very dense	GM									
GRAVELLY SAND -w/lt, sl. moist, white to lt. brown			dense to very dense	SM				5	51	R	3.3	1906	
SILTY SAND -very fine, sl. moist, lt. green			very dense	SM				6	49	SPT			
SANDY GRAVEL -w/lt, sl. moist, white to lt. brown			dense	GM				6					
CLAYEY SILT -w/trace gravel, sl. moist, white			stiff	ML				7	23	R	8.0	1442	
SILTY SAND -sl. moist, lt. green			med. dense	SM				7	14	SPT	7.9		
SILTY CLAY -sl. moist, green to lt. green			stiff	CL				8					
SANDY GRAVEL -w/clay, trace silt, sl. moist, lt. green			very dense	GC				8	59	R	4.6	1810	
GRAVELLY SAND -w/clay, sl. moist, lt. green				SC				9	51	SPT			
Continued Next Page													
THE CLASSIFICATION LINE REPRESENTS APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK. IN SITU, THE TRANSITION MAY BE GRADUAL.					SAMPLE TYPE: D = Dry, L = Liquid SPT = Standard Penetration Test C = Com								
NOTES: Groundwater not encountered. Logged by Rick Erickson					DATE DRILLED:					PAGE NUMBER:			
					5-8-00					Page 2 of 7			
DRIVING WEIGHT (kg): 63.5					PROJECT NO.:	64005007A				PLATE:	A-5		



FED. RD. REC. NO.	STATE	PROJECT NO.	COUNTY	SHEET NO.
9	NEVADA	EB-NH-095-2(029)	CLARK	BL-4

ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE NOTED. ALL STATIONS AND OFFSETS ARE IN METERS.

LOG OF BORING NO. 2

CLIENT: Parsons Transportation Group	BORING LOCATION: See Alignment Plan	ELEVATION (m): 713.64	PROJECT:		TESTS			
			SITE: Torrey Pines Drive Bridge		Torrey Pines and US 95			
SOIL DESCRIPTION								
			CONSISTENCY	GRAPHIC	USCS SYMBOL	DEPTH (m)	SAMPLES	
SANDY GRAVEL -w/ silt, trace cobbles, sl. moist, white to lt. brown	very dense			GM			BLOWS/0.3m	
GRAVELLY SAND -w/ silt, sl. moist, white to lt. brown	dense to very dense			SM				
SILTY SAND -very fine, sl. moist, lt. green	very dense							
SANDY GRAVEL -w/ silt, sl. moist, white to lt. brown	dense			GM				
CLAYEY SILT -trace gravel, sl. moist, white	stiff			ML				
SILTY SAND -sl. moist, lt. green	med. dense			SM				
SILTY CLAY -sl. moist, green to lt. green	stiff			CL				
SANDY GRAVEL -w/ clay, trace silt, sl. moist, lt. green	very dense			GC				
GRAVELLY SAND -w/ clay, sl. moist, lt. green				SC				
Continued Next Page								
THE FOLLOWING LOGS REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK. REFOR IN-SITU, THE BOUNDARY MAY BE GRADUAL.			SAMPLE TYPES: D = Dry, L = Liquid SPT = Standard Penetration Test C = Cone					
NOTES: Groundwater not encountered. Logged by Rick Erickson	Terracon		DATE DRILLED: 5-8-00		PAGE NUMBER: Page 2 of 7			
DRIVING WEIGHT (kg): 635	PROJECT NO.: 64005007A		PLATE: A-5					

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.

1/4/01

EXPO

PROJ

NO. 2

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.



FED. RD. REG. NO.	STATE	PROJECT NO.	COUNTY	SHEET NO.
9	NEVADA	EB-NH-095-2(029)	CLARK	BL-4

ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE NOTED. ALL STATIONS AND OFFSETS ARE IN METERS.

LOG OF BORING NO. 2

CLIENT: Parsons Transportation Group	BORING LOCATION: See Alignment Plan	ELEVATION (m): 713.64	PROJECT: Torrey Pines Drive Bridge	SITE: Torrey Pines and US 95		SAMPLES		TESTS			
				SOIL DESCRIPTION	CONSISTENCY	GRAPHIC	USCS SYMBOL	DEPTH (m)	SAMPLE	BLOWS/0.3m	TYPE*
SANDY GRAVEL -w/ilt, trace cobbles, sl. moist, white to lt brown				very dense			GM				
GRAVELLY SAND -w/ilt, sl. moist, white to lt brown				dense to very dense			SM	5	SI	R	3.3
SILTY SAND -very fine, sl. moist, lt green				very dense				6	49	SPT	
SANDY GRAVEL -w/ilt, sl. moist, white to lt brown				dense			GM	6			
CLAYEY SILT -w/trace gravel, sl. moist, white				stiff			ML	7	23	R	8.0
SILTY SAND -sl. moist, lt green				med. dense			SM	7	14	SPT	7.9
SILTY CLAY -sl. moist, green to lt green				stiff			CL	8	59	R	4.6
SANDY GRAVEL -w/clay, trace silt, sl. moist, lt green				very dense			GC	8			1810
GRAVELLY SAND -w/clay, sl. moist, lt green							SC	9	51	SPT	
Continued Next Page											
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES IN-HOLE, THE TRANSITION MAY BE GRADUAL				SAMPLE TYPES: D = Drilled, L = Liquefied SPT = Standard Penetration Test, C = Cone							
NOTES: Groundwater not encountered. Logged by Rick Erickson				DATE DRILLED:		PAGE NUMBER:					
DRIVING WEIGHT (kN): 63.5	Terracon			5-8-00		Page 2 of 7					
				PROJECT NO.: 64005007A		PLATE:		A-5			

THIS SUMMARY APPLIES ONLY AT THIS LOCATION AT THE TIME OF LOGGING. CONDITIONS MAY DIFFER WITH TIME OR AT OTHER LOCATIONS.

CLIENT:		PROJECT:	
Parsons Transportation Group		Torrey Pines Drive Bridge	
BORING LOCATION:	ELEVATION (m):	SITE	
See Alignment Plan		Torrey Pines and US 95	
SOIL DESCRIPTION		SAMPLES	TESTS
GRAVELLY SAND -sl. moist, lt. green		DEPTH (m)	ATTERBERG LIMITS
SILTY SAND -sl. moist, lt. green		very dense	DRY DENSITY kg/m ³
SANDY CLAY - sl. moist, lt. green		dense	TYPE*
CLAYEY SAND -sl. moist, partially cemented lenses, sl. moist, lt. green		very stiff	MOISTURE %
SILTY SAND -sl. moist, lt. green		dense	BLOWS/0.3m
CLAYEY SAND -sl. moist, lt. gray		very stiff	SPT
SANDY CLAY -white, sl. moist, white to lt. green w/trace clayey sand lenses		very stiff	8.3
w/trace gravel			1554
Continued Next Page		11	1522
SEE FRAGMENTATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES. IN-SITU, THE EXAMINER MAY BE GRADUAL.		12	1249
NOTES: Groundwater not encountered. Logged by Rick Erickson		13	0.15
DRIVING WEIGHT (kN) 63.5		0.9	5-8-00
			PAGE NUMBER: Page 3 of 7
			PROJECT NO.: 64005007A
			PLATE: A-6

LOG OF BORING NO.

Terracon

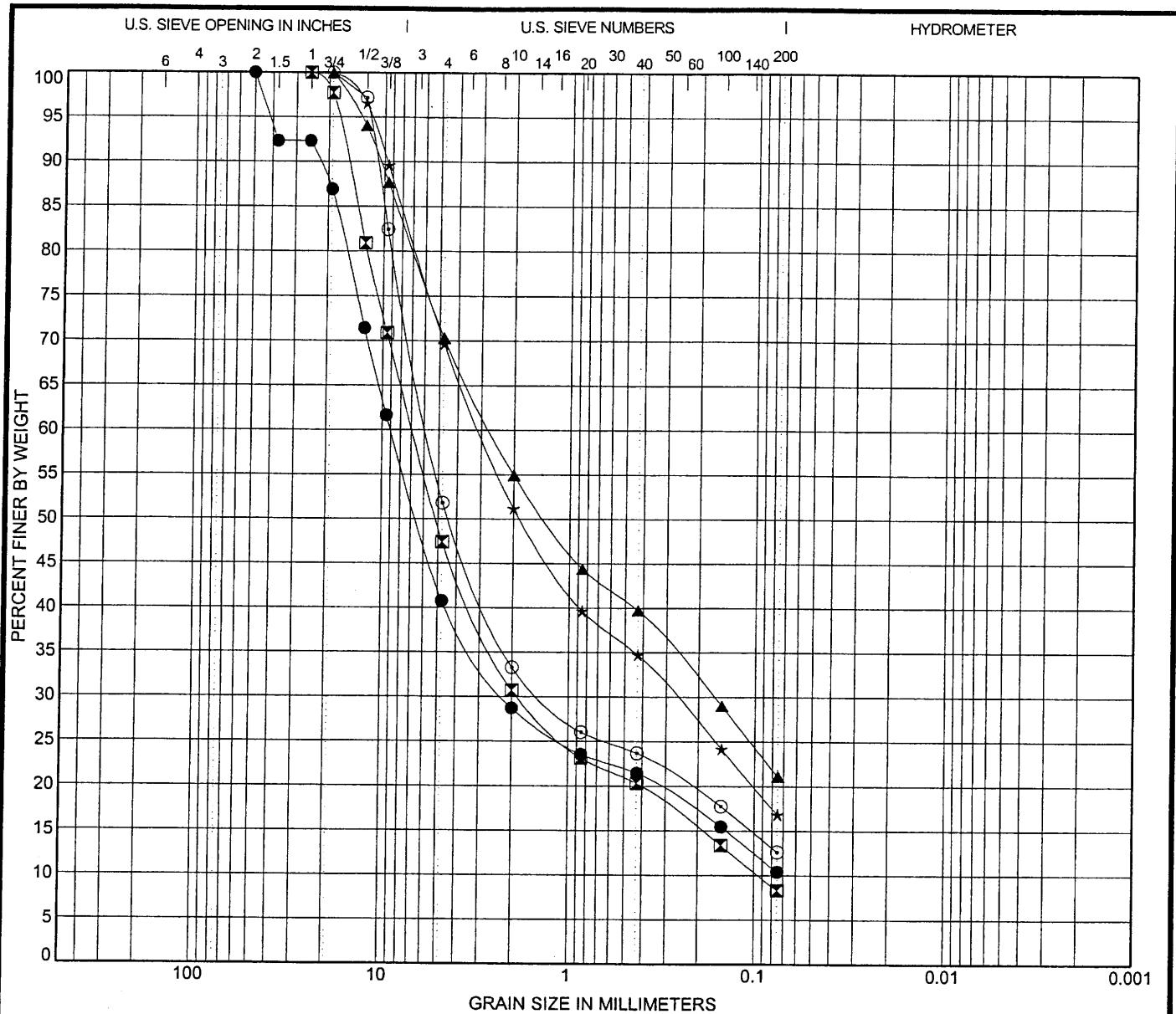
LOG OF BORING NO. 2

CLIENT:		PROJECT:	
Parsons Transportation Group		Torrey Pines Drive Bridge	
BORING LOCATION: See Alignment Plan	ELEVATION (m): 713.64	SITE	
		Torrey Pines and US 95	
SOIL DESCRIPTION		SAMPLES	TESTS
CONSISTENCY	GRAPHIC	DEPTH (m)	
USCS SYMBOL		SAMPLE	BLOWS/0.3m
			TYPE *
			MOISTURE %
			DRY DENSITY kg/m³
			ATTERBERG LIMITS
SANDY GRAVEL - very dry to s. moist, white to h. brown		very dense to mod. hard	SC
CALICHE (Cemented SAND & GRAVEL) - very hard, dry, lt. brown w/partially cemented lenses		mod. hard	SC
Bottom at 36.42 surface			
THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY LINES BETWEEN SOIL AND ROCK TYPES IN-SITU, THE TRANITION MAY BE GRADUAL.		SAMPLE TYPES: B = BAG, L = LIQUEFACTION, R = RIGID, SPT = Standard Penetration Test, C = CORE	
NOTES: Groundwater not encountered. Logged by Rick Erickson		DATE DRILLED: 5-8-00	PAGE NUMBER: Page 7 of 7
DRIVING WEIGHT (kN): 63.5	Terracon	PROJECT NO.: 64005007A	PLATE: A-10

LOG OF BORING NO.

APPENDIX II

TEST RESULTS



COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification						LL	PL	PI	Cc	Cu
● B-01 1.9	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						28	16	12	7.56	127.23
☒ B-01 6.5	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)						21	15	6	5.24	73.19
▲ B-01 7.7	CLAYEY SAND with GRAVEL (SC)						31	19	12		
★ B-01 9.9	CLAYEY SAND with GRAVEL (SC)						29	18	11		
○ B-01 12.6	SILTY, CLAYEY GRAVEL with SAND (GC-GM)						21	14	7		

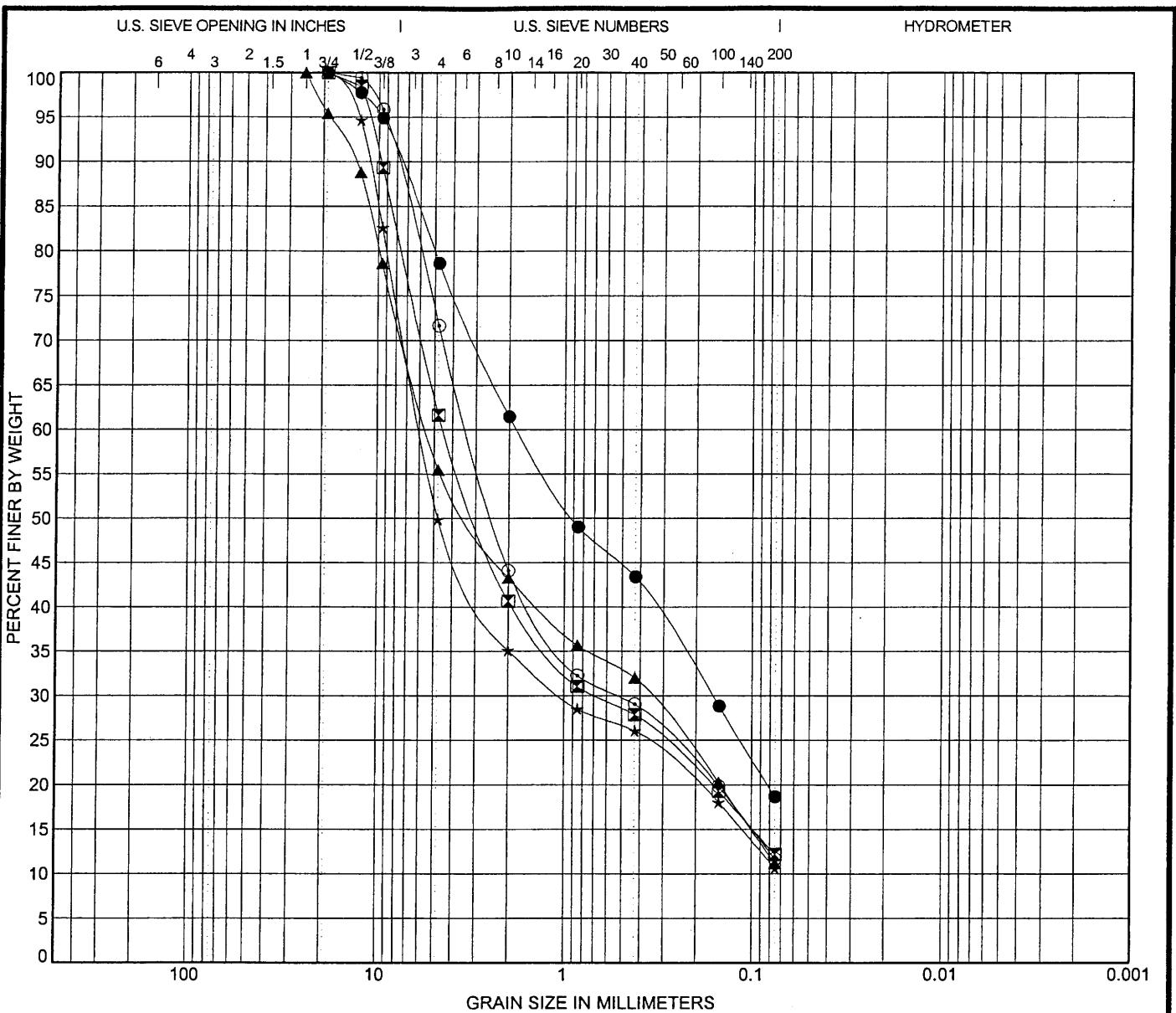
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-01 1.9	50	8.988	2.191		2.3	59.2	30.3		10.4
☒ B-01 6.5	25	6.894	1.844	0.094	1.4	52.6	39.0		8.3
▲ B-01 7.7	19	2.66	0.165		4.2	29.7	49.2		21.1
★ B-01 9.9	19	3.022	0.266		2.6	30.3	52.8		16.8
○ B-01 12.6	19	5.716	1.357		2.0	48.2	39.2		12.6



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Telephone: (775) 359-6600
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-1 Plate Number: 4a



COBBLES	GRAVEL			SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine					

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

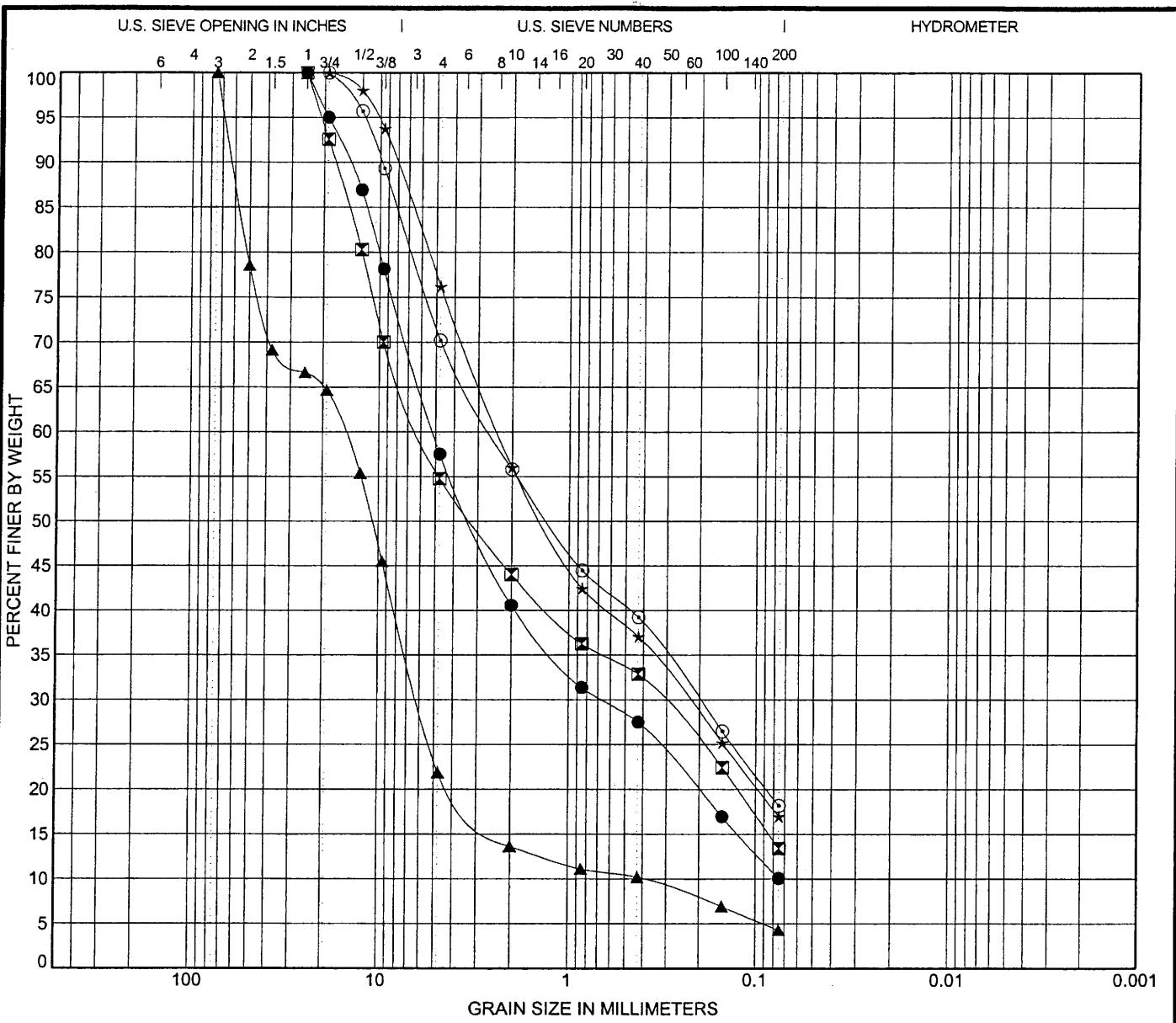


Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-01 16.0									
	CLAYEY SAND with GRAVEL (SC)						26	17	9
☒ B-01 18.7									
	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						19	15	4
▲ B-01 21.7									
	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						18	15	3
★ B-01 24.8									
	WELL-GRADED GRAVEL with SILTY CLAY and SAND (GW-GC)						18	14	4
○ B-01 29.3									
	WELL-GRADED SAND with SILT and GRAVEL (SW-SM)						NV	NV	NP
	1.27	50.70							

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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-1 Plate Number: 4b



COBBLES	GRAVEL			SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine					

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

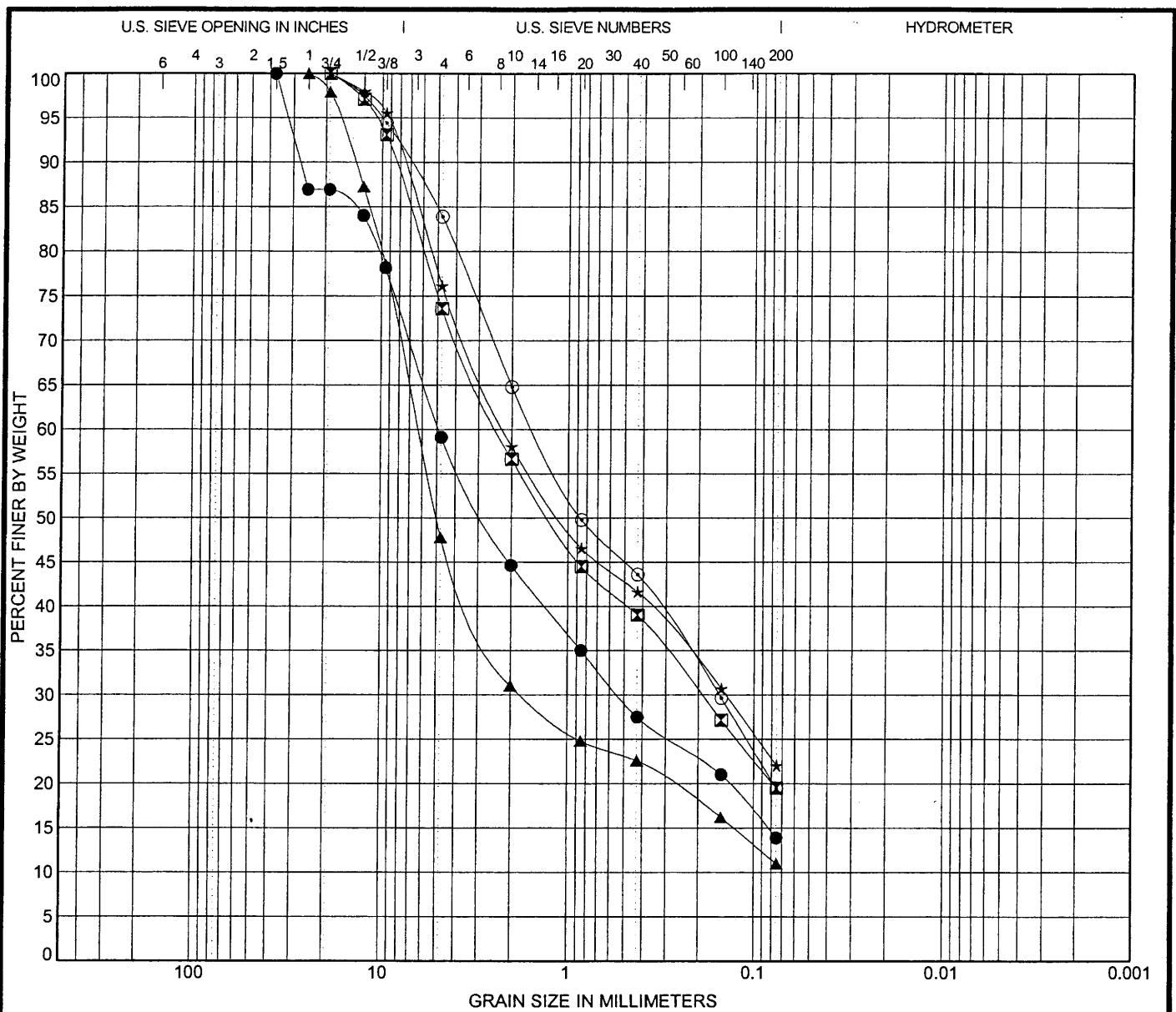
Specimen Identification		Classification						LL	PL	PI	Cc	Cu
●	B-02 1.9	WELL-GRADED SAND with SILT and GRAVEL (SW-SM)						20	17	3	1.15	69.43
☒	B-02 3.4	CLAYEY GRAVEL with SAND (GC)						28	17	11		
▲	B-02 5.0	POORLY GRADED GRAVEL with SAND (GP)						26	17	9	5.99	39.01
★	B-02 6.5	CLAYEY SAND with GRAVEL (SC)						30	18	12		
○	B-02 7.7	CLAYEY SAND with GRAVEL (SC)						48	24	24		
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-02 1.9	25	5.16	0.665		1.3	42.5	47.4			10.1	
☒	B-02 3.4	25	6.02	0.319		2.5	45.2	41.4			13.4	
▲	B-02 5.0	75	15.389	6.033	0.394	0.7	78.2	17.5			4.3	
★	B-02 6.5	19	2.37	0.229		2.8	23.8	59.2			17.0	
○	B-02 7.7	19	2.571	0.2		4.4	29.8	52.0			18.2	



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-1 Plate Number: 4c



COBBLES	GRAVEL			SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine					
● B-02 11.0						CLAYEY SAND with GRAVEL (SC)	32	18	14	

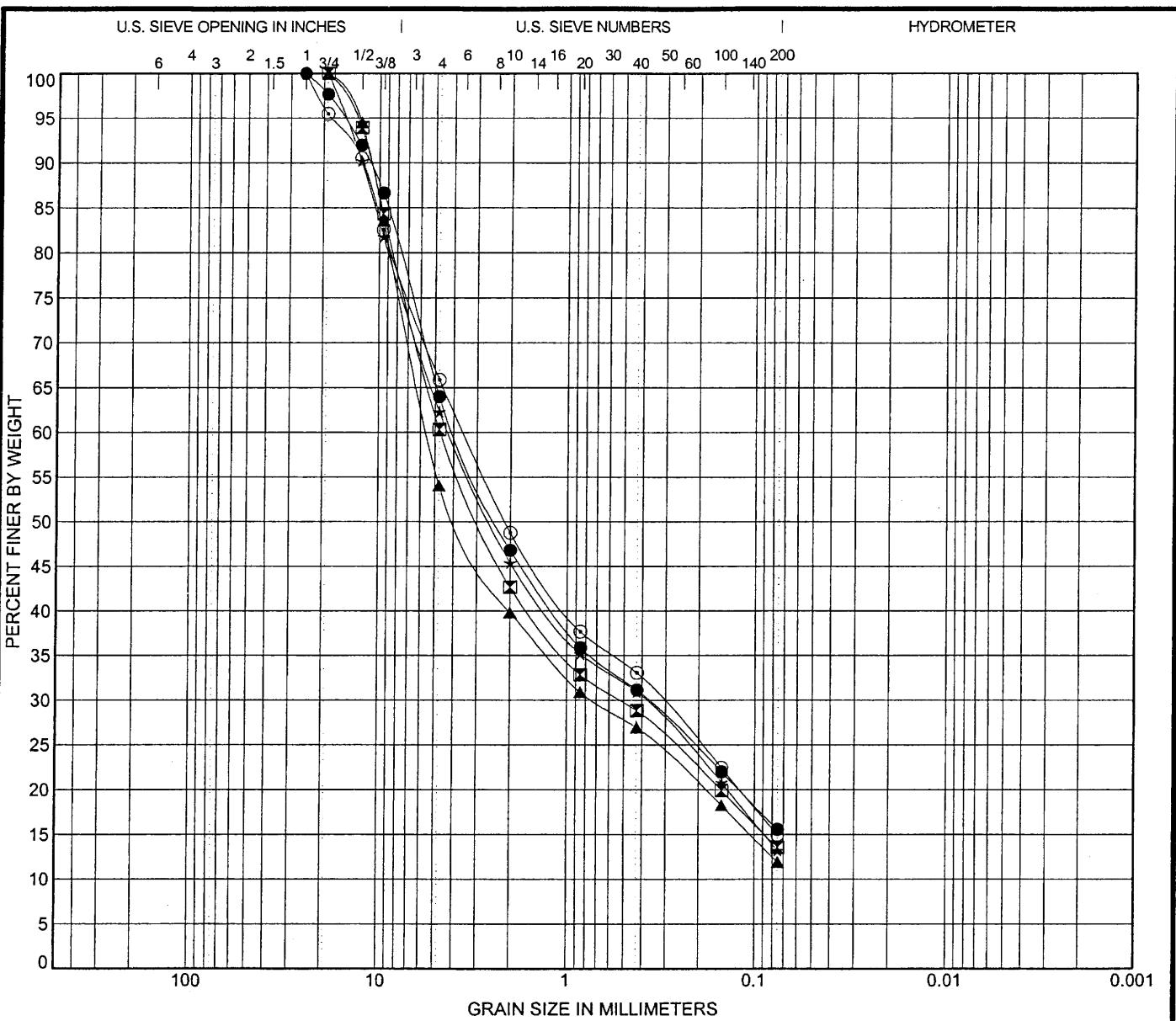
Note: NV - No Value, NP - Non Plastic, sample depth in meters.



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-1 Plate Number: 4d

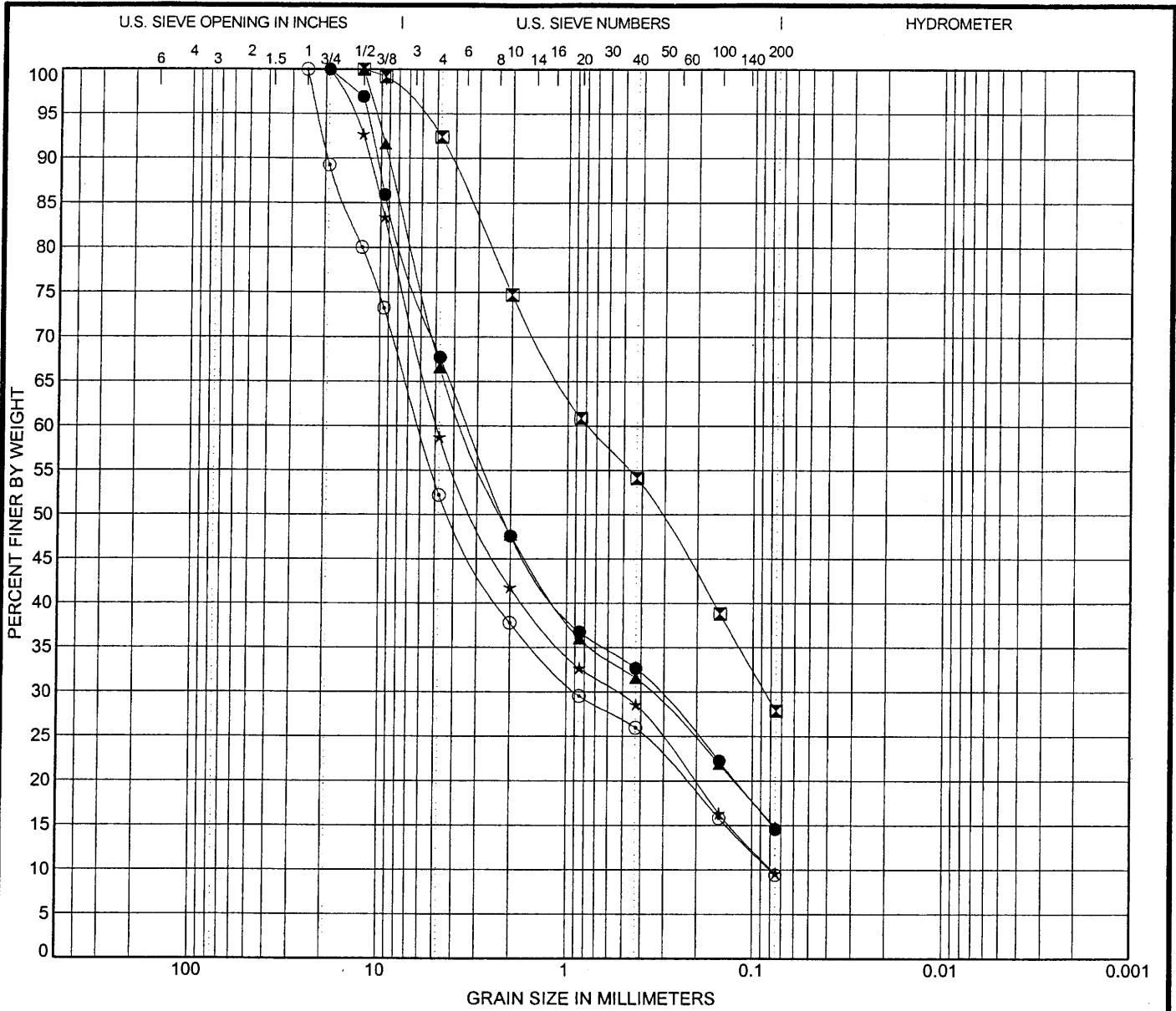


COBBLES	GRAVEL			SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine					

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification						LL	PL	PI	Cc	Cu
●	B-03	1.9	SILTY, CLAYEY SAND with GRAVEL (SC-SM)					19	14	5		
☒	B-03	3.4	SILTY, CLAYEY SAND with GRAVEL (SC-SM)					19	15	4		
▲	B-03	5.0	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)					17	15	2	1.59	90.02
★	B-03	6.5	SILTY SAND with GRAVEL (SM)					17	14	3		
○	B-03	9.5	SILTY, CLAYEY SAND with GRAVEL (SC-SM)					19	14	5		
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-03	1.9	25	3.882	0.373		0.9	36.0	48.4		15.6	
☒	B-03	3.4	19	4.678	0.521		0.9	39.7	46.8		13.6	
▲	B-03	5.0	19	5.462	0.727		0.7	46.0	42.1		11.9	
★	B-03	6.5	19	4.221	0.385		1.8	37.7	49.1		13.2	
○	B-03	9.5	25	3.529	0.315		1.5	34.1	50.9		15.0	





COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

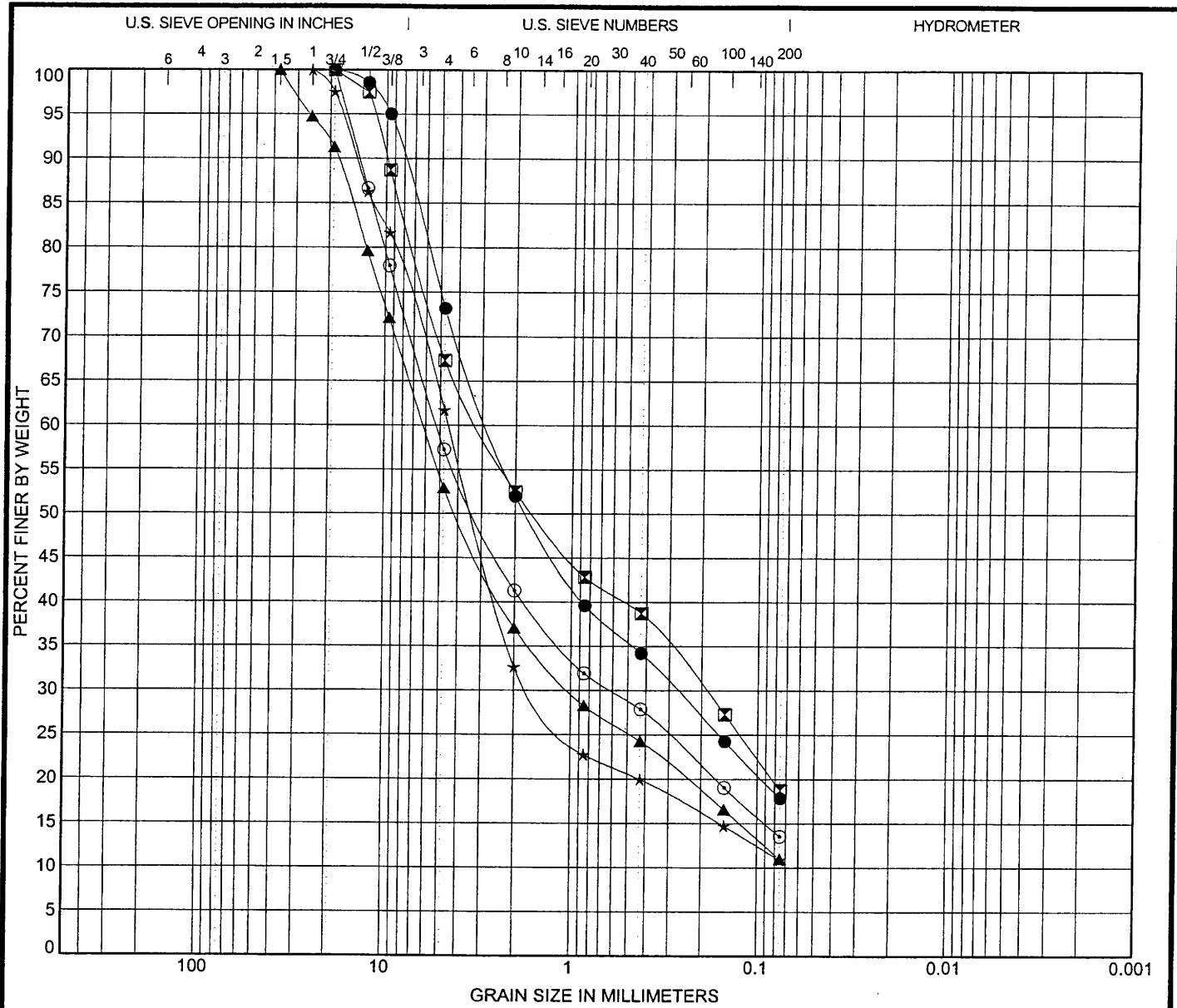
Specimen Identification		Classification						LL	PL	PI	Cc	Cu
●	B-03 12.6	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						19	15	4		
◻	B-03 14.1	CLAYEY SAND (SC)						26	16	10		
▲	B-03 15.6	SILTY SAND with GRAVEL (SM)						15	14	1		
★	B-04 1.9	POORLY GRADED SAND with SILT and GRAVEL (SP-SM)						18	16	2	0.76	63.28
○	B-04 3.4	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						18	15	3	1.63	77.14
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-03 12.6	19	3.408	0.325			1.4	32.3	53.2		14.6	
◻	B-03 14.1	12.5	0.777	0.086			3.8	7.6	64.5		27.9	
▲	B-03 15.6	12.5	3.514	0.359			2.0	33.4	51.7		14.8	
★	B-04 1.9	19	4.919	0.54	0.078	0.7	41.2	49.1			9.7	
○	B-04 3.4	25	6.139	0.892	0.08	0.8	47.8	42.8			9.5	

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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-1 Plate Number: 4f





COBBLES	GRAVEL		SAND			SILT OR CLAY				
	coarse	fine	coarse	medium	fine					
● B-04	7.7		CLAYEY SAND with GRAVEL (SC)			32	20	12		
☒ B-04	10.7		CLAYEY SAND with GRAVEL (SC)			30	19	11		
▲ B-07	1.1	1.1	WELL-GRADED GRAVEL with SILTY CLAY and SAND (GW-GC)			21	16	5	2.50	92.84
★ B-07	2.6	2.6	POORLY GRADED SAND with SILTY CLAY and GRAVEL (SP-SC)			21	16	5	8.85	71.06
○ B-07	4.1		SILTY, CLAYEY SAND with GRAVEL (SC-SM)			20	15	5		

Note: NV - No Value, NP - Non Plastic, sample depth in meters.



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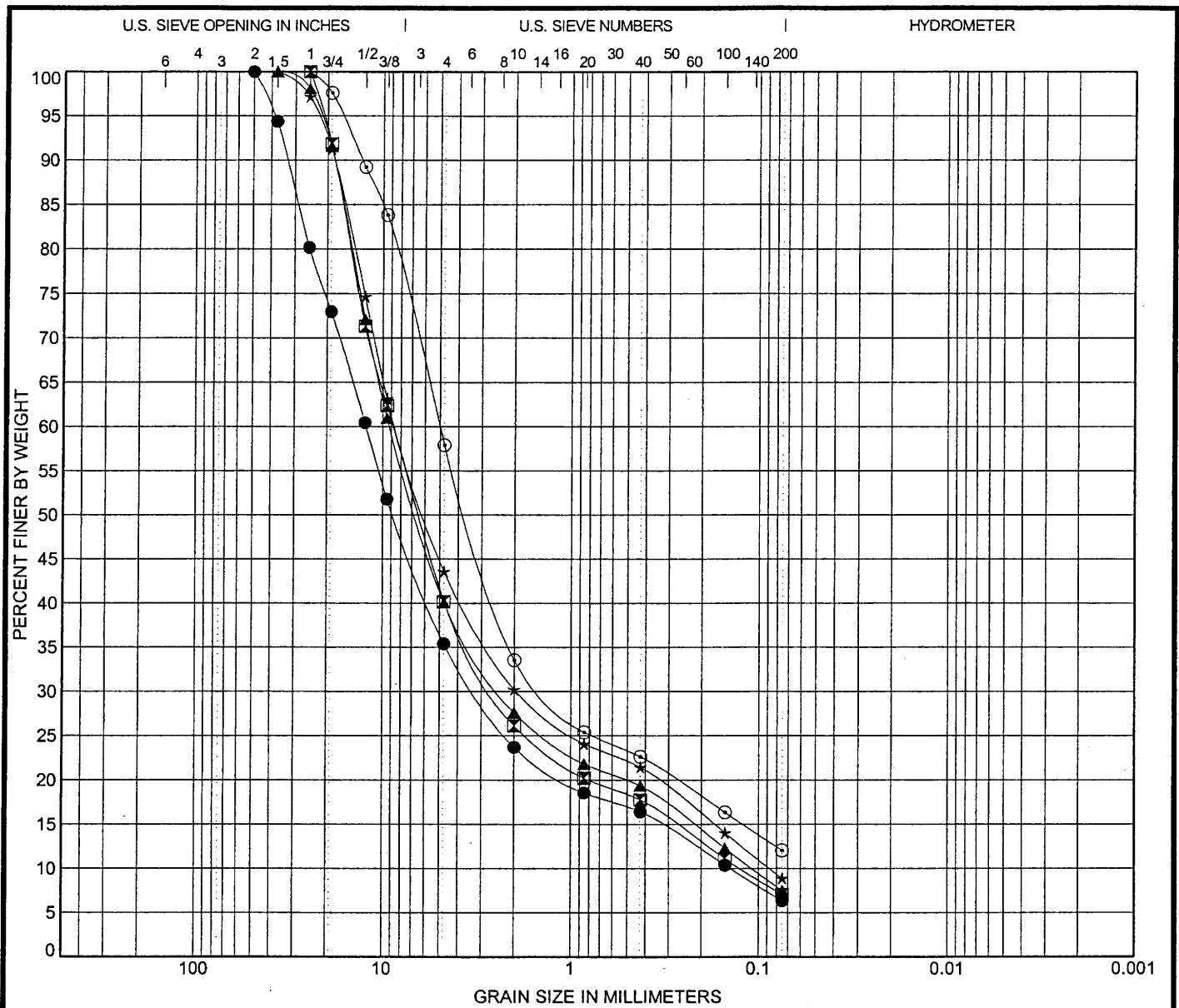
GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

Project Number: 0324-01-1

Plate Number: 4g



COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				
● B-05 1.1	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)					18	17	1	5.89 87.91

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification						LL	PL	PI	Cc	Cu
● B-05 1.1	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						18	17	1	5.89	87.91
☒ B-05 2.6	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						20	17	3	5.91	71.17
▲ B-05 4.1	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						20	17	3	5.64	85.58
★ B-05 5.6	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						18	17	1	5.10	97.55
○ B-05 11.7	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						22	17	5	7.04	93.24
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
● B-05 1.1	50	12.326	3.19	0.14	1.0	64.6	29.0			6.4	
☒ B-05 2.6	25	8.816	2.541	0.124	1.0	59.8	33.1			7.1	
▲ B-05 4.1	37.5	9.208	2.364	0.108	1.3	60.0	32.5			7.5	
★ B-05 5.6	37.5	8.492	1.941	0.087	1.4	56.4	34.7			8.9	
○ B-05 11.7	25	5.025	1.381			2.4	42.1	45.9		12.0	



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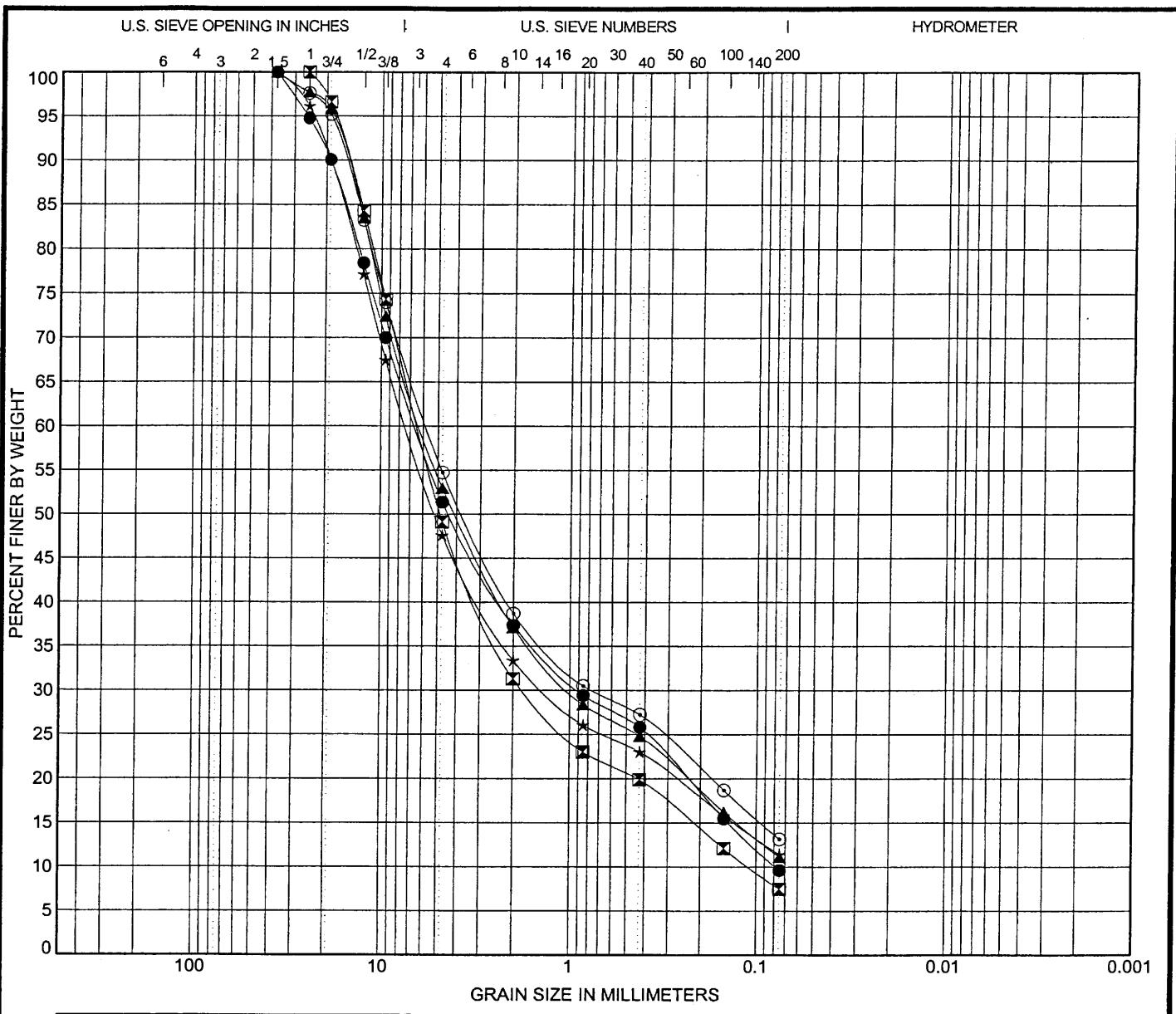
GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

Project Number: Plate Number:

4a



COBBLES	GRAVEL			SAND			SILT OR CLAY				
	coarse	fine	coarse	medium	fine						

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification						LL	PL	PI	Cc	Cu
●	B-06 1.1	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						NV	NV	NP	1.59	83.56
☒	B-06 2.6	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						NV	NV	NP	4.38	58.57
▲	B-06 4.1	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						19	16	3	2.54	95.24
★	B-06 5.6	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)						23	17	6	4.14	122.32
○	B-06 11.7	SILTY GRAVEL with SAND (GM)						17	17	NP		



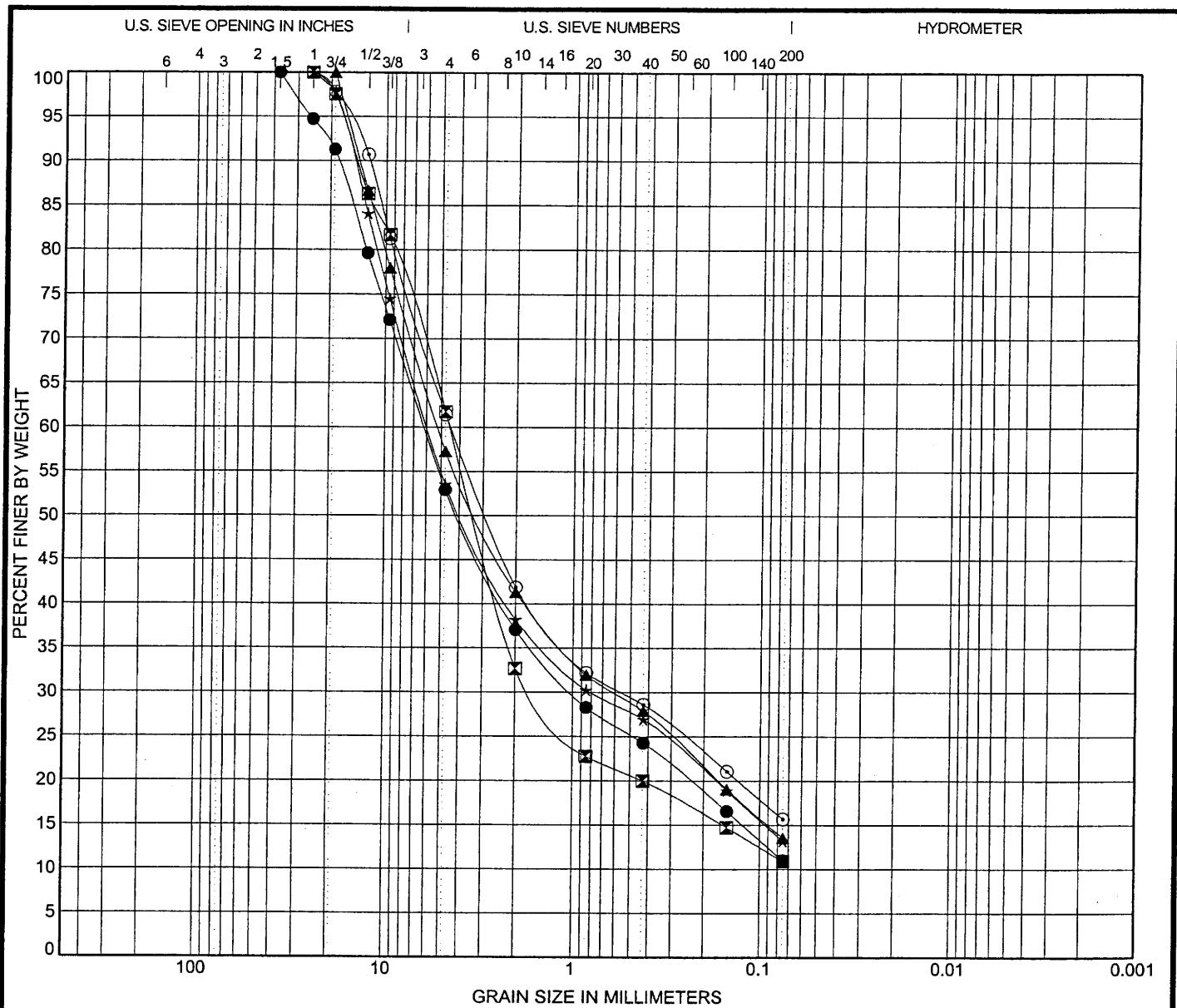
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

Project Number: Plate Number:



COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification						LL	PL	PI	Cc	Cu
● B-07	1.1	WELL-GRADED GRAVEL with SILTY CLAY and SAND (GW-GC)	21	16	5	2.50	92.84				
☒ B-07	2.6	POORLY GRADED SAND with SILTY CLAY and GRAVEL (SP-SC)	21	16	5	8.85	71.06				
▲ B-07	4.1	SILTY, CLAYEY SAND with GRAVEL (SC-SM)	20	15	5						
★ B-07	5.6	SILTY, CLAYEY GRAVEL with SAND (GC-GM)	24	17	7						
○ B-07	11.7	SILTY SAND with GRAVEL (SM)	19	16	3						
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
● B-07	1.1	37.5	6.133	1.006		1.4	47.1	41.9		11.0	
☒ B-07	2.6	25	4.511	1.592		1.4	38.3	50.8		10.9	
▲ B-07	4.1	19	5.207	0.61		1.9	42.7	43.7		13.5	
★ B-07	5.6	25	5.88	0.807		2.3	46.5	40.3		13.2	
○ B-07	11.7	25	4.457	0.558		2.6	38.6	45.8		15.7	



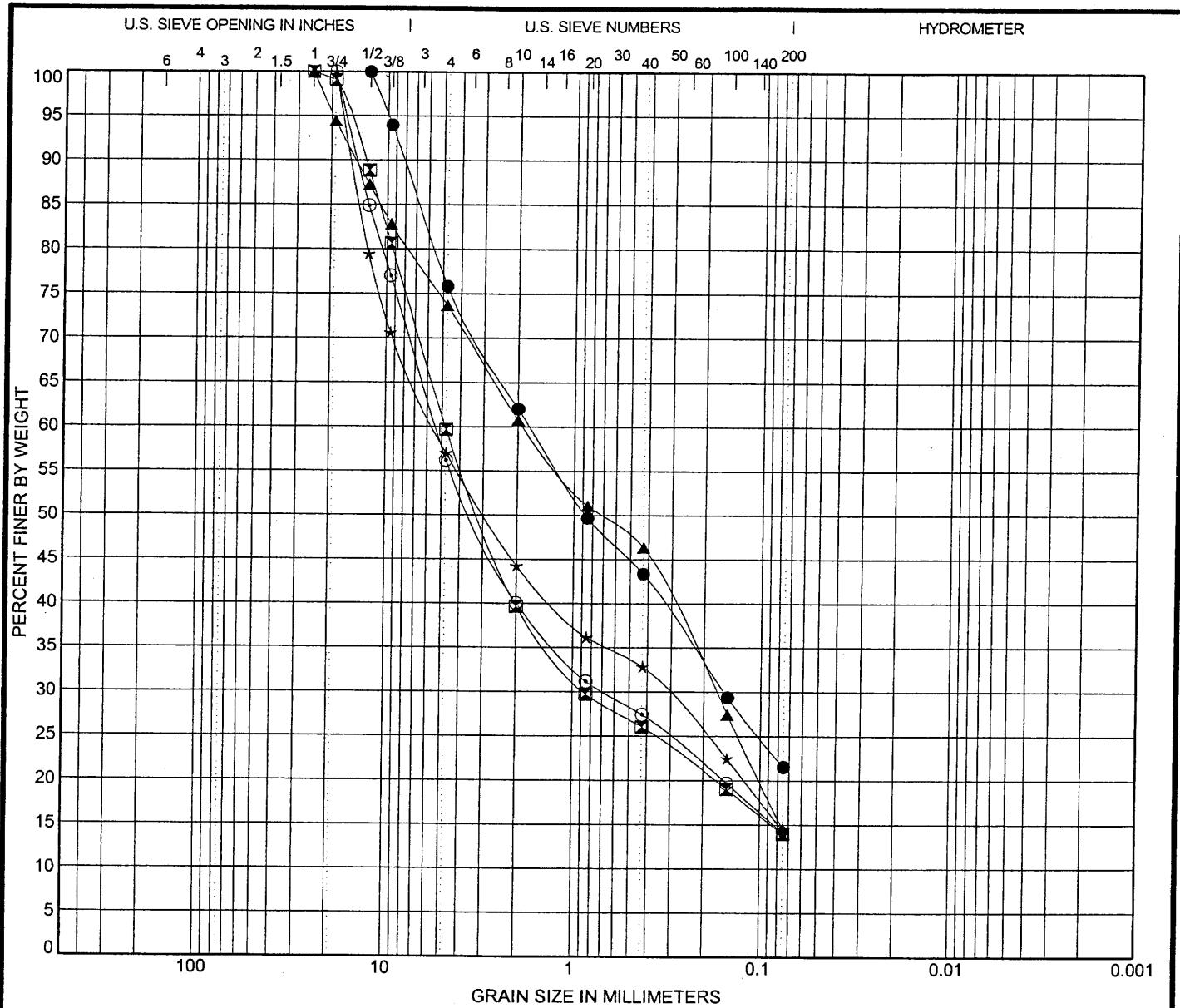
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

Project Number: Plate Number:



COBBLES	GRAVEL			SAND			SILT OR CLAY				
	coarse	fine	coarse	medium	fine						

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification						LL	PL	PI	Cc	Cu
● B-07	14.8	CLAYEY SAND with GRAVEL (SC)						45	26	19		
☒ B-07	15.4	CLAYEY SAND with GRAVEL (SC)						23	15	8		
▲ B-07	23.9	SILTY SAND with GRAVEL (SM)						NV	NV	NP		
★ B-08	1.1	SILTY, CLAYEY GRAVEL with SAND (GC-GM)						20	16	4		
○ B-08	4.1	CLAYEY GRAVEL with SAND (GC)						27	17	10		



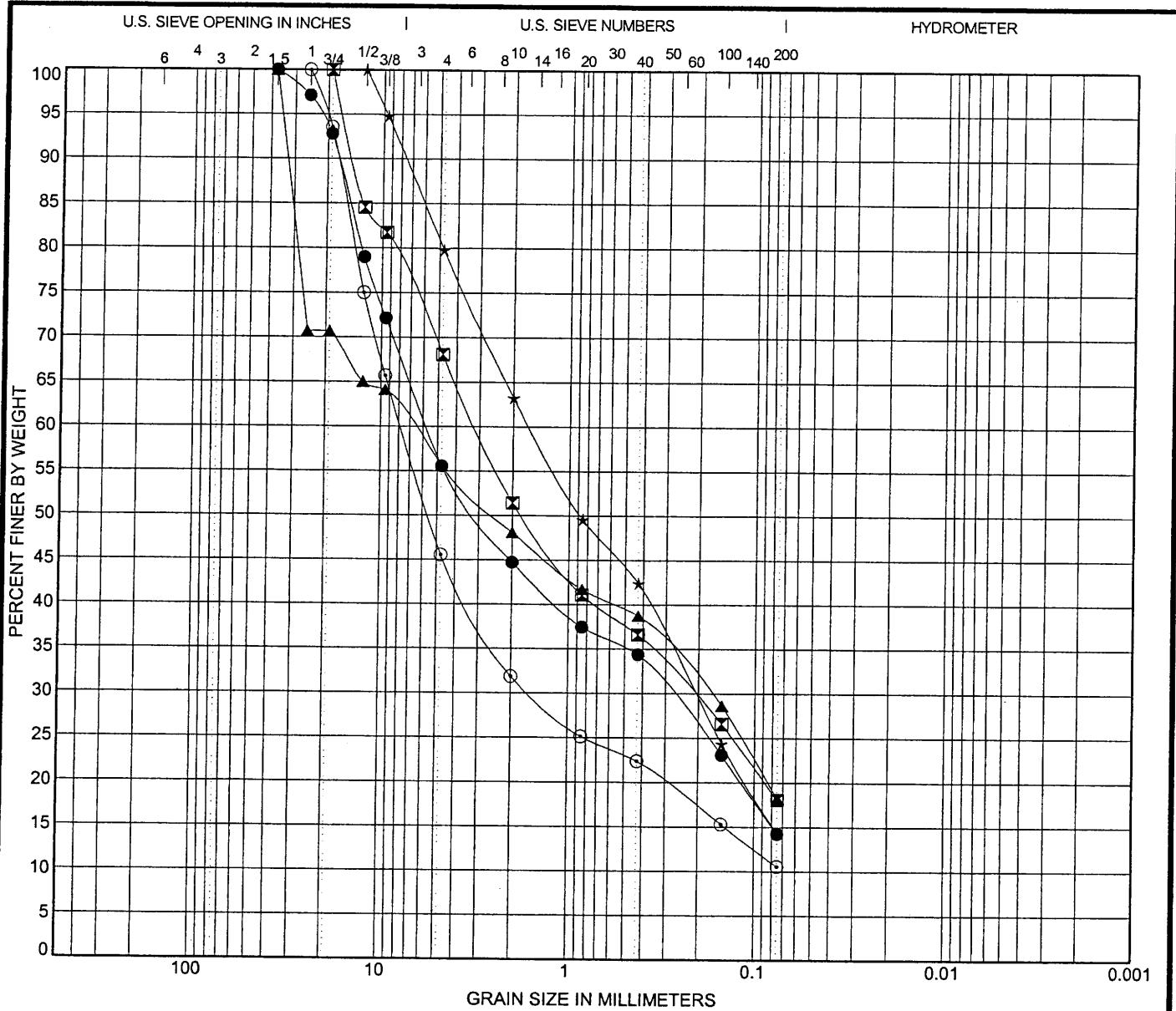
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

Project Number: Plate Number:



COBBLES	GRAVEL		SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification						LL	PL	PI	Cc	Cu
●	B-08 5.6	SILTY GRAVEL with SAND (GM)						15	13	2		
☒	B-08 7.2	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						20	15	5		
▲	B-08 8.7	SILTY, CLAYEY GRAVEL with SAND (GC-GM)						19	14	5		
★	B-08 20.9	CLAYEY SAND with GRAVEL (SC)						26	18	8		
○	B-09 1.1	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC) 26						19	7	4.63	113.32	

Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-08 5.6	37.5	5.719	0.284			4.7	44.4	41.3	14.2
☒	B-08 7.2	19	3.123	0.214			3.0	31.9	50.0	18.0
▲	B-08 8.7	37.5	6.793	0.173			4.6	44.4	37.4	18.2
★	B-08 20.9	12.5	1.631	0.208			1.5	20.2	65.4	14.3
○	B-09 1.1	25	7.812	1.578			1.4	54.5	34.9	10.6



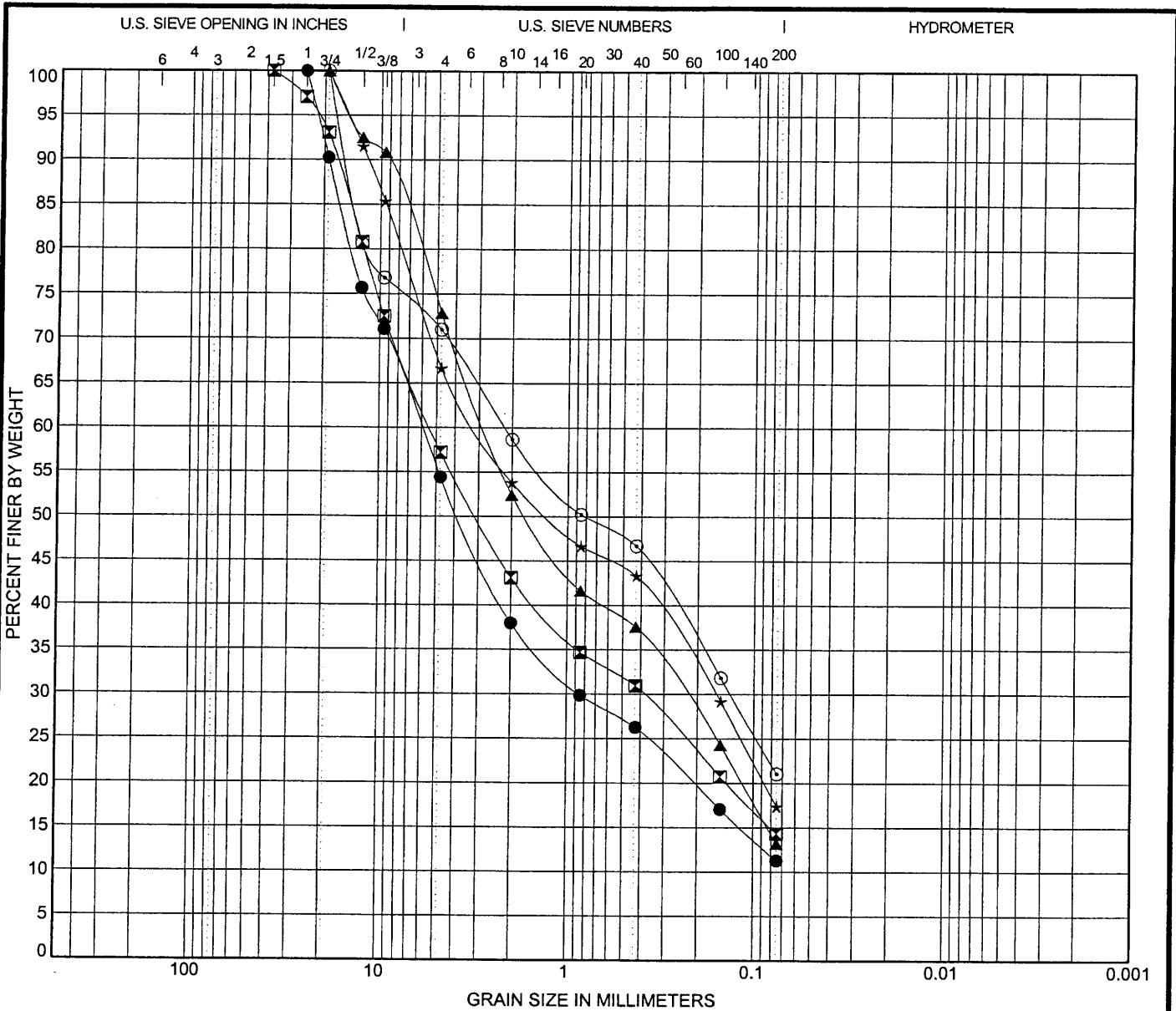
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

Project Number: Plate Number:



COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification					LL	PL	PI	Cc	Cu
●	B-09	2.6	WELL-GRADED GRAVEL with CLAY and SAND (GW-GC)				30	21	9	1.94	93.34
◻	B-09	4.1	CLAYEY SAND with GRAVEL (SC)				38	21	17		
▲	B-09	5.6	SILTY, CLAYEY SAND with GRAVEL (SC-SM)				27	21	6		
★	B-09	7.2	CLAYEY SAND with GRAVEL (SC)				39	24	15		
○	B-09	10.2	CLAYEY SAND with GRAVEL (SC)				34	22	12		



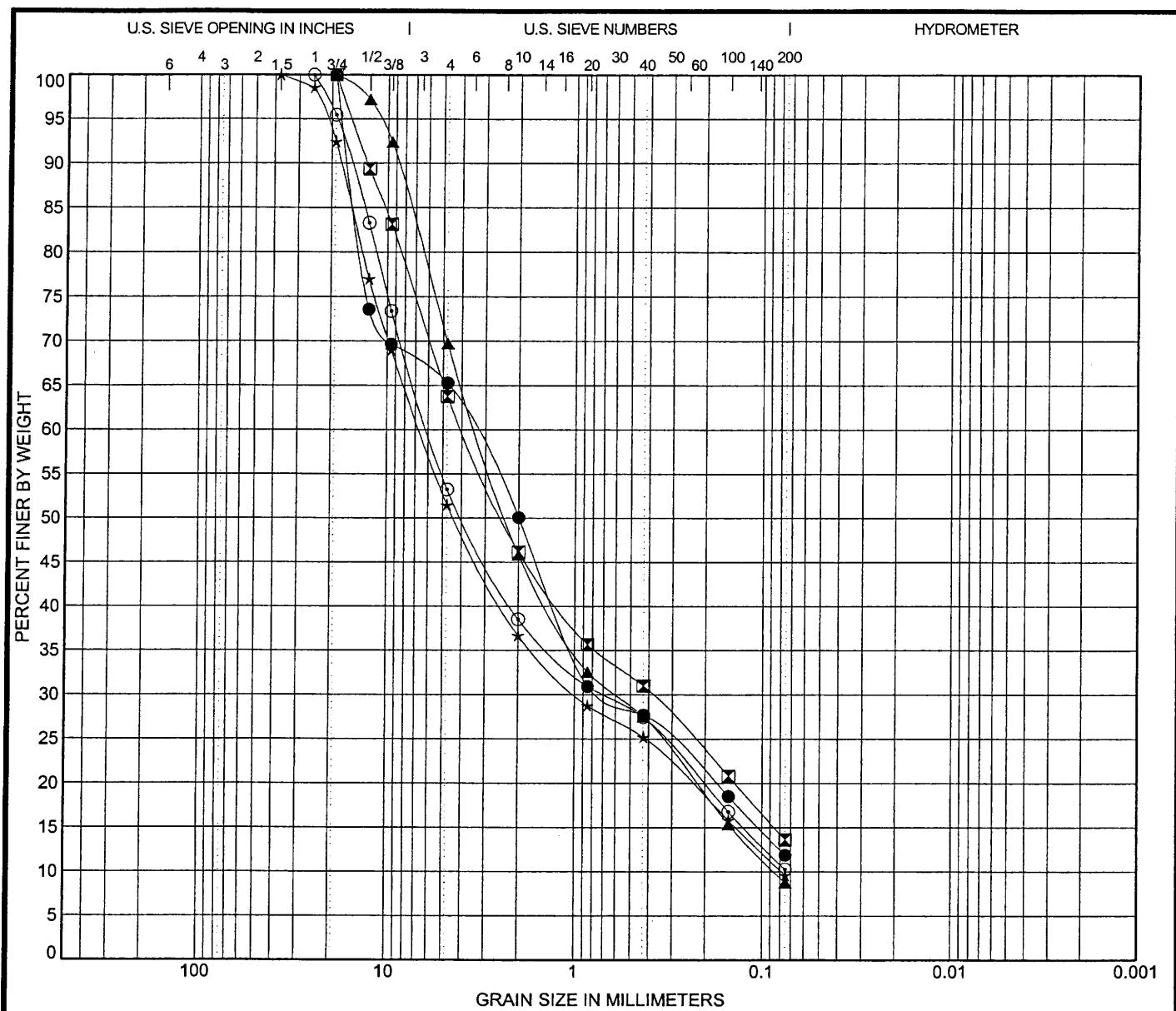
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

Project Number: Plate Number:



COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification						LL	PL	PI	Cc	Cu
●	B-09	14.8	WELL-GRADED SAND with CLAY and GRAVEL (SW-SC)					28	20	8	2.25	57.32
☒	B-10	1.1	SILTY, CLAYEY SAND with GRAVEL (SC-SM)					27	20	7		
▲	B-10	2.6	WELL-GRADED SAND with CLAY and GRAVEL (SW-SC)					39	23	16	1.26	39.22
★	B-10	4.1	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)					20	17	3	1.82	85.22
○	B-10	5.6	WELL-GRADED GRAVEL with SILTY CLAY and SAND (GW-GC)	22	18	4	1.14	82.38				

Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-09	14.8	19	3.519	0.698		1.7	34.7	53.4	11.9
☒	B-10	1.1	19	3.949	0.385		2.2	36.2	50.2	13.6
▲	B-10	2.6	19	3.341	0.599	0.085	0.7	30.3	60.9	8.8
★	B-10	4.1	37.5	6.659	0.973	0.078	1.3	48.5	41.8	9.6
○	B-10	5.6	25	5.994	0.706		1.6	46.8	43.0	10.3



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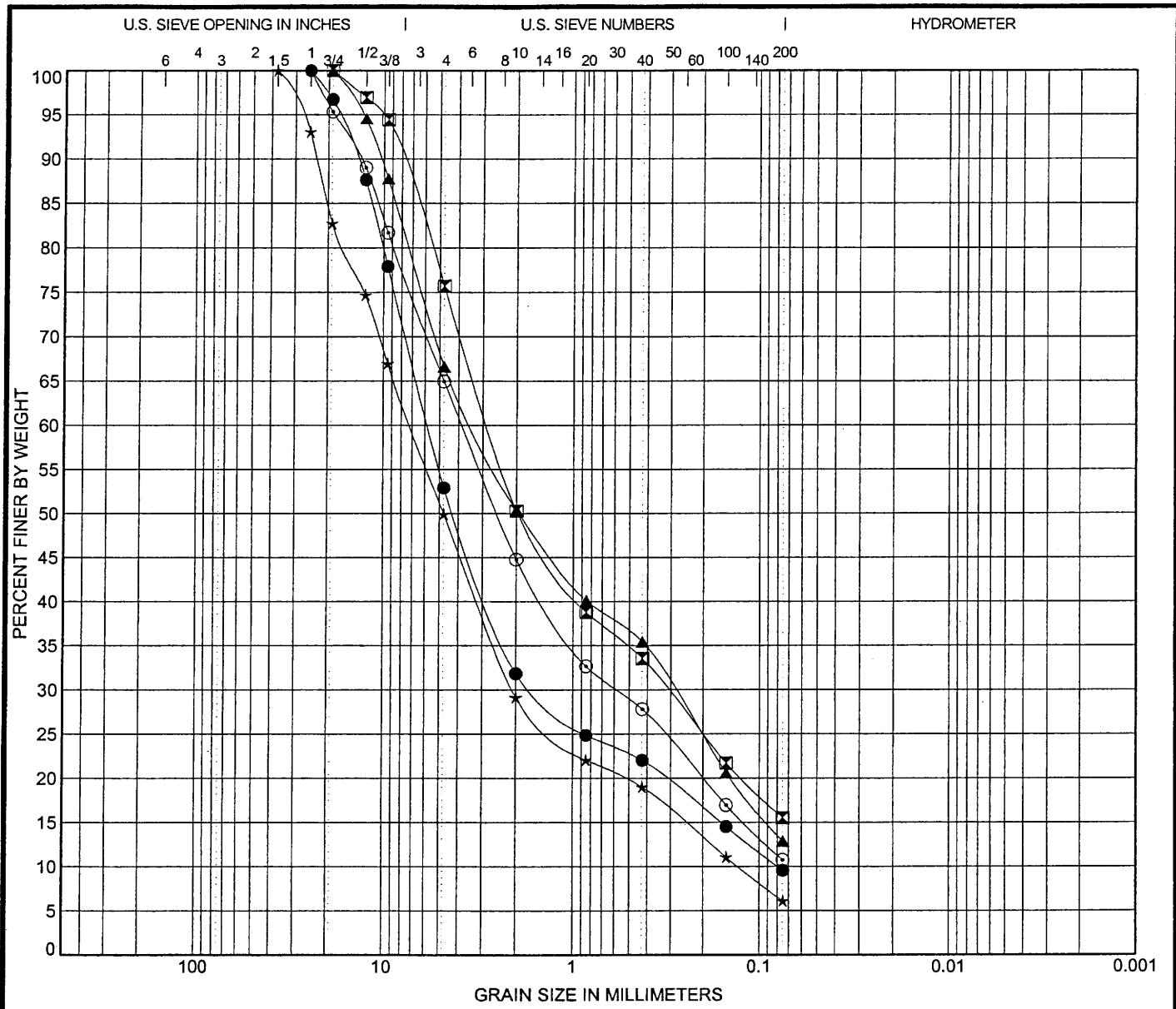
GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

Project Number: Plate Number:

4g



COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification						LL	PL	PI	Cc	Cu
●	B-10	5.9	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)					19	16	3	5.55	72.65
✖	B-10	17.8	CLAYEY SAND with GRAVEL (SC)					31	20	11		
▲	B-10	22.4	CLAYEY SAND with GRAVEL (SC)					32	20	12		
★	B-11	1.1	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)					NV	NV	NP	4.65	55.46
○	B-11	2.6	WELL-GRADED SAND with SILTY CLAY and GRAVEL (SW-SC)					21	16	5	1.28	55.65

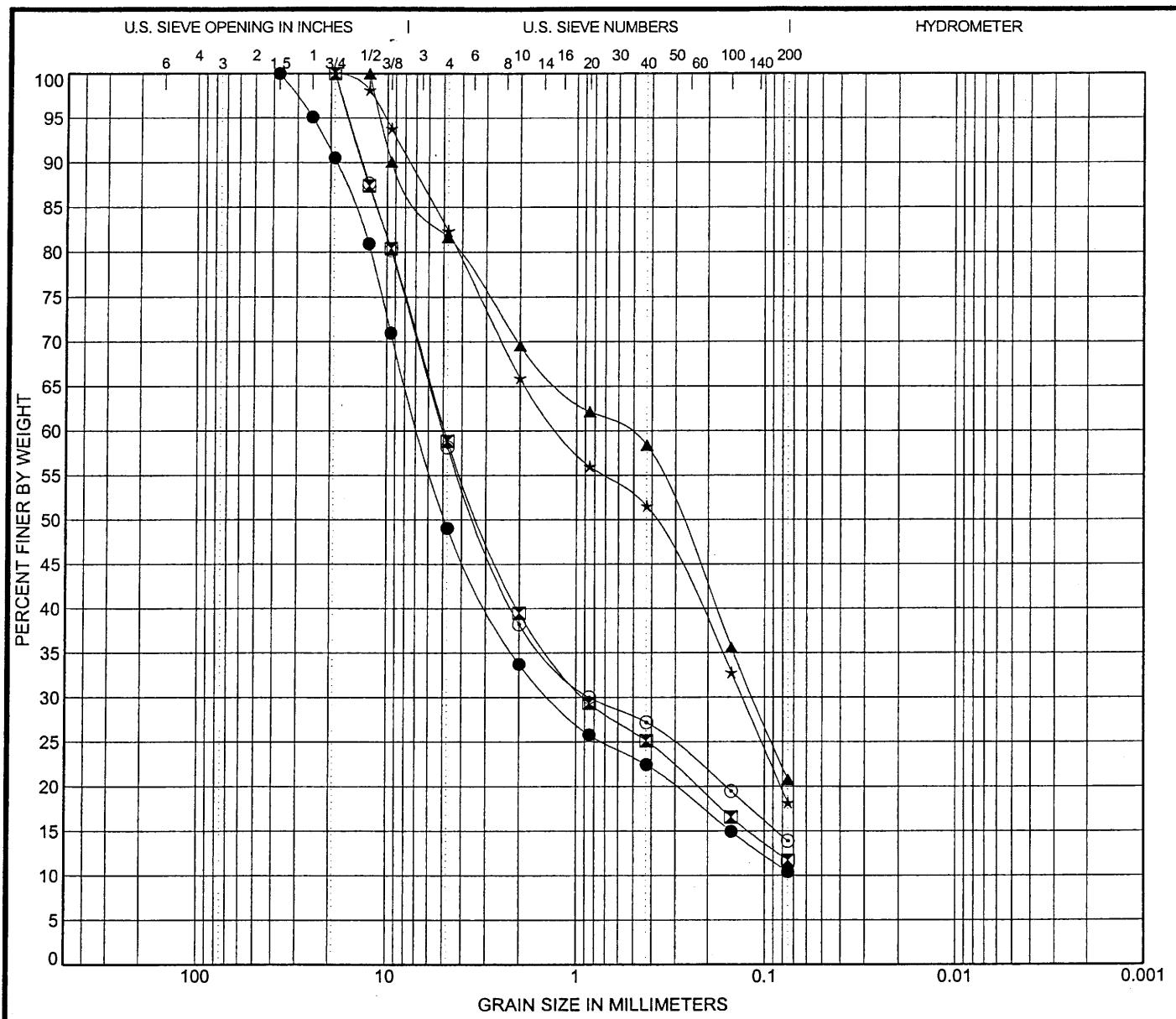
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-10	5.9	25	5.782	1.598	0.08	1.3	47.1	43.3	9.6
✖	B-10	17.8	19	2.785	0.311		2.5	24.3	60.2	15.5
▲	B-10	22.4	19	3.339	0.291		2.6	33.4	53.8	12.9
★	B-11	1.1	37.5	7.159	2.073	0.129	0.7	50.1	43.8	6.1
○	B-11	2.6	25	3.841	0.582		1.6	35.0	54.2	10.7



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls
Location: Las Vegas, Nevada
Project Number: Plate Number: 4h



COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification						LL	PL	PI	Cc	Cu
●	B-11 4.1	WELL-GRADED GRAVEL with SILTY CLAY and SAND (GW-GC)						26	19	7	3.79	95.50
☒	B-11 5.6	WELL-GRADED SAND with CLAY and GRAVEL (SW-SC)						30	19	11	2.80	83.94
▲	B-11 7.2	CLAYEY SAND with GRAVEL (SC)						40	22	18		
★	B-11 8.7	CLAYEY SAND with GRAVEL (SC)						35	22	13		
○	B-11 14.8	CLAYEY SAND with GRAVEL (SC)						26	17	9		

Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-11 4.1	37.5	6.716	1.338		0.9	51.0	38.6		10.4
☒	B-11 5.6	19	4.93	0.901		2.4	41.2	47.1		11.7
▲	B-11 7.2	12.5	0.573	0.116		6.7	18.4	60.9		20.8
★	B-11 8.7	19	1.2	0.132		5.9	17.6	64.2		18.1
○	B-11 14.8	19	5.035	0.85		2.8	41.9	44.3		13.9

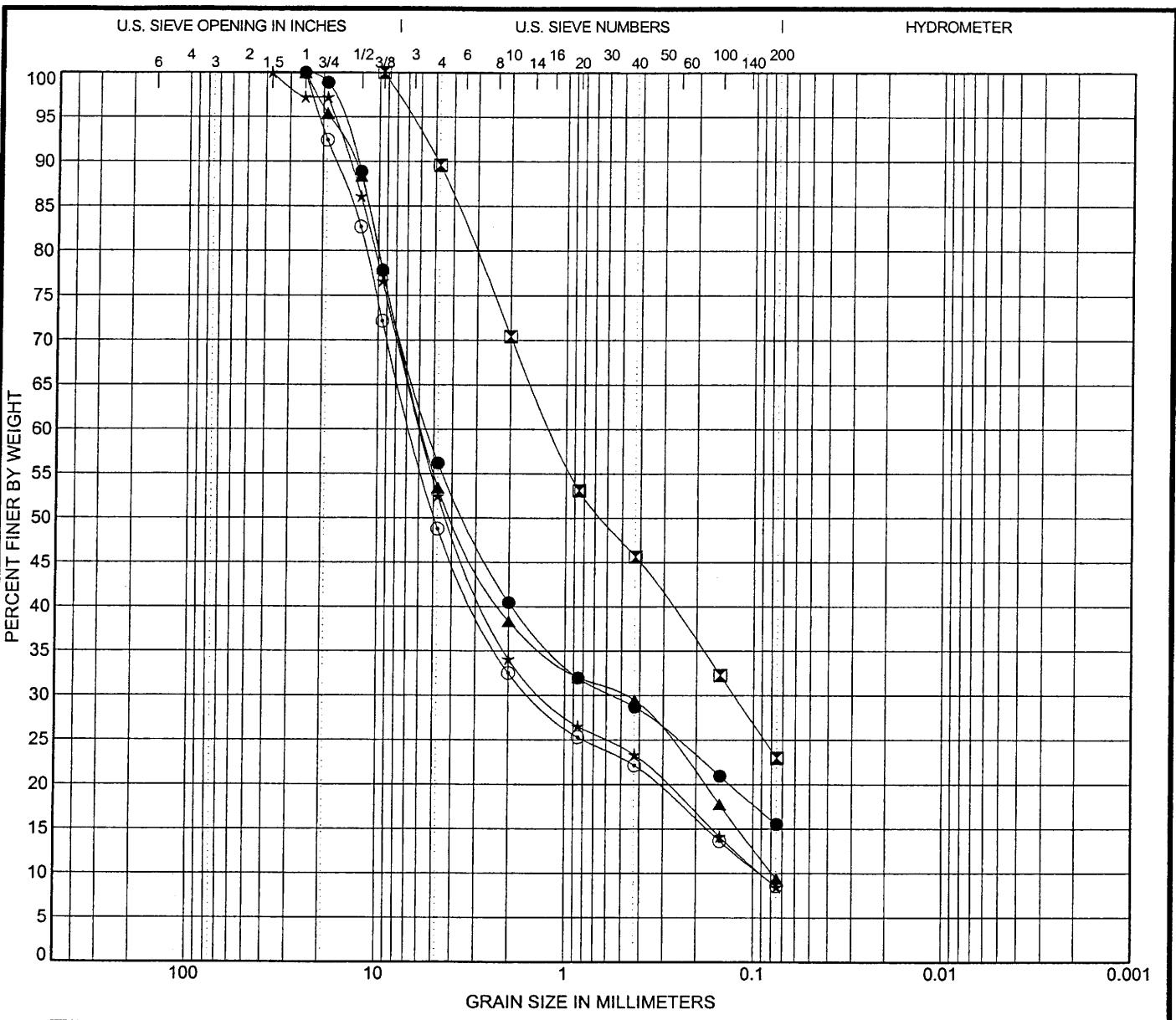
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

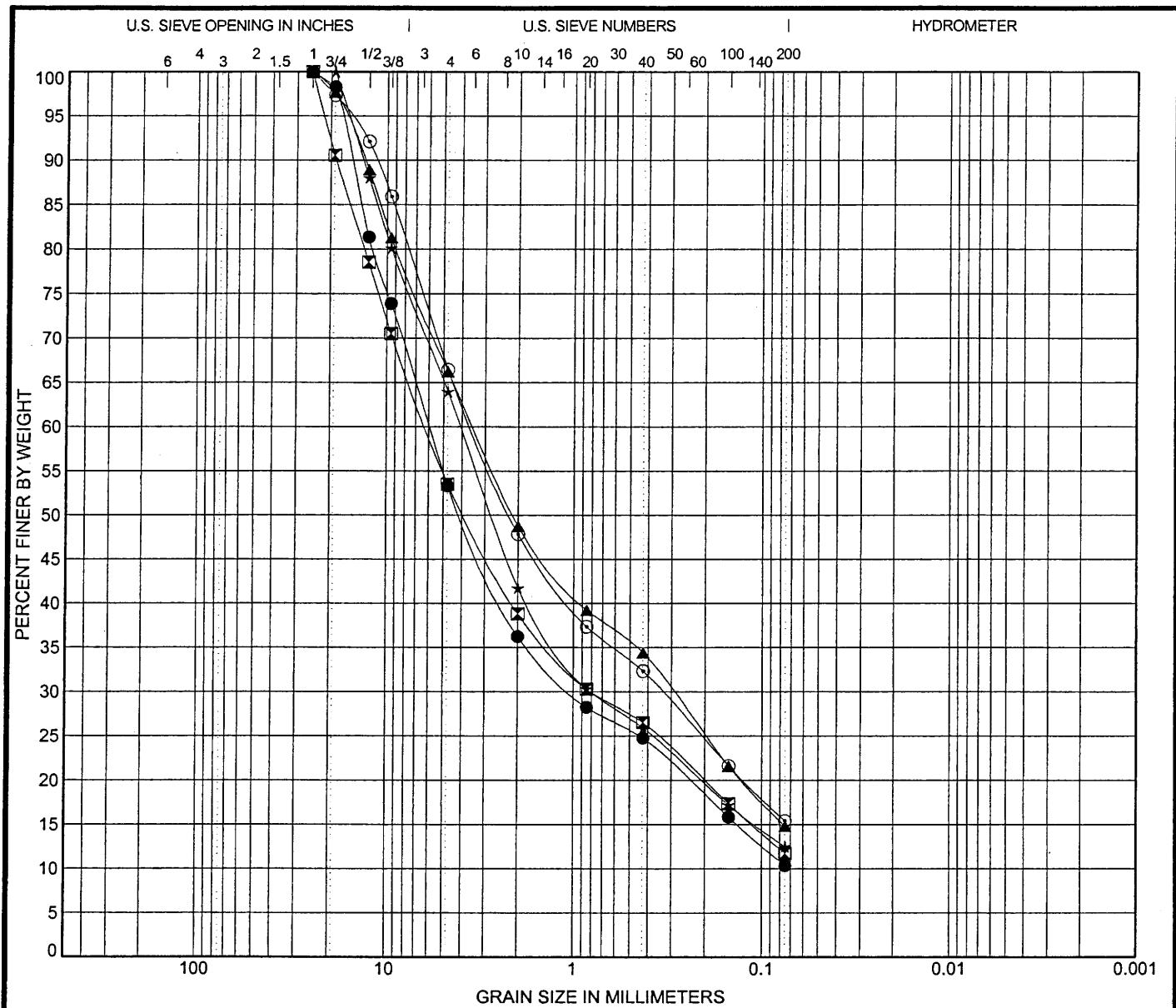
Project Number: Plate Number:



Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification					LL	PL	PI	Cc	Cu			
	GRAVEL		SAND										
COBBLES	coarse	fine	coarse	medium	fine	SILT OR CLAY							
● B-11 20.9	SILTY, CLAYEY GRAVEL with SAND (GC-GM)					18	14	4					
◻ B-11 22.4	SILTY, CLAYEY SAND (SC-SM)					25	19	6					
▲ B-12 1.1	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)					NV	NV	NP	0.53	72.46			
★ B-12 2.6	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)					NV	NV	NP	2.97	65.21			
○ B-12 3.8	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)					19	17	2	3.65	72.78			
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay				
● B-11 20.9	25	5.367	0.559		2.7	43.8	40.7			15.5			
◻ B-11 22.4	9.5	1.195	0.127		2.3	10.4	66.6			23.0			
▲ B-12 1.1	25	5.718	0.49	0.079	1.8	46.6	44.0			9.4			
★ B-12 2.6	37.5	5.897	1.259	0.09	1.4	47.5	44.0			8.5			
○ B-12 3.8	25	6.627	1.485	0.091	1.2	51.2	40.2			8.6			





COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification					LL	PL	PI	Cc	Cu
● B-12	5.6	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)					17	15	2	2.48	83.10
☒ B-12	11.7	WELL-GRADED GRAVEL with SILTY CLAY and SAND (GW-GC)					23	17	6	1.74	102.52
▲ B-13	1.1	SILTY, CLAYEY SAND with GRAVEL (SC-SM)					21	17	4		
★ B-13	2.6	SILTY, CLAYEY SAND with GRAVEL (SC-SM)					24	18	6		
○ B-13	4.1	CLAYEY SAND with GRAVEL (SC)					29	19	10		

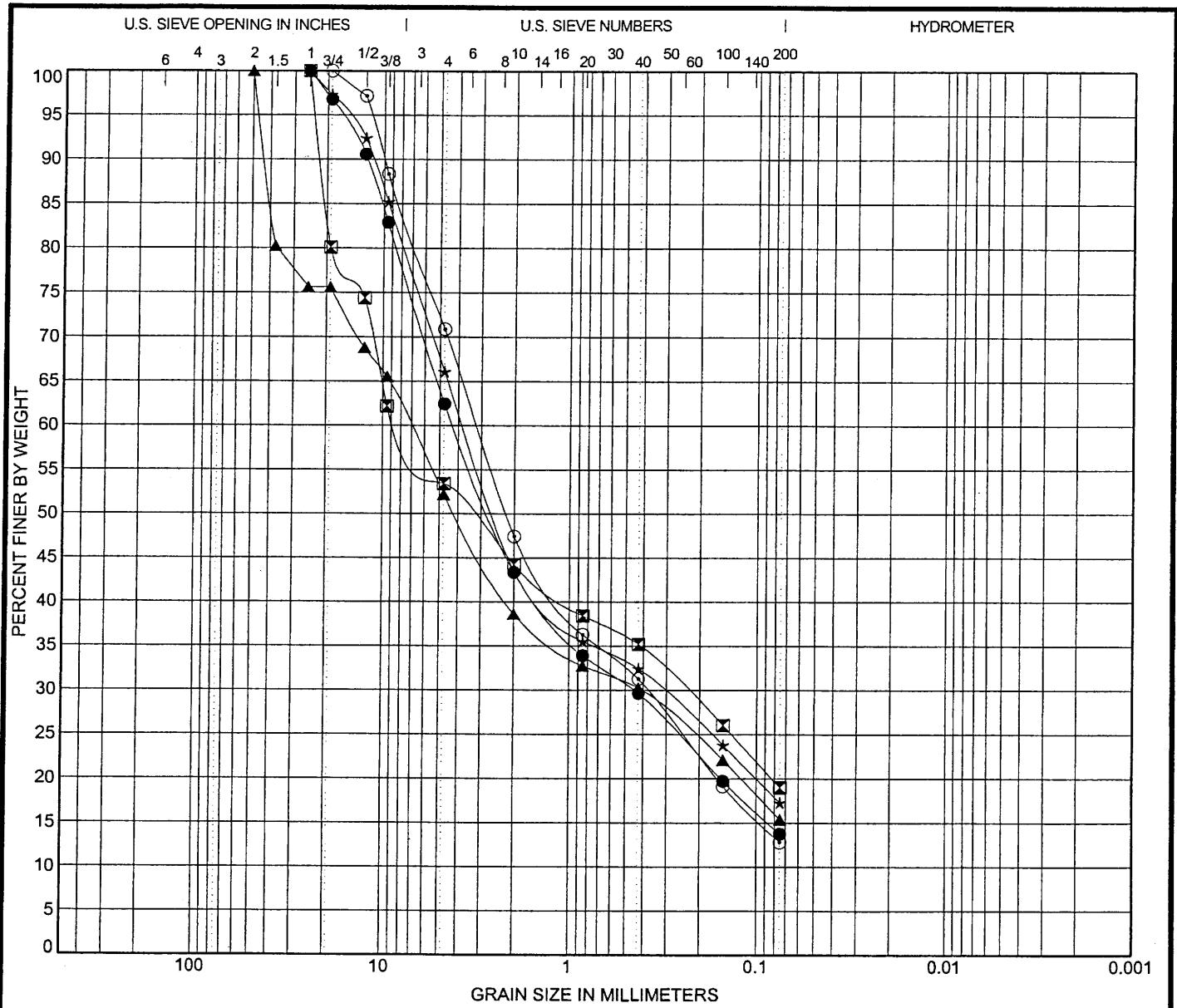
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-12		25	5.95	1.027		1.7	46.7	42.9		10.4
☒ B-12		25	6.187	0.806		2.1	46.5	41.8		11.8
▲ B-13		25	3.49	0.297		1.7	33.8	51.4		14.8
★ B-13		19	4.069	0.807		2.2	36.0	51.5		12.5
○ B-13		25	3.521	0.339		3.0	33.6	51.0		15.4



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls
Location: Las Vegas, Nevada
Project Number: Plate Number: 4k



COBBLES	GRAVEL		SAND			SILT OR CLAY				
	coarse	fine	coarse	medium	fine					

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification						LL	PL	PI	Cc	Cu
● B-13 5.6	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						24	19	5		
☒ B-13 7.2	CLAYEY GRAVEL with SAND (GC)						29	21	8		
▲ B-13 8.7	CLAYEY GRAVEL with SAND (GC)						26	17	9		
★ B-13 11.7	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						23	16	7		
○ B-13 14.8	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						26	21	5		
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
● B-13 5.6	25	4.251	0.45		2.5	37.5	48.7		13.8		
☒ B-13 7.2	25	8.004	0.235		3.5	46.6	34.4		19.0		
▲ B-13 8.7	50	7.134	0.411		3.1	47.8	36.8		15.4		
★ B-13 11.7	25	3.762	0.317		3.5	33.9	48.8		17.3		
○ B-13 14.8	19	3.18	0.381		1.5	29.1	58.1		12.8		



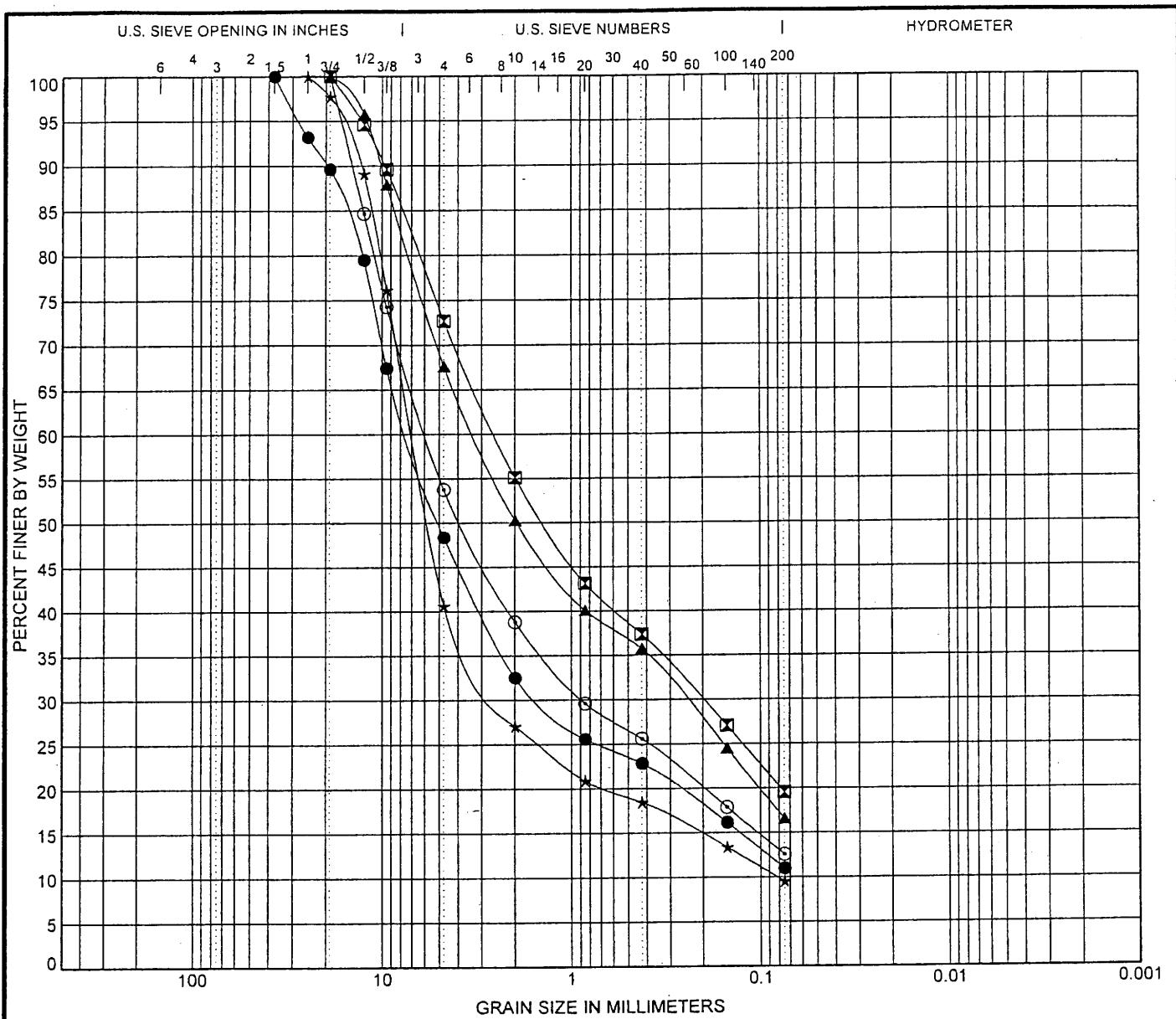
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening / Project 2D Retaining Walls

Location: Las Vegas, Nevada

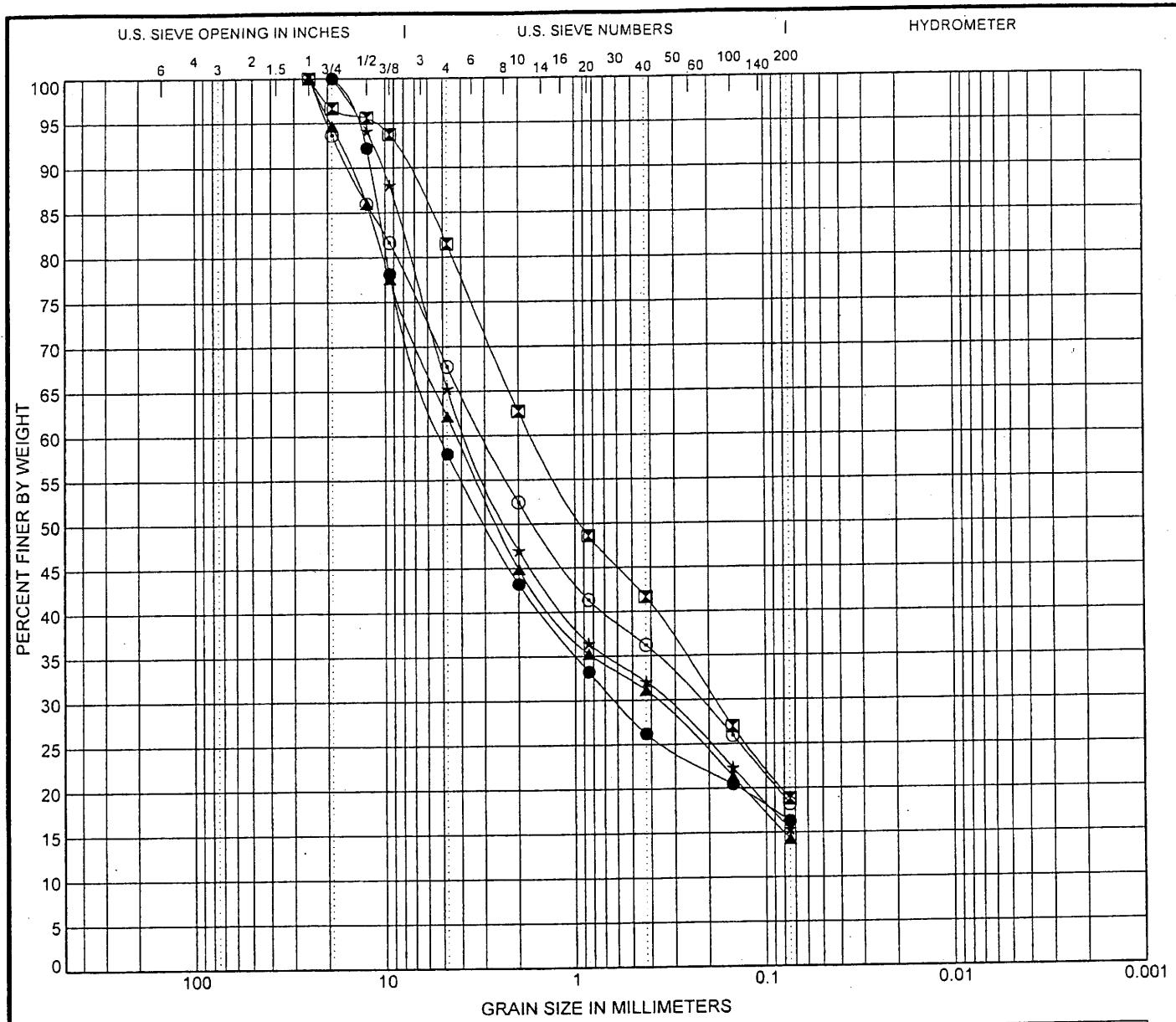
Project Number: Plate Number:



COBBLES	GRAVEL		SAND			SILT OR CLAY				
	coarse	fine	coarse	medium	fine					

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification		Classification							LL	PL	PI	Cc	Cu
●	B-14	0.9	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)	20	16	4	4.53	110.70					
☒	B-14	1.5	SILTY, CLAYEY SAND with GRAVEL (SC-SM)		19	14	5						
▲	B-14	3.0	CLAYEY SAND with GRAVEL (SC)		24	16	8						
★	B-14	6.2	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)		23	14	9	10.35	85.35				
○	B-14	7.8	SILTY, CLAYEY GRAVEL with SAND (GC-GM)		22	15	7						
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay			
●	B-14	0.9	37.5	7.252	1.467		2.0	51.6	37.4		11.0		
☒	B-14	1.5	19	2.543	0.202		2.8	27.3	53.2		19.5		
▲	B-14	3.0	19	3.25	0.25		3.0	32.4	51.0		16.6		
★	B-14	6.2	25	6.931	2.413	0.081	3.2	59.4	31.1		9.6		
○	B-14	7.8	19	5.865	0.883		1.9	46.2	41.2		12.6		



Note: NV - No Value, NP - Non Plastic, sample depth in meters.

GRAIN SIZE2 METRIC 0324013 GP US LAB GDT 12/9/2002

Specimen Identification	Classification						LL	PL	PI	Cc	Cu
	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
● B-14 9.1	CLAYEY GRAVEL with SAND (GC)				4.0	42.0	41.7		16.3		
☒ B-14 10.7	CLAYEY SAND with GRAVEL (SC)				2.5	18.5	62.7		18.8		
▲ B-15 0.8	CLAYEY SAND with GRAVEL (SC)				2.8	37.8	47.9		14.3		
★ B-15 1.5	CLAYEY SAND with GRAVEL (SC)				3.3	34.7	49.9		15.4		
○ B-15 3.0	SILTY, CLAYEY SAND with GRAVEL (SC-SM)				4.1	32.2	49.5		18.2		



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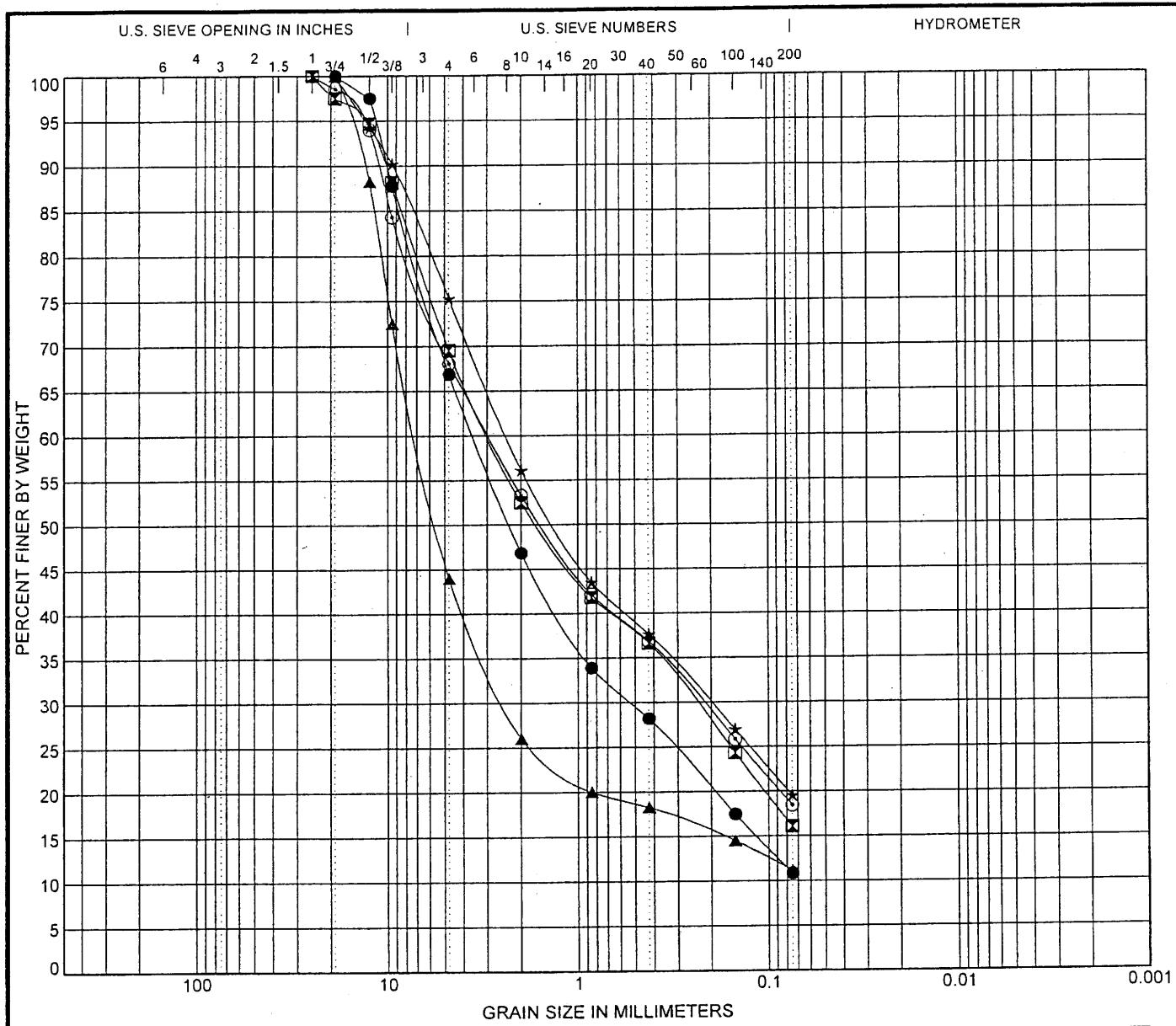
GRAIN SIZE DISTRIBUTION

Project: US 95 - Rainbow Blvd Retaining Walls

Location: Las Vegas, Nevada

Project Number: 0324-01-3

Plate Number: 4b



Note: NV - No Value, NP - Non Plastic, sample depth in meters.

COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

B-15		3.3	POCKET GRADED GRAVEL WITH CLAY AND SAND (SC-SC)										
★	B-15	10.8	CLAYEY SAND with GRAVEL (SC)						23	14	9		
◎	B-15	11.6	CLAYEY SAND with GRAVEL (SC)						22	14	8		
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt		%Clay		
●	B-15	4.6	19	3.532	0.53		2.5	33.1	56.0		10.9		
☒	B-15	6.1	25	2.929	0.243		3.1	30.5	53.4		16.1		
▲	B-15	9.3	19	7.012	2.423		1.8	56.0	32.8		11.2		
★	B-15	10.8	19	2.381	0.202		2.8	24.7	55.7		19.6		
◎	B-15	11.6	25	2.963	0.222		2.6	31.9	49.6		18.5		

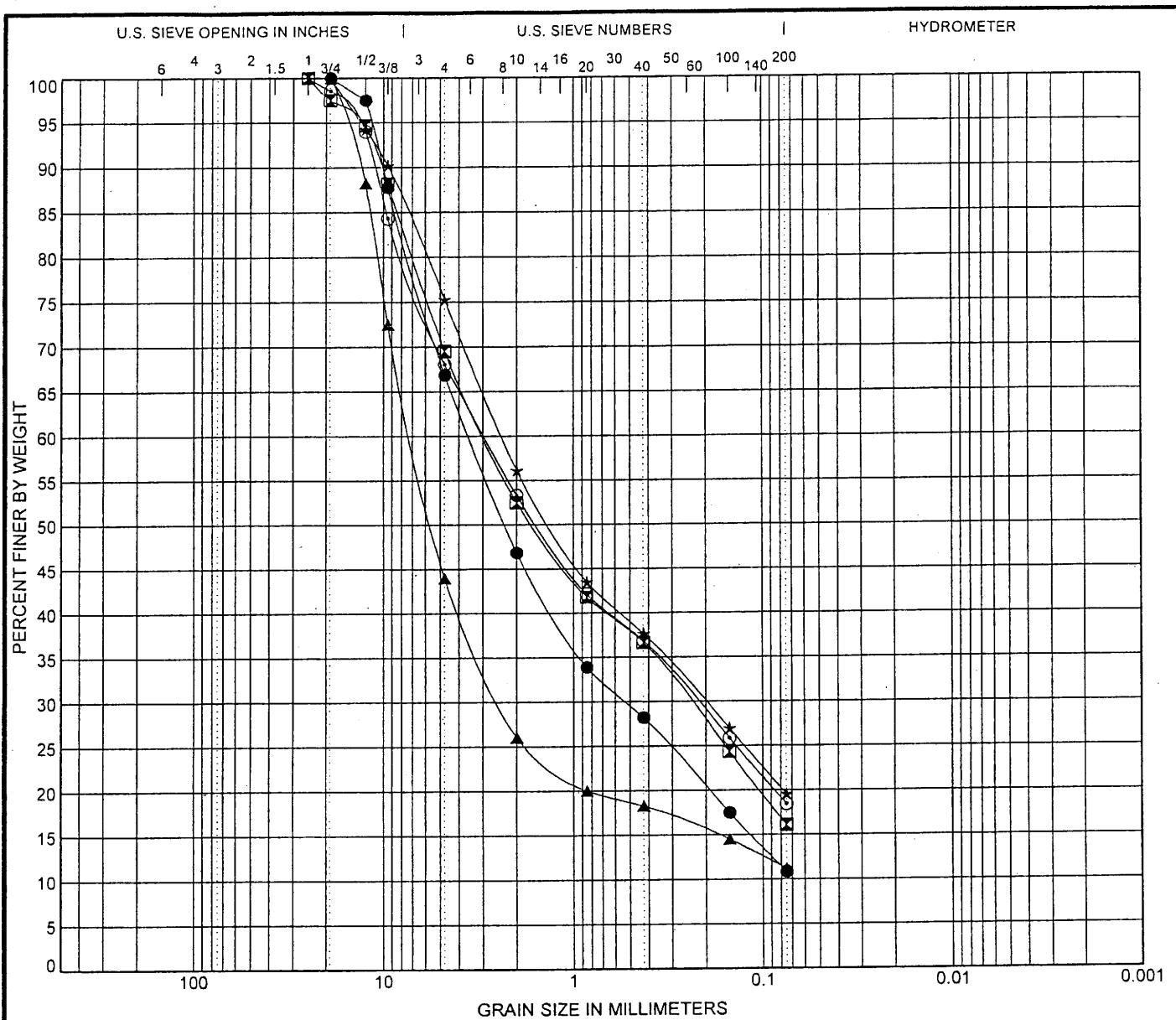


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GRAIN SIZE DISTRIBUTION

Project: US 95 - Rainbow Blvd Retaining Walls

Location: Las Vegas, Nevada



COBBLES	GRAVEL			SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine				
● B-15 4.6	WELL-GRADED SAND with SILTY CLAY and GRAVEL (SW-SC)			23	18	5	1.16	51.73	

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

GRAIN SIZE2 METRIC 0324013.GP.J.US LAB GDT 1/29/2002

Specimen Identification	Classification						LL	PL	PI	Cc	Cu
● B-15 4.6	WELL-GRADED SAND with SILTY CLAY and GRAVEL (SW-SC)			23	18	5	1.16	51.73			
■ B-15 6.1	CLAYEY SAND with GRAVEL (SC)			25	17	8					
▲ B-15 9.3	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)			23	14	9	14.32	119.92			
★ B-15 10.8	CLAYEY SAND with GRAVEL (SC)			23	14	9					
○ B-15 11.6	CLAYEY SAND with GRAVEL (SC)			22	14	8					
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
● B-15 4.6	19	3.532	0.53		2.5	33.1	56.0			10.9	
■ B-15 6.1	25	2.929	0.243		3.1	30.5	53.4			16.1	
▲ B-15 9.3	19	7.012	2.423		1.8	56.0	32.8			11.2	
★ B-15 10.8	19	2.381	0.202		2.8	24.7	55.7			19.6	
○ B-15 11.6	25	2.963	0.222		2.6	31.9	49.6			18.5	

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GRAIN SIZE DISTRIBUTION

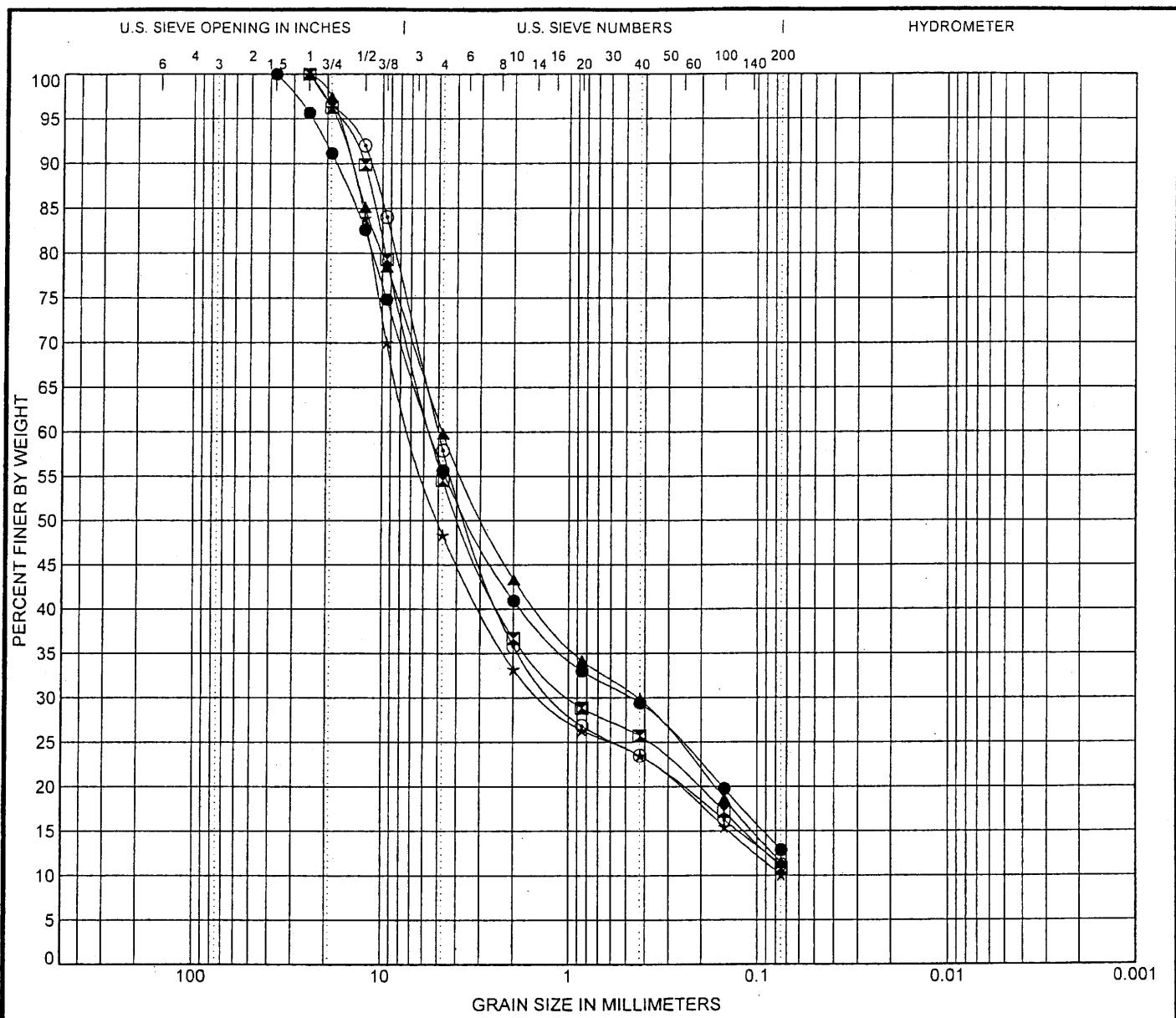
Project: US 95 - Rainbow Blvd Retaining Walls

Location: Las Vegas, Nevada

Project Number: 0324 01 3

Plate Number: 4c

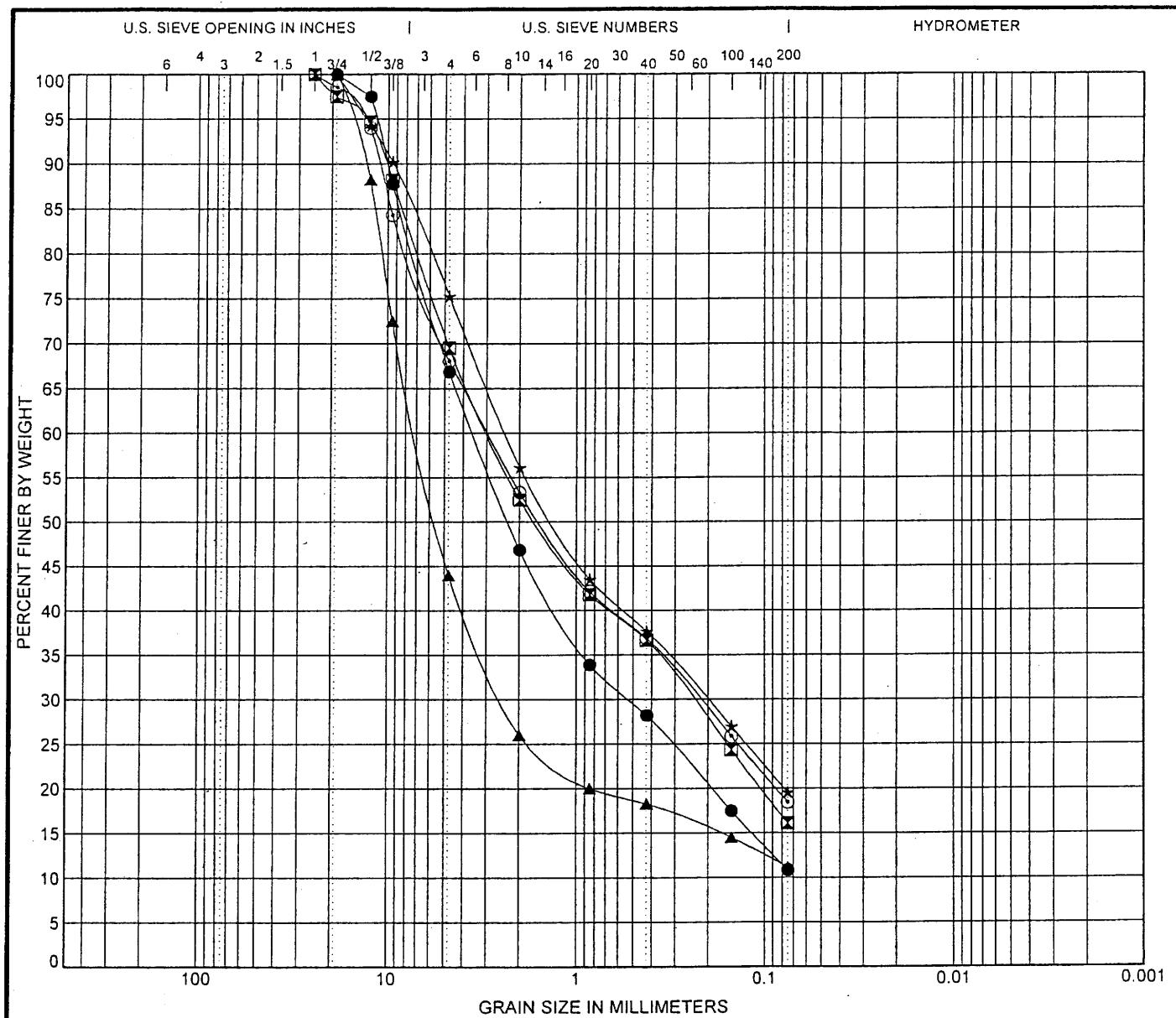




Note: NV - No Value, NP - Non Plastic, sample depth in meters.

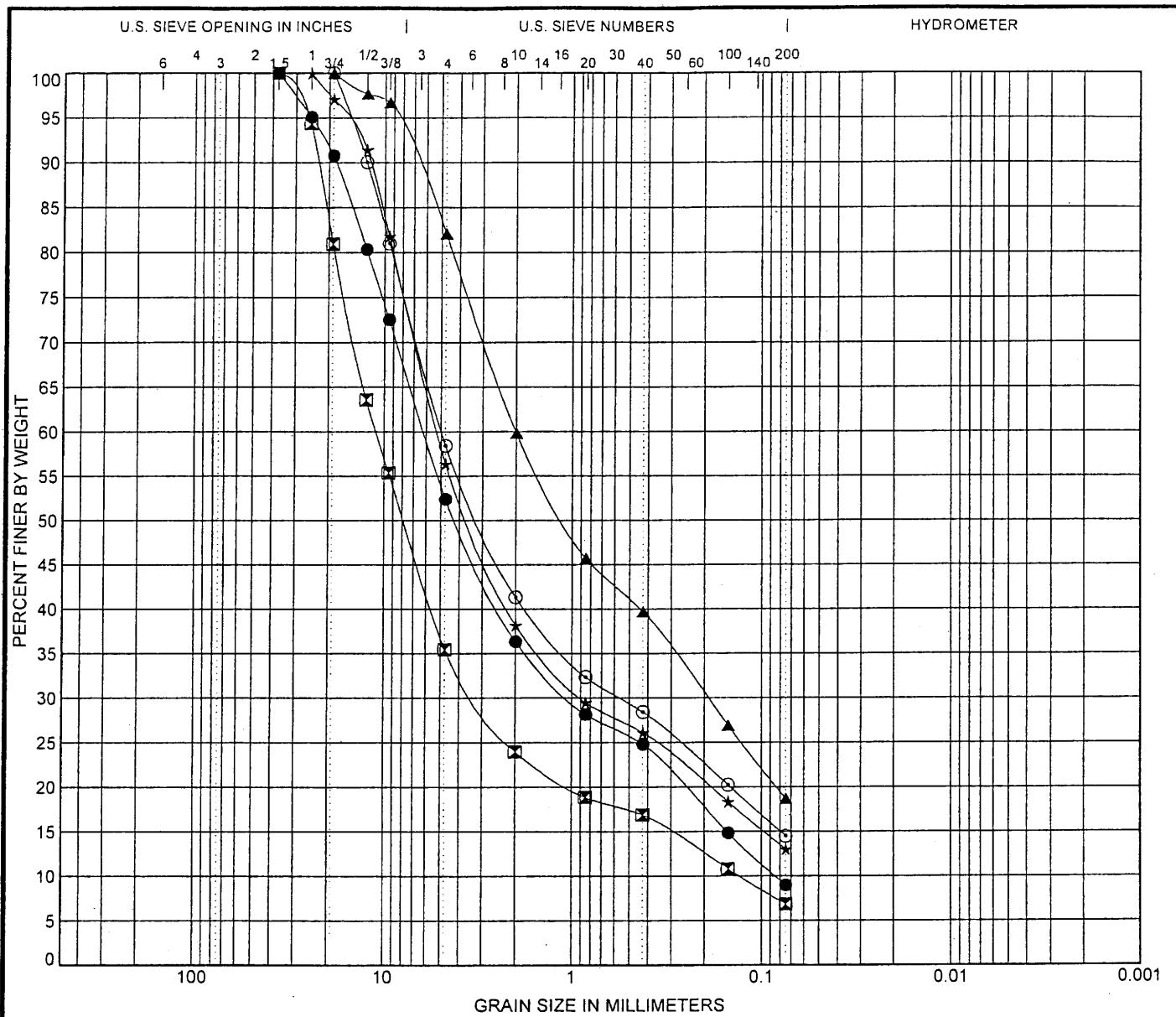
Specimen Identification	Classification							LL	PL	PI	Cc	Cu
	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt		%Clay		
● B-17	0.9		SILTY, CLAYEY GRAVEL with SAND (GC-GM)			1.7	44.3	42.8			12.9	
☒ B-17	1.7		WELL-GRADED GRAVEL with SILTY CLAY and SAND (GW-GC)	26		1.4	45.5	43.6			10.9	
▲ B-17	3.2	25	4.782	0.436		1.4	40.2	48.3			11.5	
★ B-17	4.7	25	6.893	1.341		1.4	51.6	38.3			10.1	
○ B-17	6.2	25	5.02	1.151		0.9	42.1	46.6			11.3	





Note: NV - No Value, NP - Non Plastic, sample depth in meters.



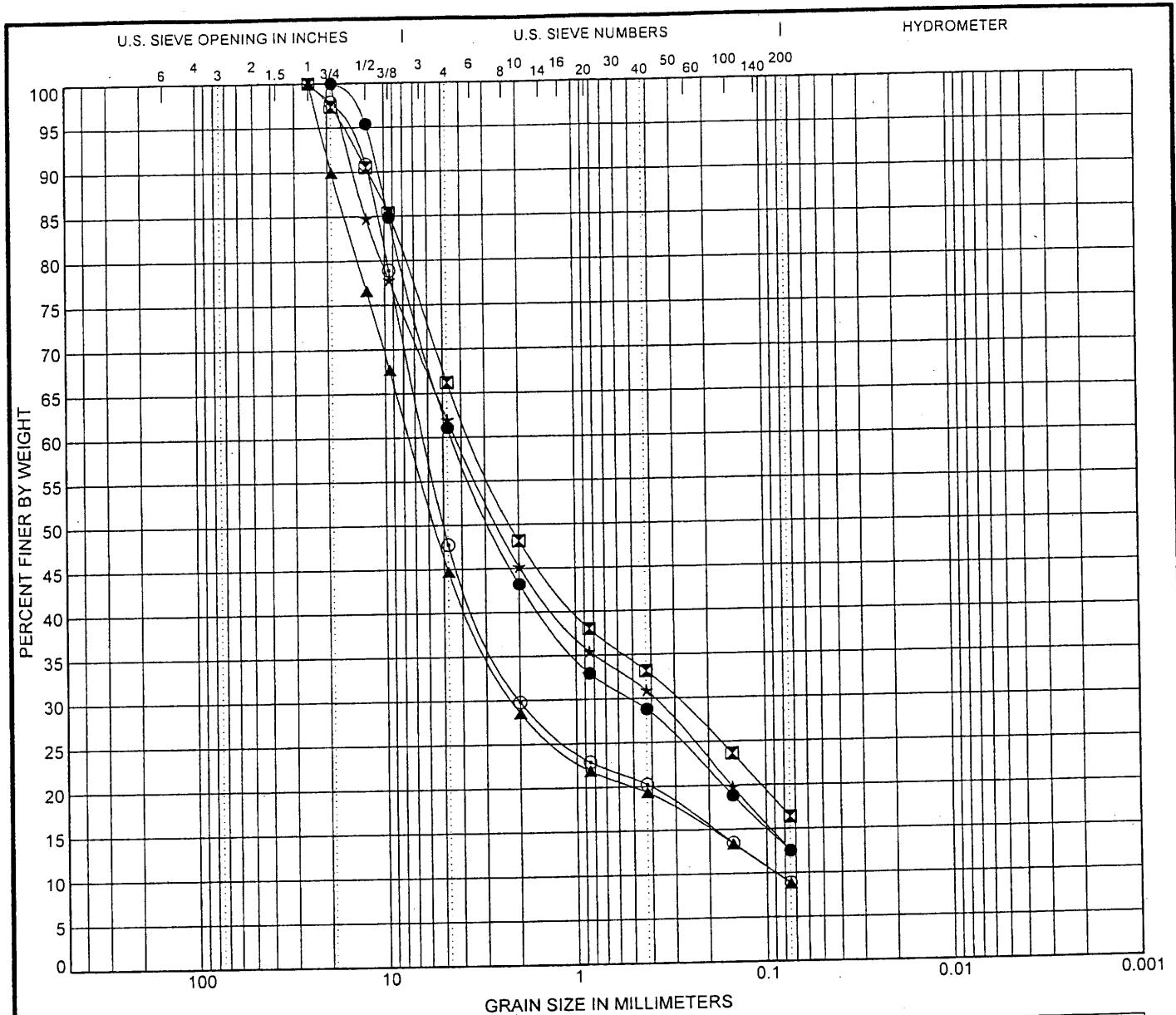


COBBLES	GRAVEL		SAND			SILT OR CLAY				
	coarse	fine	coarse	medium	fine					

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification						LL	PL	PI	Cc	Cu
● B-16 0.9	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						20	17	3	2.04	73.11
☒ B-16 1.7	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)						15	18	7	6.91	85.48
▲ B-16 3.0	CLAYEY SAND with GRAVEL (SC)						43	24	19		
★ B-16 4.6	CLAYEY GRAVEL with SAND (GC)						36	20	16		
○ B-16 6.1	CLAYEY SAND with GRAVEL (SC)						35	21	14		
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
● B-16 0.9	37.5	6.17	1.031	0.084	1.5	47.6	43.4		9.0		
☒ B-16 1.7	37.5	11.092	3.153	0.13	1.3	64.6	28.6		6.9		
▲ B-16 3.0	19	2.012	0.193			4.5	17.9	63.4		18.7	
★ B-16 4.6	25	5.243	0.894			2.8	43.6	43.3		13.0	
○ B-16 6.1	19	4.984	0.561			2.8	41.6	43.9		14.5	





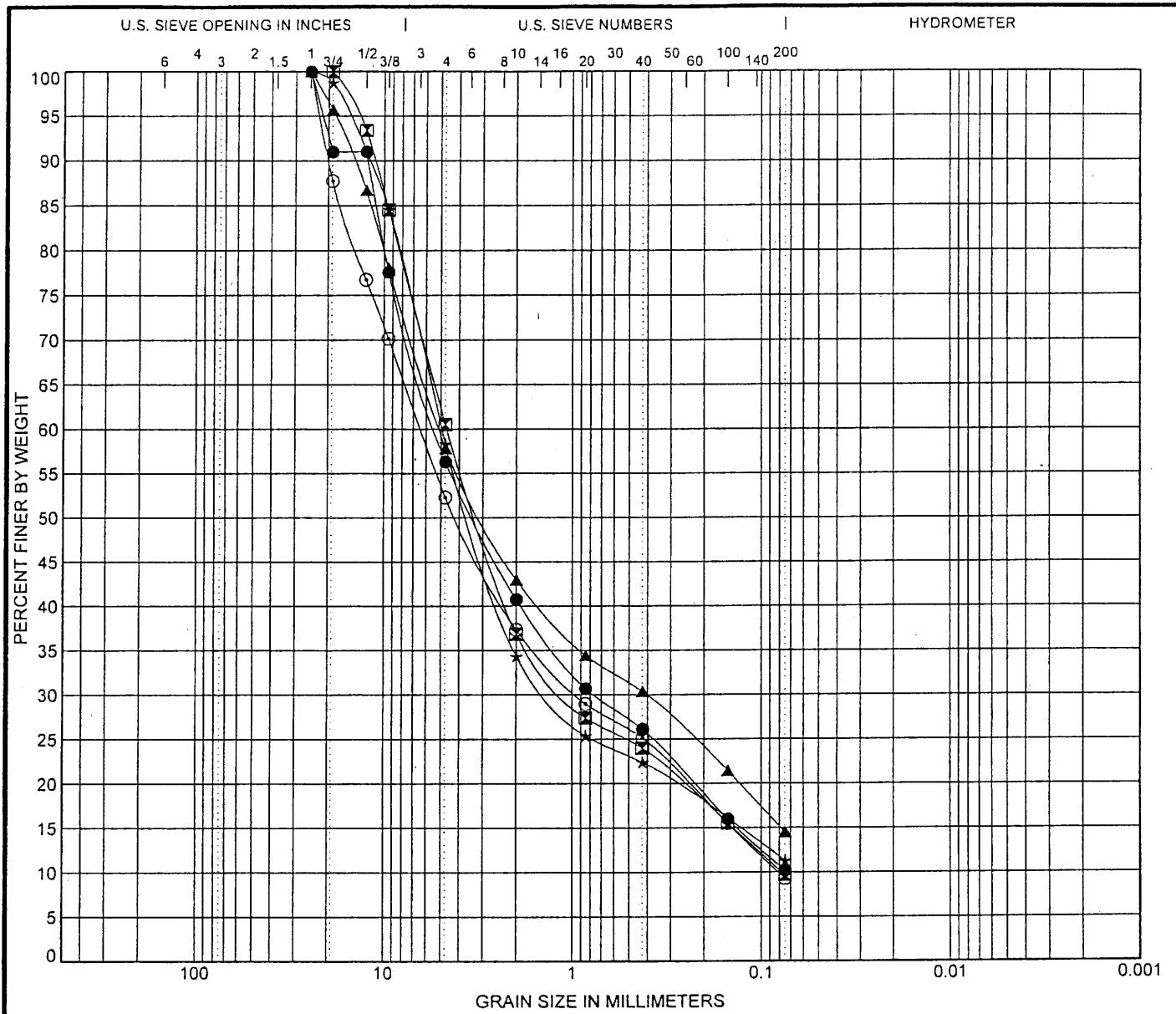
COBBLES	GRAVEL			SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine					
● B-17	7.0					SILTY SAND with GRAVEL (SM)	19	17	2	
☒ B-18	0.9					SILTY, CLAYEY SAND with GRAVEL (SC-SM)	20	16	4	
▲ B-18	1.7					POORLY GRADED GRAVEL with SILT and SAND (GP-GM)	18	17	1	6.92 83.80
★ B-18	3.0					SILTY, CLAYEY SAND with GRAVEL (SC-SM)	23	17	6	
○ B-18	4.7					POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)	21	16	5	7.37 70.29

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification						LL	PL	PI	Cc	Cu
● B-17	SILTY SAND with GRAVEL (SM)						19	17	2		
☒ B-18	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						20	16	4		
▲ B-18	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						18	17	1	6.92	83.80
★ B-18	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						23	17	6		
○ B-18	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)						21	16	5	7.37	70.29

Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-17	7.0	19	4.509	0.52		1.0	38.9	48.5	12.5
☒ B-18	0.9	25	3.528	0.301		1.4	33.8	49.8	16.4
▲ B-18	1.7	25	7.532	2.164	0.09	1.0	55.3	35.9	8.8
★ B-18	3.0	19	4.286	0.39		1.6	38.0	49.4	12.6
○ B-18	4.7	25	6.236	2.02	0.089	1.4	52.2	38.9	8.9



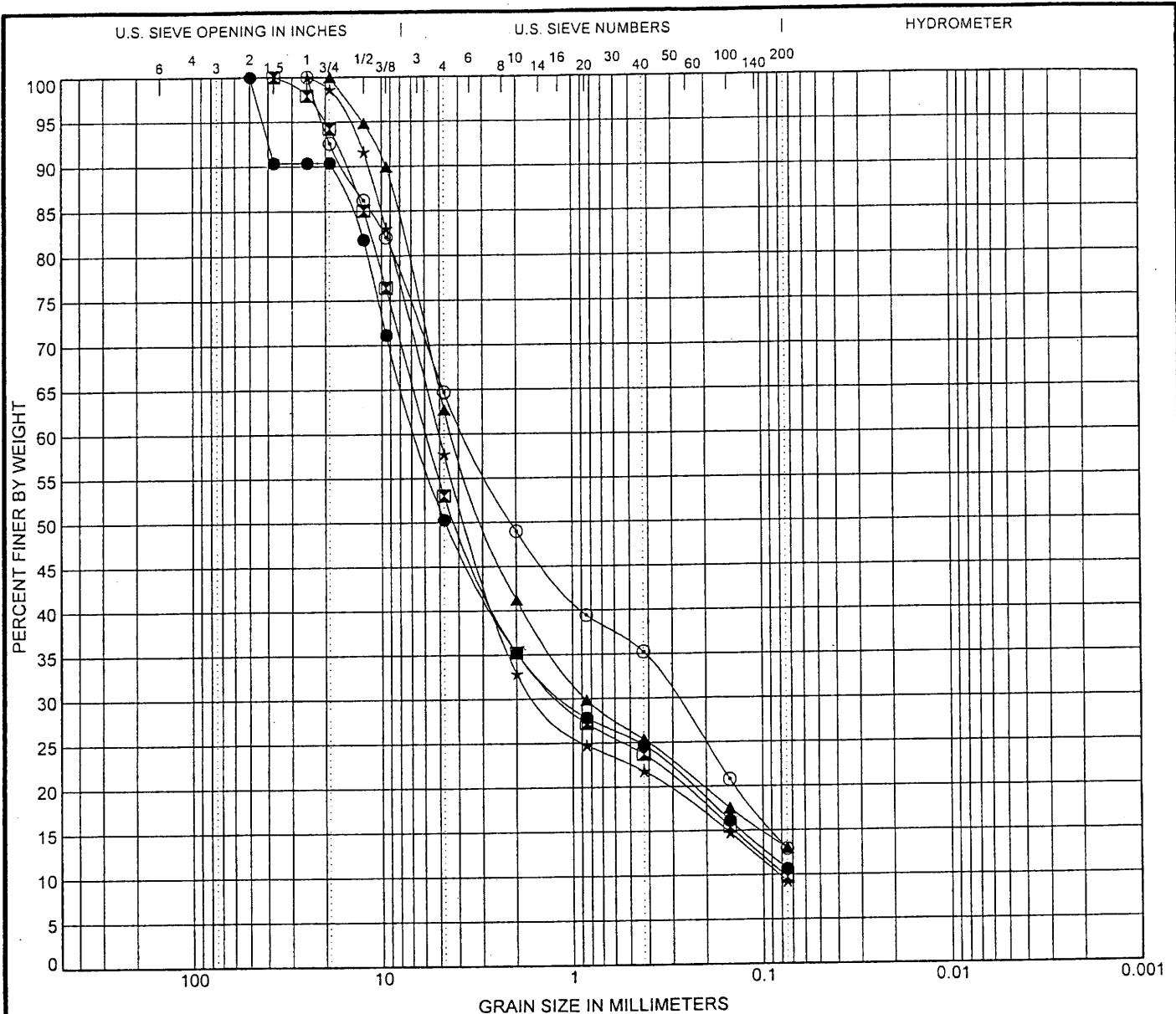


COBBLES	GRAVEL		SAND			SILT OR CLAY				
	coarse	fine	coarse	medium	fine					

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification							LL	PL	PI	Cc	Cu
● B-18 6.1	WELL-GRADED SAND with SILTY CLAY and GRAVEL (SW-SC)	22	17	5	1.50	73.44						
◻ B-18 7.0	WELL-GRADED SAND with SILTY CLAY and GRAVEL (SW-SC)	20	15	5	3.21	60.01						
▲ B-19 0.9	SILTY SAND with GRAVEL (SM)		19	16	3							
★ B-19 1.7	POORLY GRADED SAND with SILT and GRAVEL (SP-SM)		18	17	1	5.70	80.37					
○ B-19 3.0	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)		20	18	2	1.72	78.97					
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt		%Clay		
● B-18 6.1	25	5.357	0.765		1.5	43.7	46.1	10.2				
◻ B-18 7.0	19	4.659	1.078	0.078	1.4	39.5	50.8	9.7				
▲ B-19 0.9	25	5.115	0.407		1.0	42.2	43.3	14.5				
★ B-19 1.7	25	4.963	1.322		0.9	41.7	47.0	11.3				
○ B-19 3.0	25	6.405	0.944	0.081	0.8	47.7	43.0	9.3				





COBBLES	GRAVEL			SAND			SILT OR CLAY				
	coarse	fine	coarse	medium	fine						

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

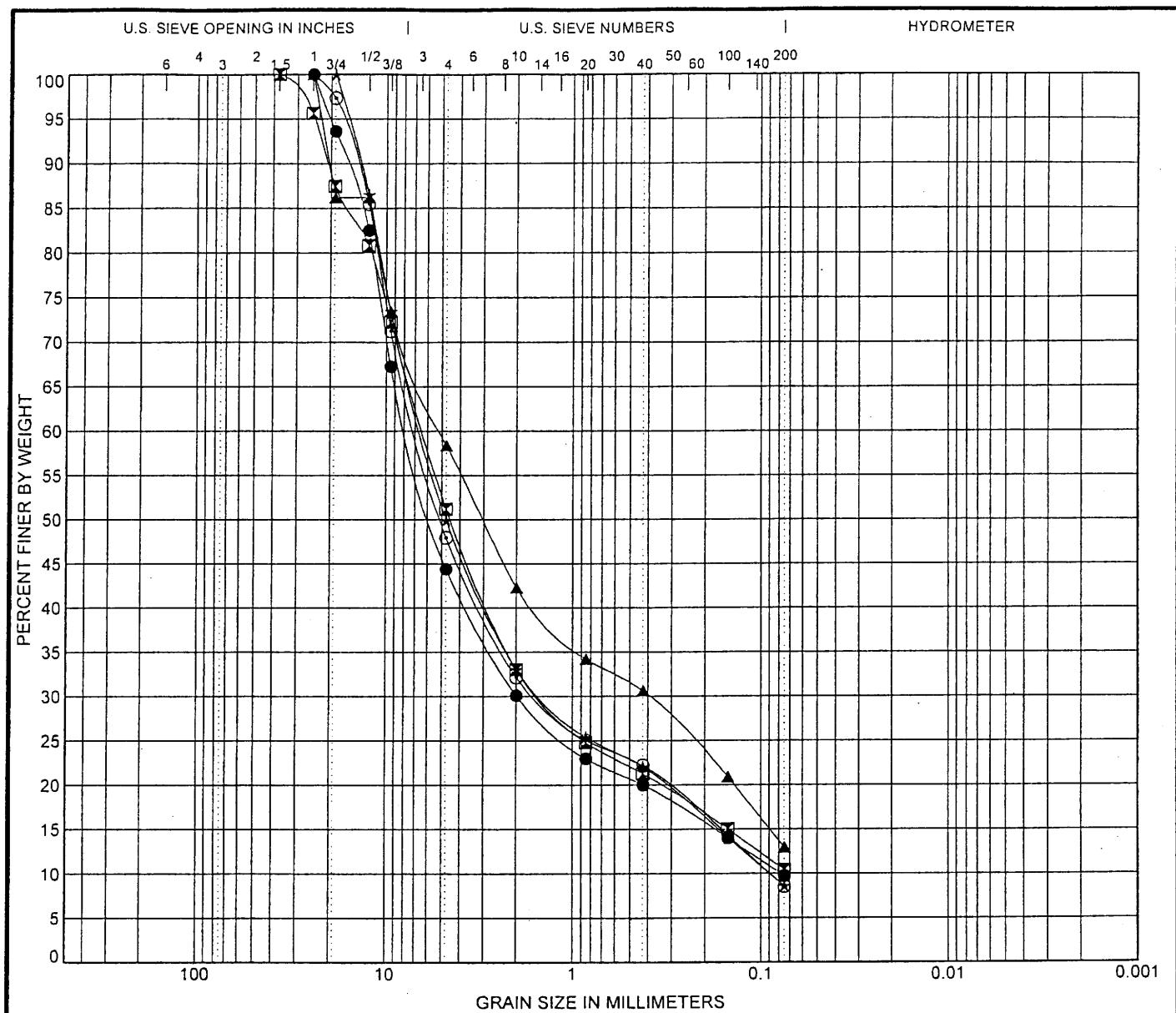


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GRAIN SIZE DISTRIBUTION

Project: US 95 - Rainbow Blvd Retaining Walls

Location: Las Vegas, Nevada

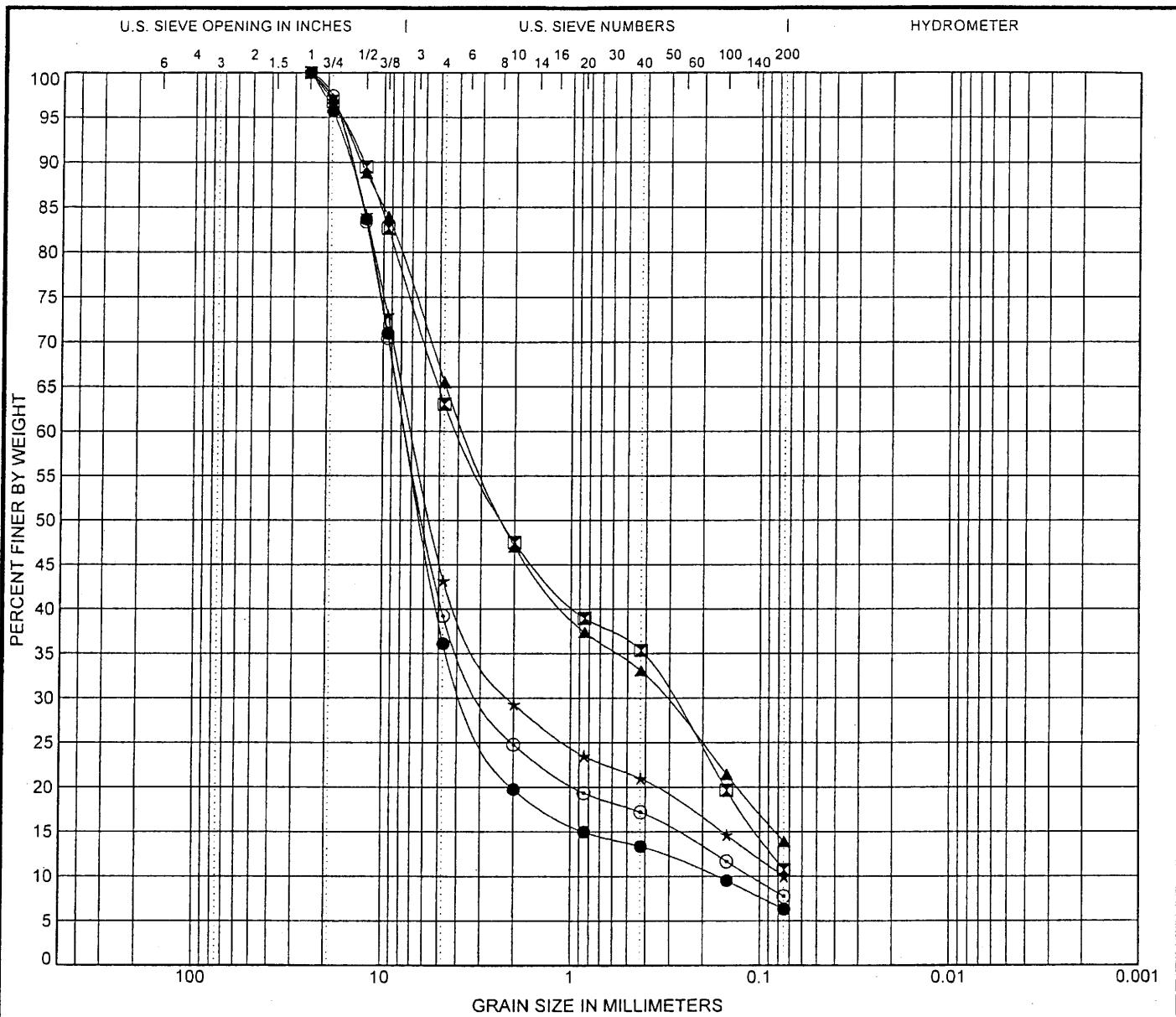


COBBLES	GRAVEL			SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine		

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification							LL	PL	PI	Cc	Cu
● B-19	13.7	Poorly Graded Gravel with Silty Clay and Sand (GP-GC)	21	16	5	6.60	97.78					
☒ B-20	0.8	Poorly Graded Gravel with Silt and Sand (GP-GM)	18	16	2	4.78	90.25					
▲ B-20	1.5	Silty, Clayey Sand with Gravel (SC-SM)	27	20	7							
★ B-20	3.0	Well-Graded Gravel with Silty Clay and Sand (GW-GC)	23	18	5	3.55	71.62					
○ B-20	6.2	Well-Graded Gravel with Silt and Sand (GW-GM)	20	17	3	3.93	76.16					
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay			
● B-19	13.7	25	7.62	1.98	0.078	1.4	55.6	34.6	9.8			
☒ B-20	0.8	37.5	6.346	1.461		1.2	48.8	40.8	10.4			
▲ B-20	1.5	25	5.119	0.398		2.9	41.6	45.4	12.9			
★ B-20	3.0	19	6.39	1.423	0.089	1.6	50.1	41.3	8.6			
○ B-20	6.2	25	6.798	1.545	0.089	1.7	52.1	39.4	8.5			



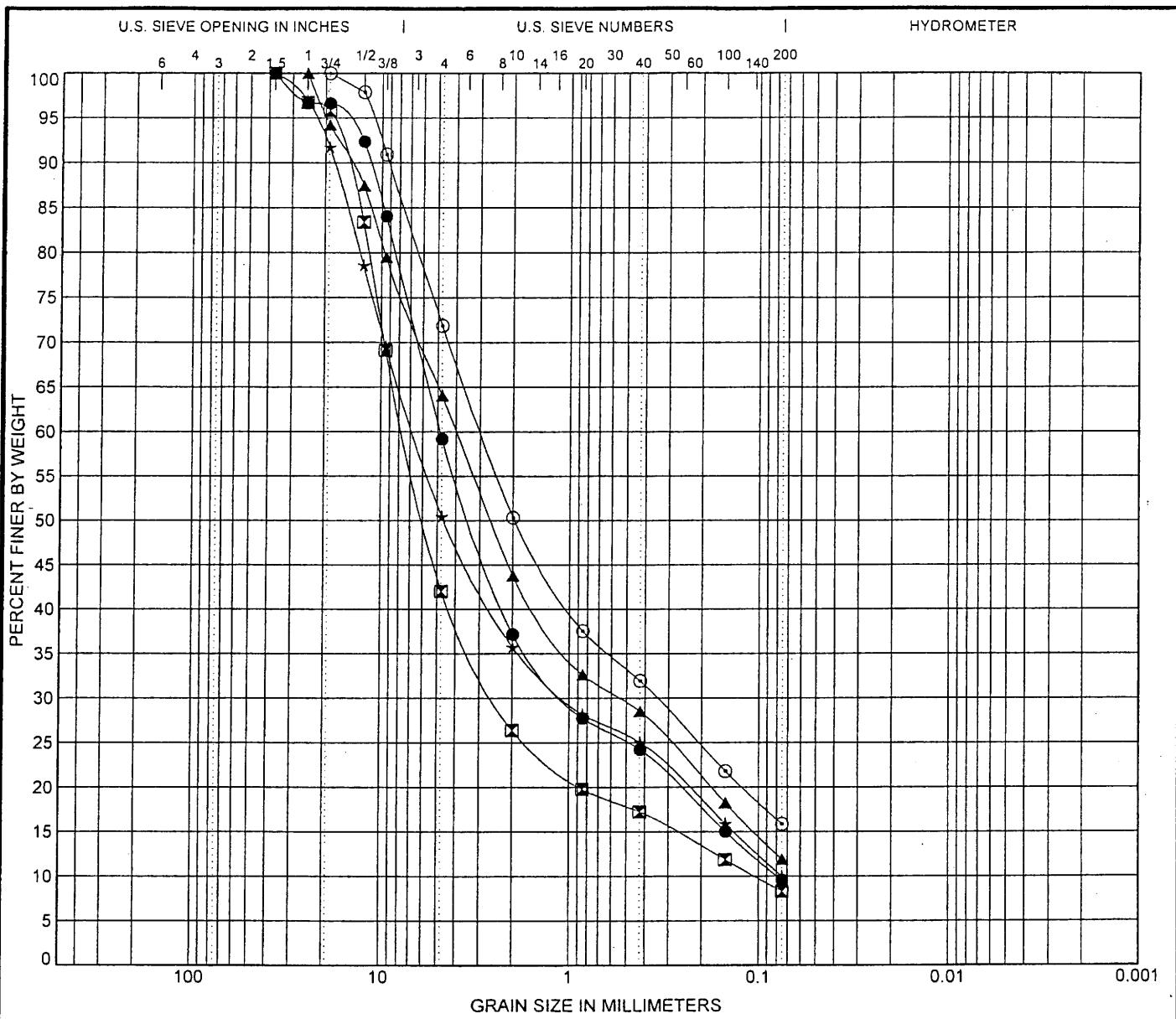


Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification							LL	PL	PI	Cc	Cu	
● B-20	7.0	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)							20	17	3	9.13	45.04
☒ B-21	0.9	POORLY GRADED SAND with SILT and GRAVEL (SP-SM)							NV	NV	NP	0.31	56.81
▲ B-21	1.5	SILTY SAND with GRAVEL (SM)							19	16	3		
★ B-21	3.2	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)							28	18	10	8.31	93.74
○ B-21	4.7	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)							18	5	8.94		67.94

Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-20	7.0	25	7.636	3.438	0.17	1.2	63.9	29.8	6.3
☒ B-21	0.9	25	4.009	0.298		1.0	36.9	52.3	10.8
▲ B-21	1.5	25	3.672	0.323		1.4	34.5	51.6	13.9
★ B-21	3.2	25	7.019	2.09		1.2	56.8	33.2	10.0
○ B-21	4.7	25	7.532	2.732	0.111	0.9	60.8	31.4	7.8



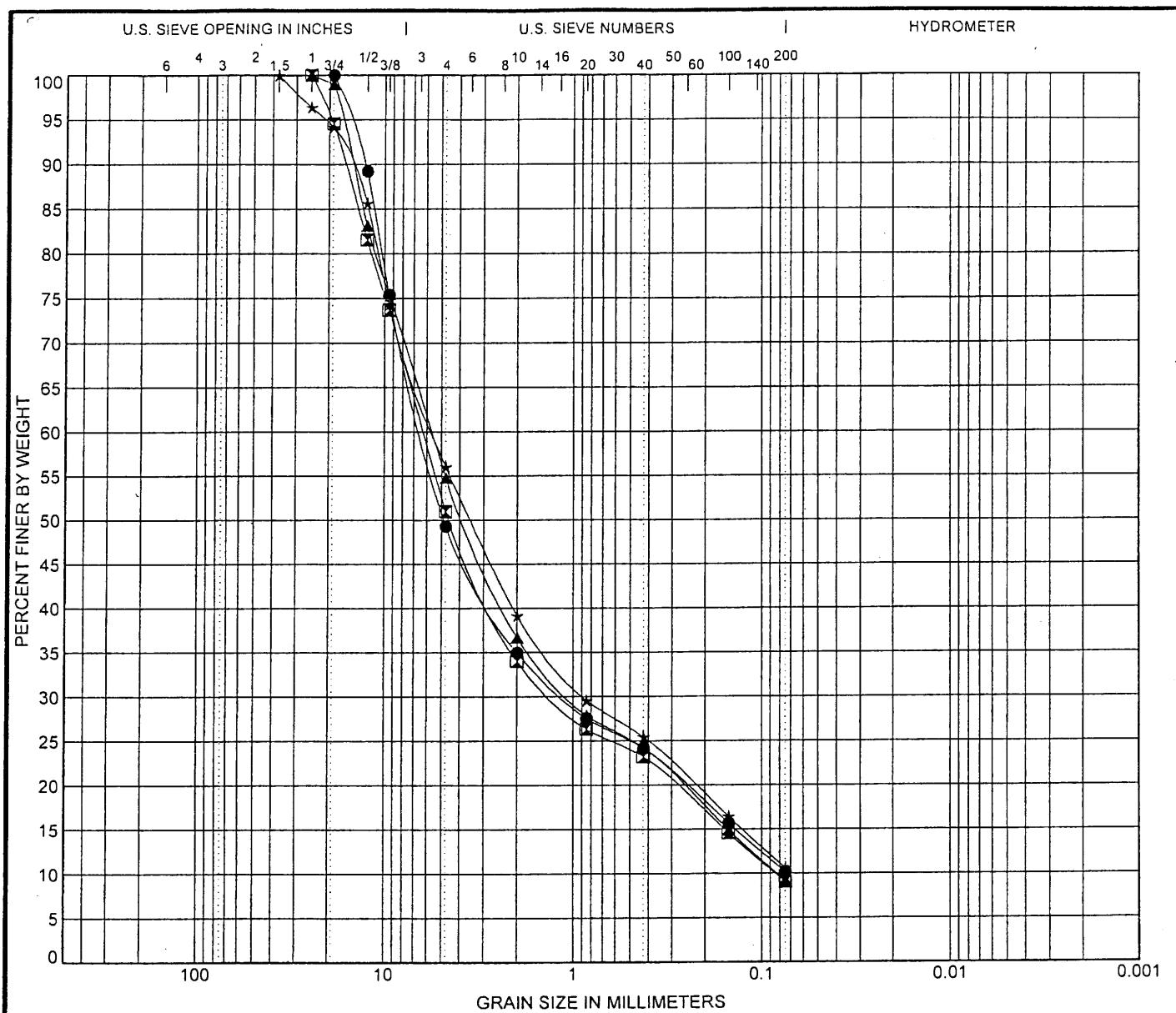


COBBLES	GRAVEL		SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine				
● B-21 6.2	WELL-GRADED SAND with SILT and GRAVEL (SW-SM)	18	17	1	2.83	61.39			

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification	Classification							LL	PL	PI	Cc	Cu
● B-21 6.2	WELL-GRADED SAND with SILT and GRAVEL (SW-SM)							18	17	1	2.83	61.39
☒ B-21 7.8	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)	20						16	4	7.63	72.27	
▲ B-21 9.1	WELL-GRADED SAND with SILT and GRAVEL (SW-SM)							20	17	3	1.22	65.64
★ B-22 0.9	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)							20	18	2	2.17	89.67
○ B-22 1.5	SILTY, CLAYEY SAND with GRAVEL (SC-SM)							21	17	4		
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt		%Clay		
● B-21 6.2	37.5	4.858	1.043	0.079	0.9	40.8	49.6	9.6				
☒ B-21 7.8	37.5	7.526	2.445	0.104	0.8	58.0	33.7	8.3				
▲ B-21 9.1	25	3.998	0.545		1.3	36.0	52.1	11.9				
★ B-22 0.9	37.5	6.714	1.045		1.3	49.5	40.5	10.0				
○ B-22 1.5	19	2.949	0.348		1.2	28.1	56.0	15.9				



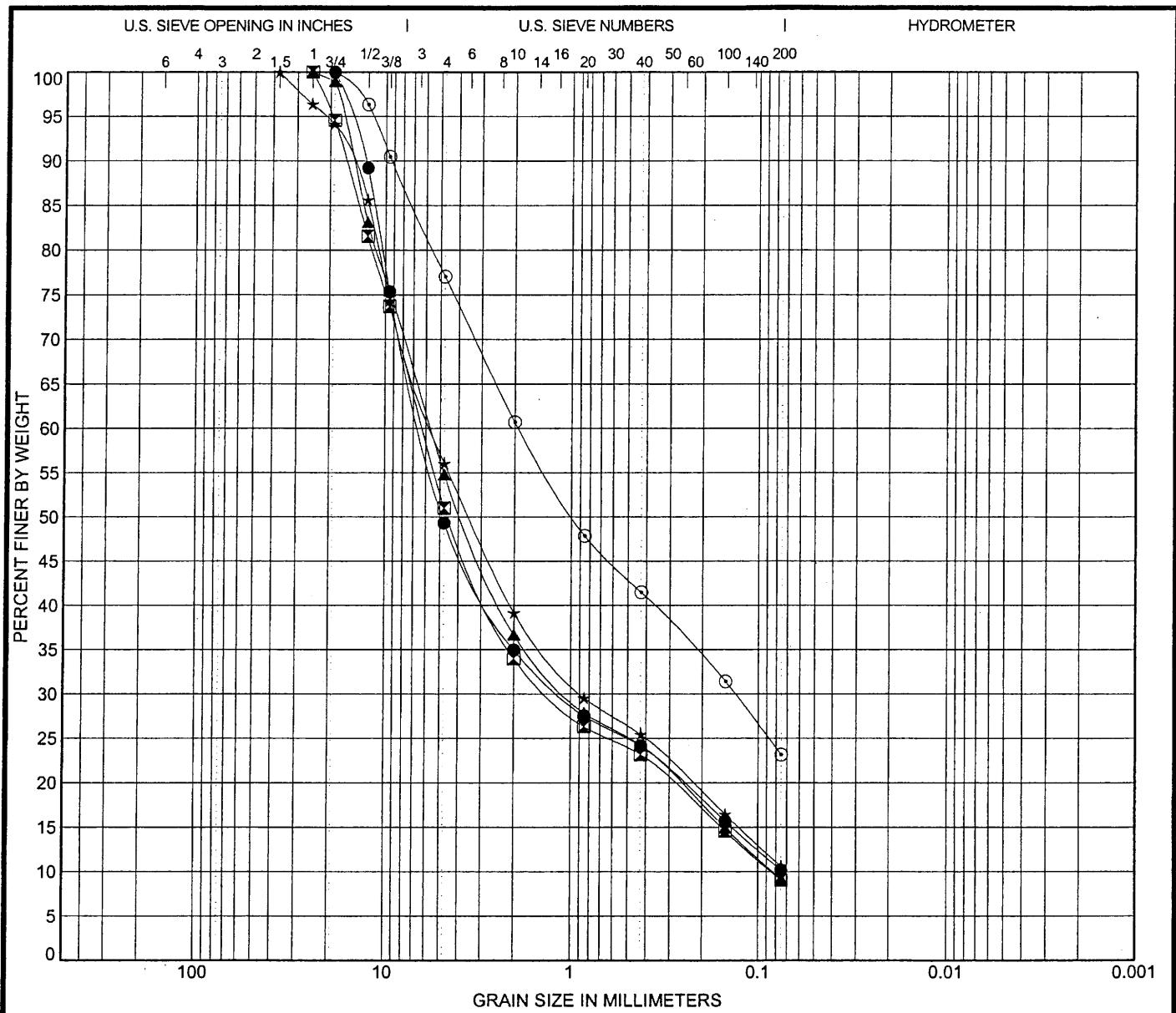


Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification			Classification						LL	PL	PI	Cc	Cu
●	B-22	3.0	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						21	18	3	2.77	86.53
☒	B-22	4.6	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						19	17	2	3.12	74.21
▲	B-22	6.2	WELL-GRADED SAND with SILT and GRAVEL (SW-SM)						19	17	2	2.35	68.74
★	B-22	7.6	WELL-GRADED SAND with SILT and GRAVEL (SW-SM)						19	17	2	2.04	79.45

Specimen Identification			D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-22	3.0	19	6.312	1.129			0.9	50.7	39.1		10.2
☒ B-22	4.6	25	6.256	1.283	0.084	0.8	49.0	41.9			9.1
▲ B-22	6.2	25	5.658	1.045	0.082	1.0	45.2	45.5			9.2
★ B-22	7.6	37.5	5.518	0.884			1.4	44.0	45.4		10.6



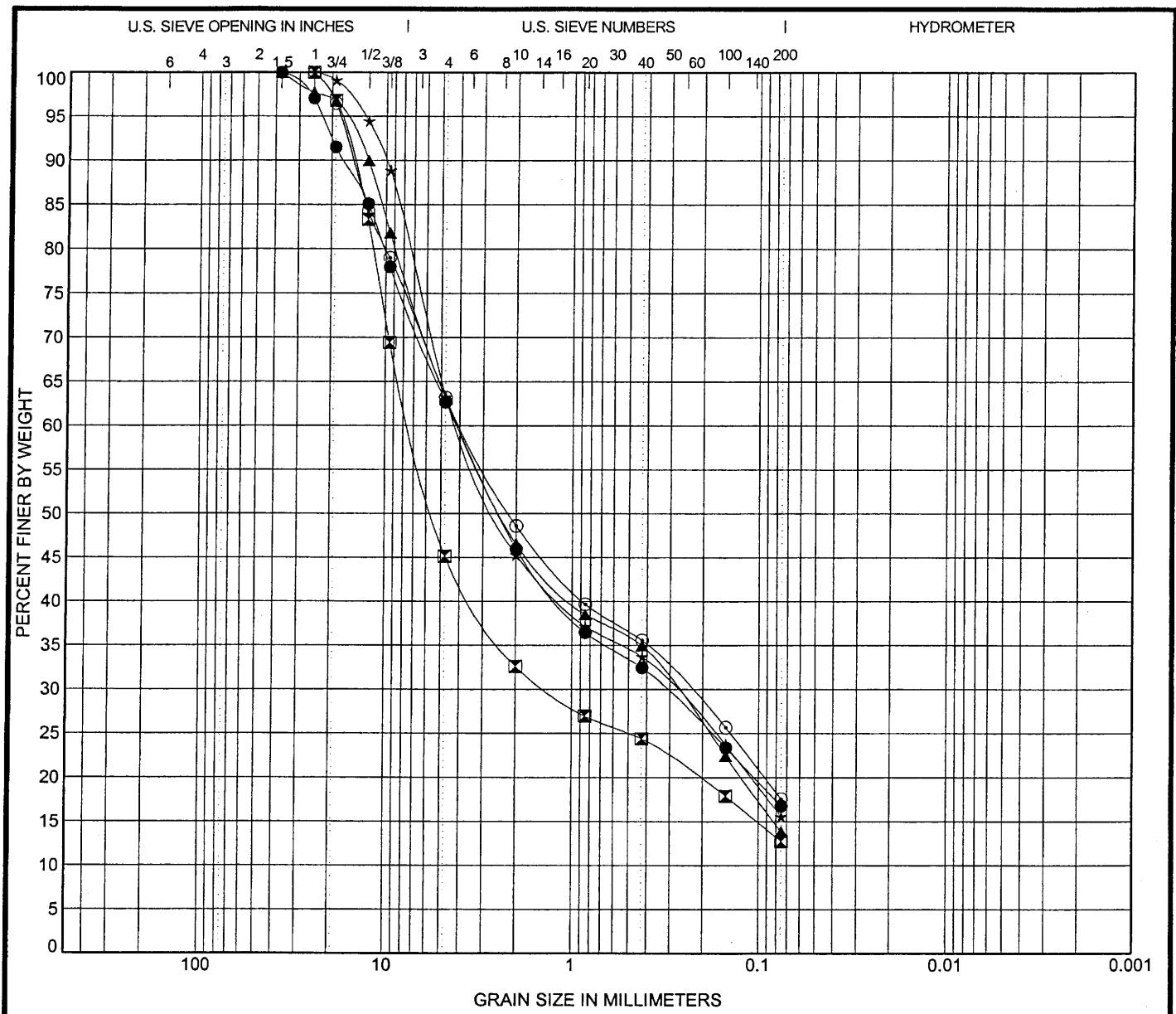


COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Note: NV - No Value, NP - Non Plastic, sample depth in meters.

Specimen Identification			Classification						LL	PL	PI	Cc	Cu
● B-22	3.0		WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						21	18	3	2.77	86.53
☒ B-22	4.6		WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						19	17	2	3.12	74.21
▲ B-22	6.2		WELL-GRADED SAND with SILT and GRAVEL (SW-SM)						19	17	2	2.35	68.74
★ B-22	7.6		WELL-GRADED SAND with SILT and GRAVEL (SW-SM)						19	17	2	2.04	79.45
○ B-40	0.8		CLAYEY SAND with GRAVEL (SC)						37	17	20		
Specimen Identification			D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
● B-22	3.0	19	6.312	1.129			0.9	50.7	39.1		10.2		
☒ B-22	4.6	25	6.256	1.283	0.084		0.8	49.0	41.9		9.1		
▲ B-22	6.2	25	5.658	1.045	0.082		1.0	45.2	45.5		9.2		
★ B-22	7.6	37.5	5.518	0.884			1.4	44.0	45.4		10.6		
○ B-40	0.8	19	1.908	0.133			5.0	23.0	53.9		23.2		





COBBLES	GRAVEL		SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine				

Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-23 5.0'	CLAYEY SAND with GRAVEL (SC)						29	18	11		
☒	B-23 10.0'	CLAYEY GRAVEL with SAND (GC)						32	18	14		
▲	B-23 15.0'	CLAYEY SAND with GRAVEL (SC)						26	16	10		
★	B-23 20.0'	CLAYEY SAND with GRAVEL (SC)						26	16	10		
○	B-23 25.0'	CLAYEY SAND with GRAVEL (SC)						26	17	9		

Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-23 5.0'	37.5	4.134	0.321		4.1	37.3	45.9		16.8
☒	B-23 10.0'	25	7.259	1.349		3.0	54.9	32.4		12.8
▲	B-23 15.0'	37.5	4.055	0.282		3.4	37.0	49.2		13.8
★	B-23 20.0'	25	4.059	0.289		3.4	36.7	47.7		15.6
○	B-23 25.0'	25	3.93	0.237		3.4	36.8	45.7		17.5



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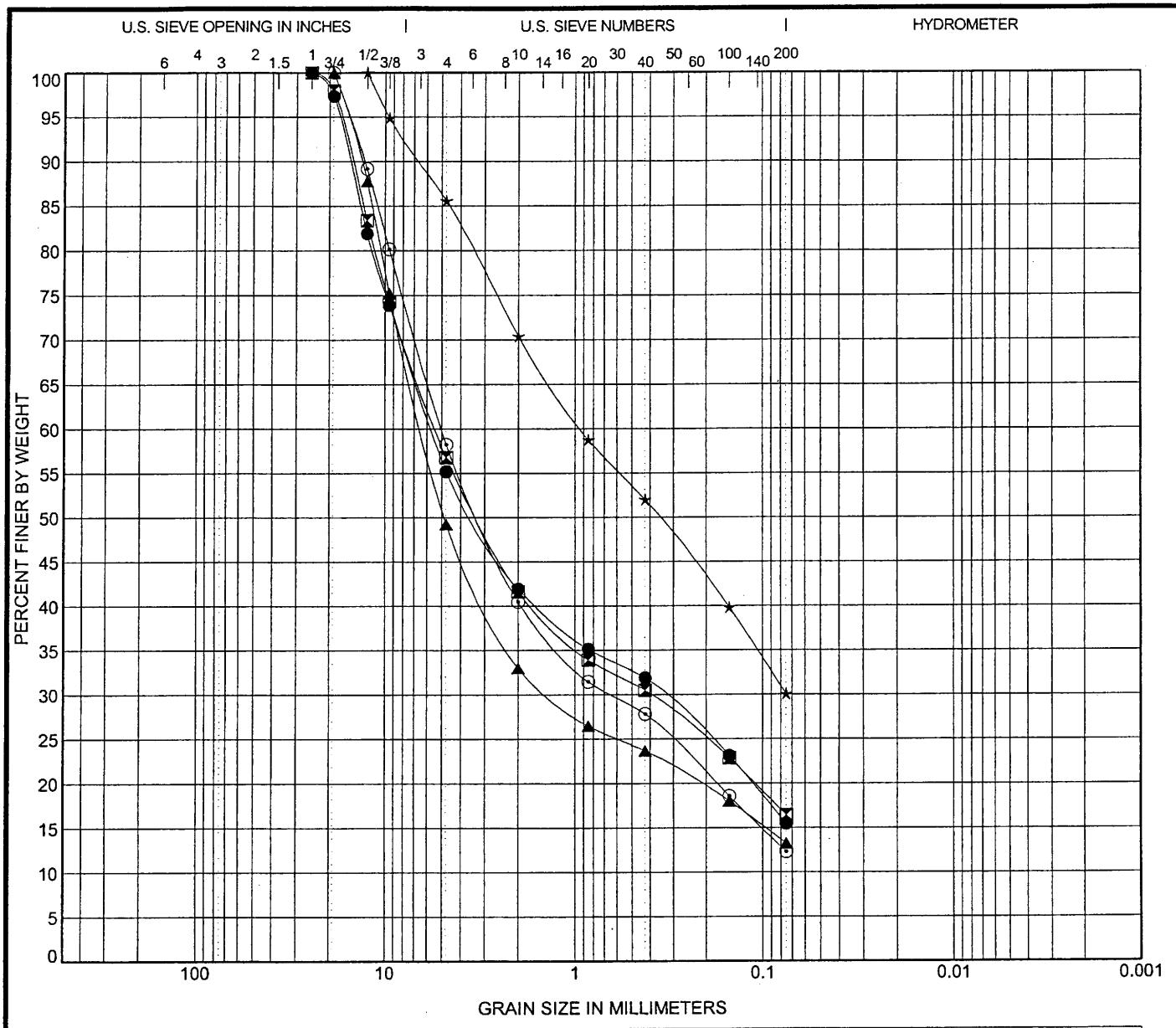
GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Retaining-Sound Walls

Location: Las Vegas, Nevada

Project Number: 0324-01-4

Plate Number: 4a



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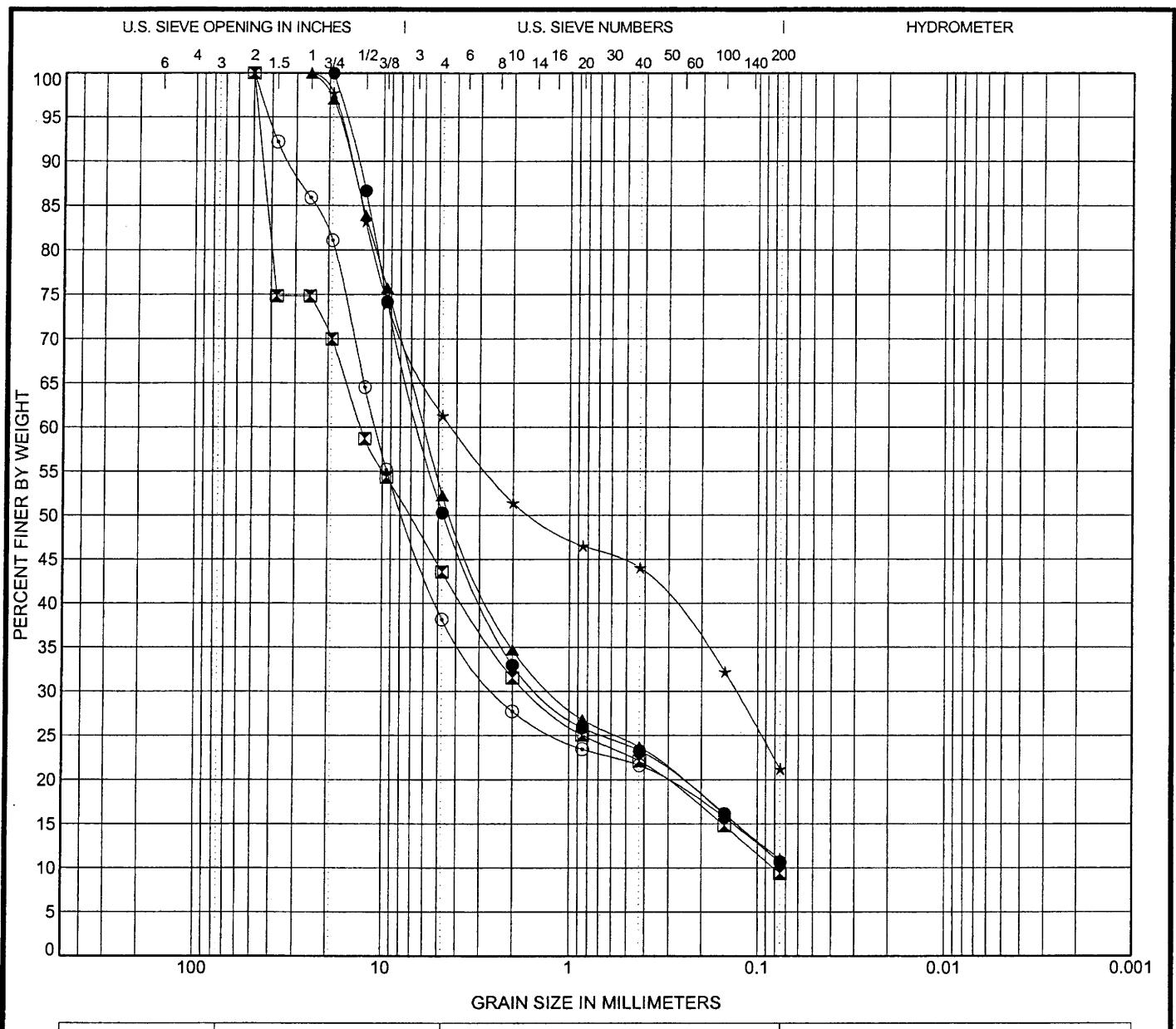
GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Retaining-Sound Wall

Location: Las Vegas, Nevada

Project Number: 0324-01-4

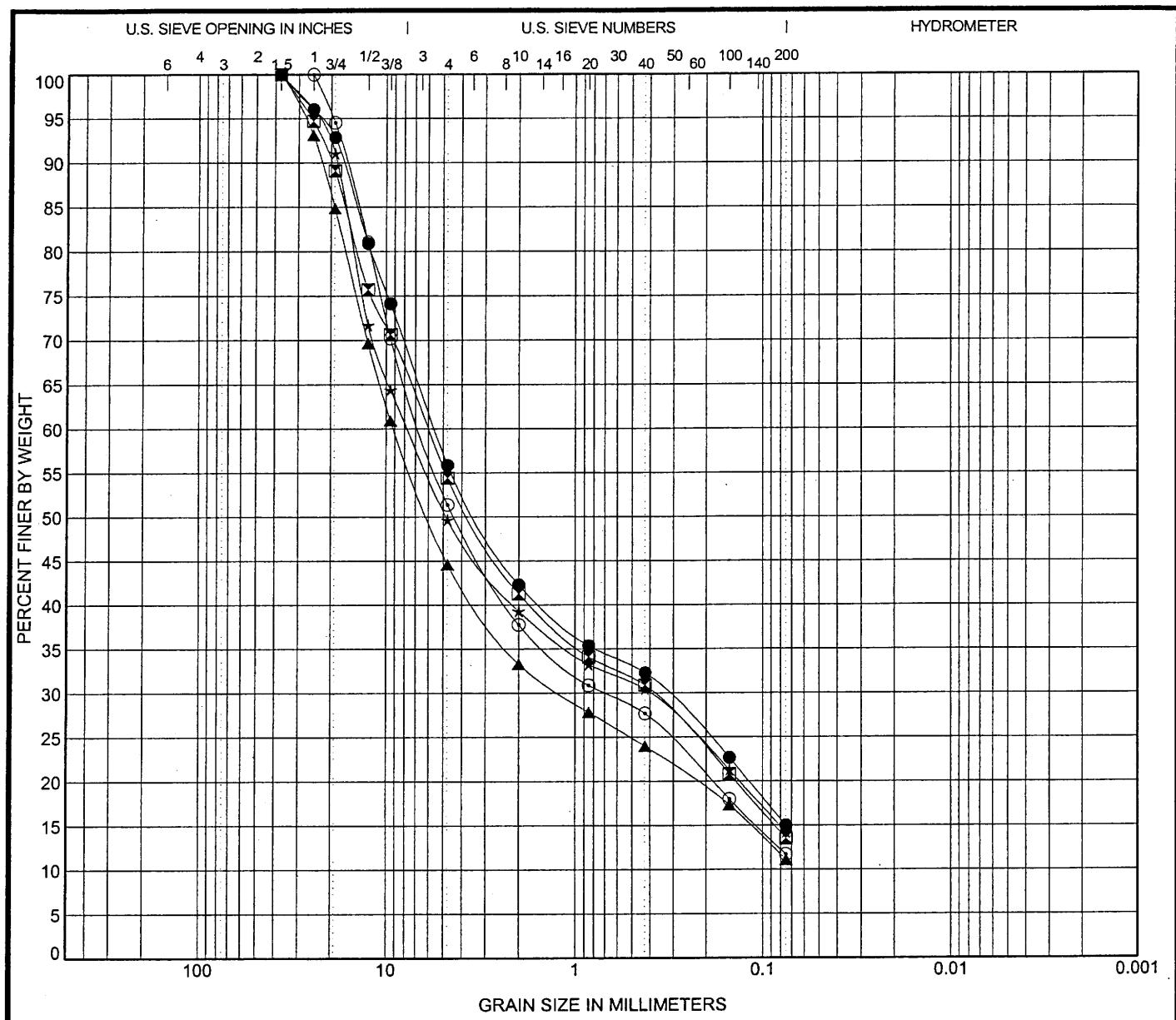
Plate Number: 4b



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
● B-24	10.0'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						30	19	11	4.48	90.92
☒ B-24	15.0'	WELL-GRADED GRAVEL with CLAY and SAND (GW-GC)						28	17	11	2.51	161.83
▲ B-24	19.0'	WELL-GRADED GRAVEL with CLAY and SAND (GW-GC)						28	18	10	3.73	91.85
★ B-25	5.0'	CLAYEY SAND with GRAVEL (SC)						35	19	16		
○ B-25	10.0'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						31	18	13	7.84	160.87
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
● B-24	10.0'	19	6.299	1.399			1.8	49.7	39.6		10.6	
☒ B-24	15.0'	50	13.127	1.634	0.081		1.5	56.4	34.2		9.4	
▲ B-24	19.0'	25	5.974	1.204			1.6	47.8	41.2		11.0	
★ B-25	5.0'	25	4.24	0.131			4.5	38.7	40.1		21.2	
○ B-25	10.0'	50	10.942	2.416			1.9	61.9	27.4		10.7	





COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

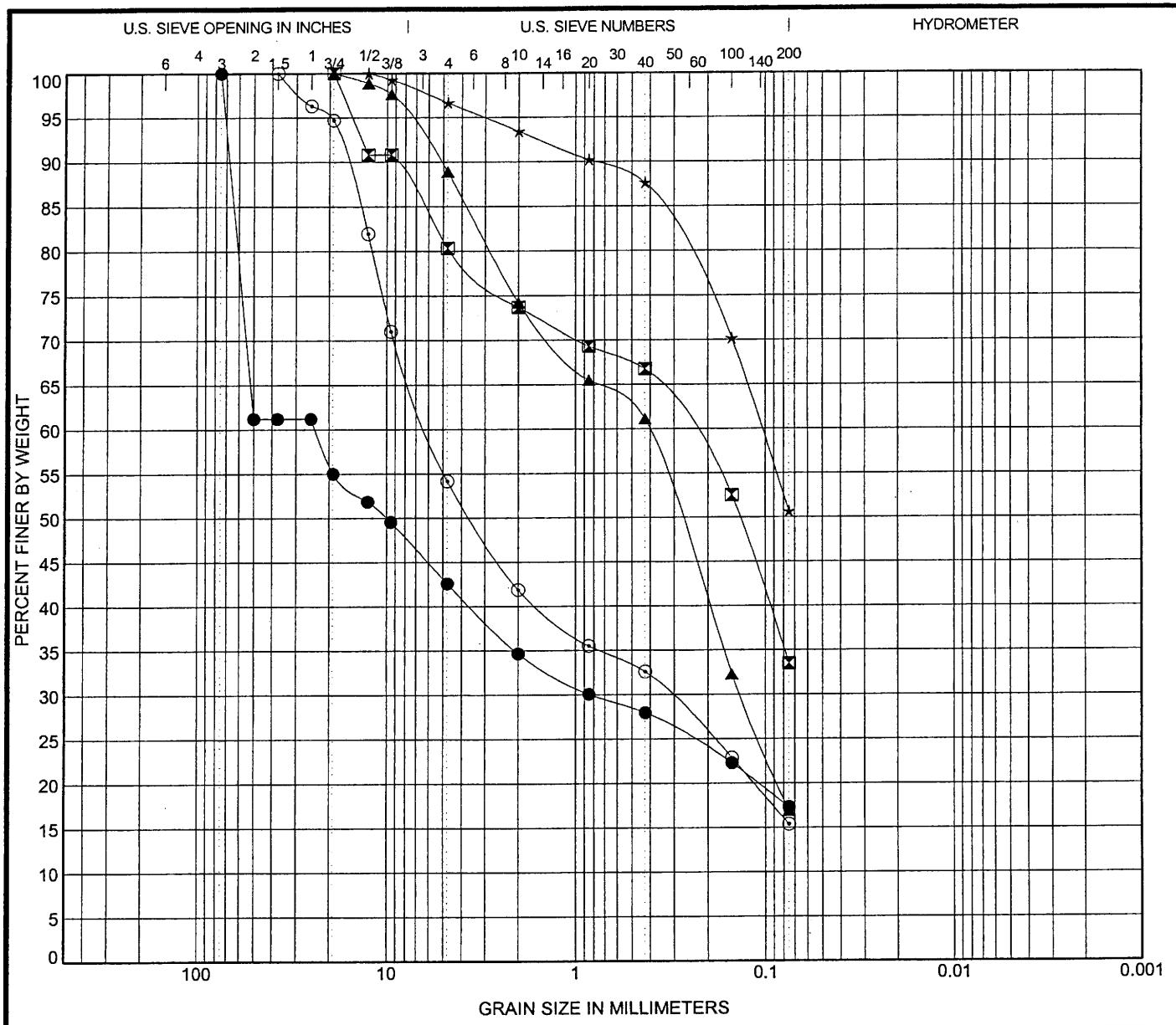
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-25 15.0'	CLAYEY GRAVEL with SAND (GC)						30	17	13		
☒	B-25 19.0'	CLAYEY GRAVEL with SAND (GC)						27	16	11		
▲	B-26 5.0'	WELL-GRADED GRAVEL with CLAY and SAND (GW-GC)						25	17	8	2.37	137.93
★	B-26 10.0'	CLAYEY GRAVEL with SAND (GC)						41	22	19		
○	B-26 15.0'	WELL-GRADED GRAVEL with CLAY and SAND (GW-GC)						28	17	11	1.23	105.44
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-25 15.0'	37.5	5.557	0.332		2.8	44.1	40.9		15.0		
☒	B-25 19.0'	37.5	6.031	0.389		2.4	45.6	40.9		13.5		
▲	B-26 5.0'	37.5	9.135	1.198		2.5	55.4	33.5		11.1		
★	B-26 10.0'	37.5	7.729	0.405		2.7	50.4	35.4		14.2		
○	B-26 15.0'	25	6.525	0.706		1.9	48.6	39.6		11.7		



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Retaining-Sound Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-4 Plate Number: 4d



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-26 20.0'	CLAYEY GRAVEL with SAND (GC)						32	18	14		
▣	B-26 25.0'	CLAYEY SAND with GRAVEL (SC)						55	23	32		
▲	B-26 30.0'	CLAYEY SAND (SC)						32	18	14		
★	B-26 35.0'	SANDY FAT CLAY (CH)						57	23	34		
○	B-28 5.0'	CLAYEY GRAVEL with SAND (GC)						40	23	17		

Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-26 20.0'	75	23.705	0.835		3.4	57.4	25.3		17.3
▣	B-26 25.0'	19	0.26			2.9	19.7	46.8		33.5
▲	B-26 30.0'	19	0.408	0.135		5.0	11.1	72.0		16.9
★	B-26 35.0'	12.5	0.105			16.0	3.3	46.0		50.6
○	B-28 5.0'	37.5	6.039	0.323		3.6	45.8	38.8		15.4



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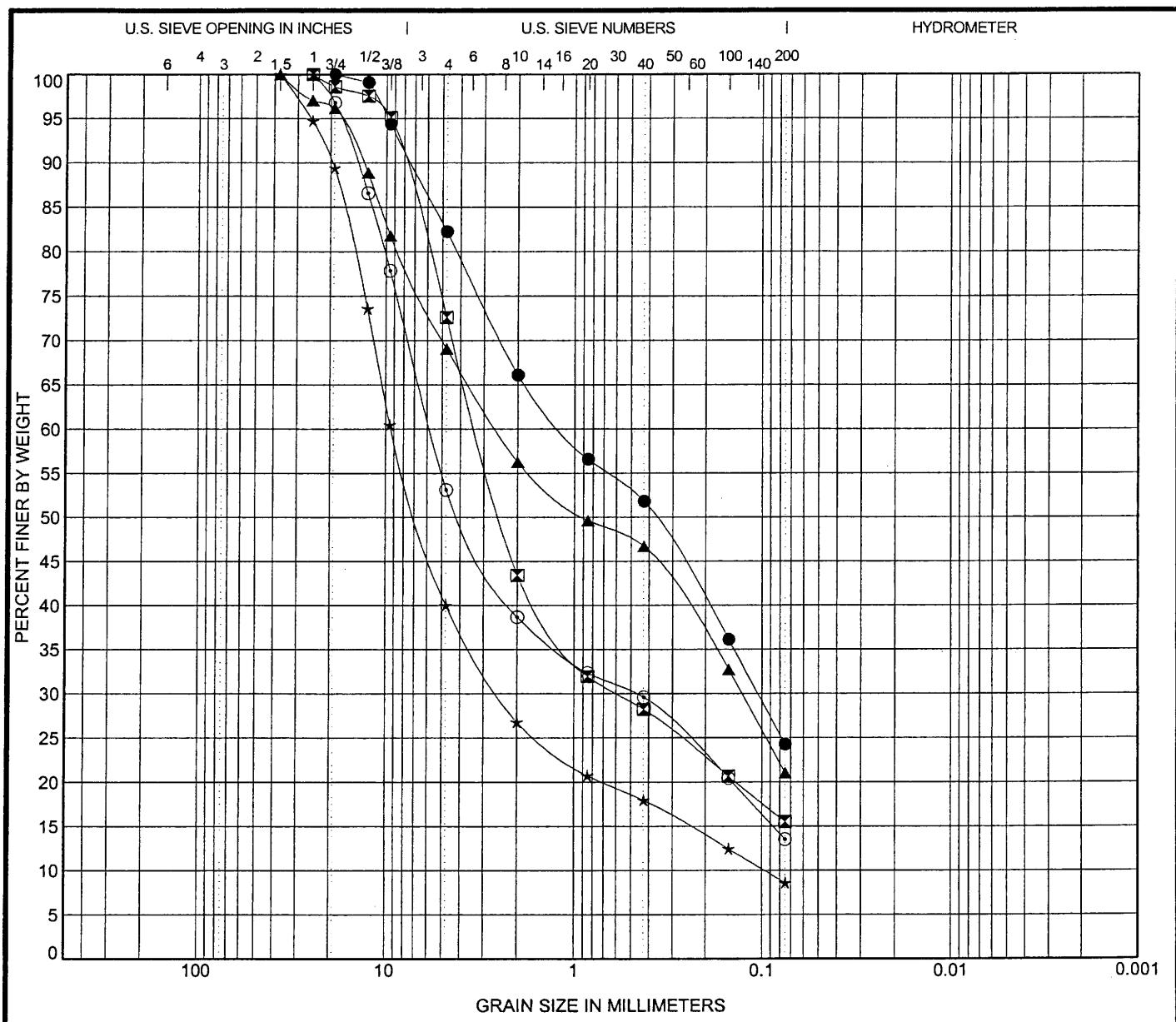
GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Retaining-Sound Walls

Location: Las Vegas, Nevada

Project Number: 0324-01-4

Plate Number: 4e



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

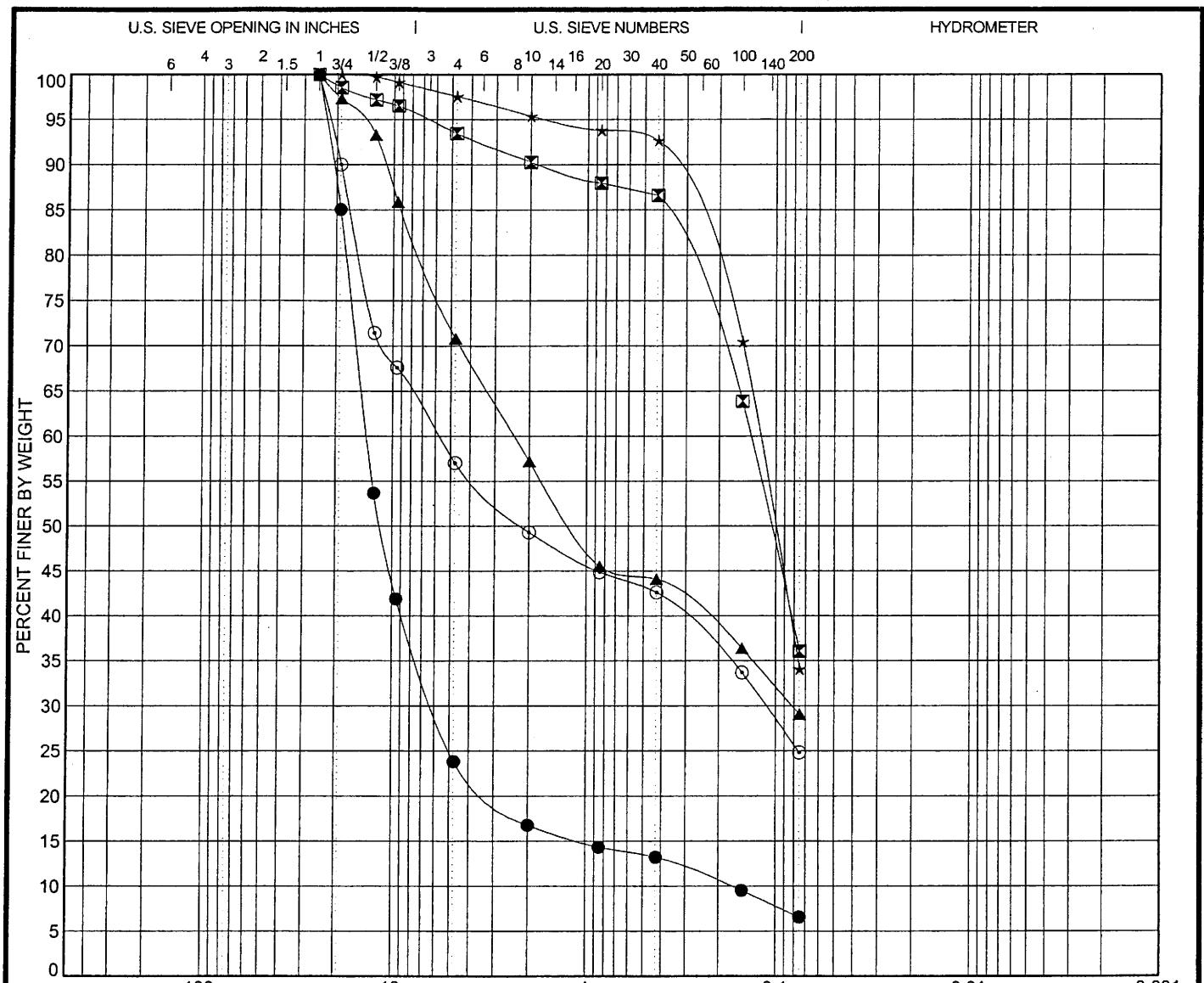
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-28 10.0'	CLAYEY SAND with GRAVEL (SC)						28	15	13		
◻	B-28 15.0'	CLAYEY SAND with GRAVEL (SC)						23	13	10		
▲	B-28 20.0'	CLAYEY SAND with GRAVEL (SC)						31	17	14		
★	B-29 5.0'	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)						23	17	6	6.77	97.02
○	B-29 10.0'	CLAYEY GRAVEL with SAND (GC)						30	15	15		
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-28 10.0'	19	1.156	0.105		5.0	17.7	58.0		24.2		
◻	B-28 15.0'	25	3.271	0.593		2.7	27.4	57.1		15.5		
▲	B-28 20.0'	37.5	2.576	0.128		8.2	30.9	48.0		21.0		
★	B-29 5.0'	37.5	9.351	2.47	0.096	1.4	60.0	31.4		8.6		
○	B-29 10.0'	25	5.762	0.472		3.1	46.9	39.6		13.5		

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GRAIN SIZE DISTRIBUTION

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COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

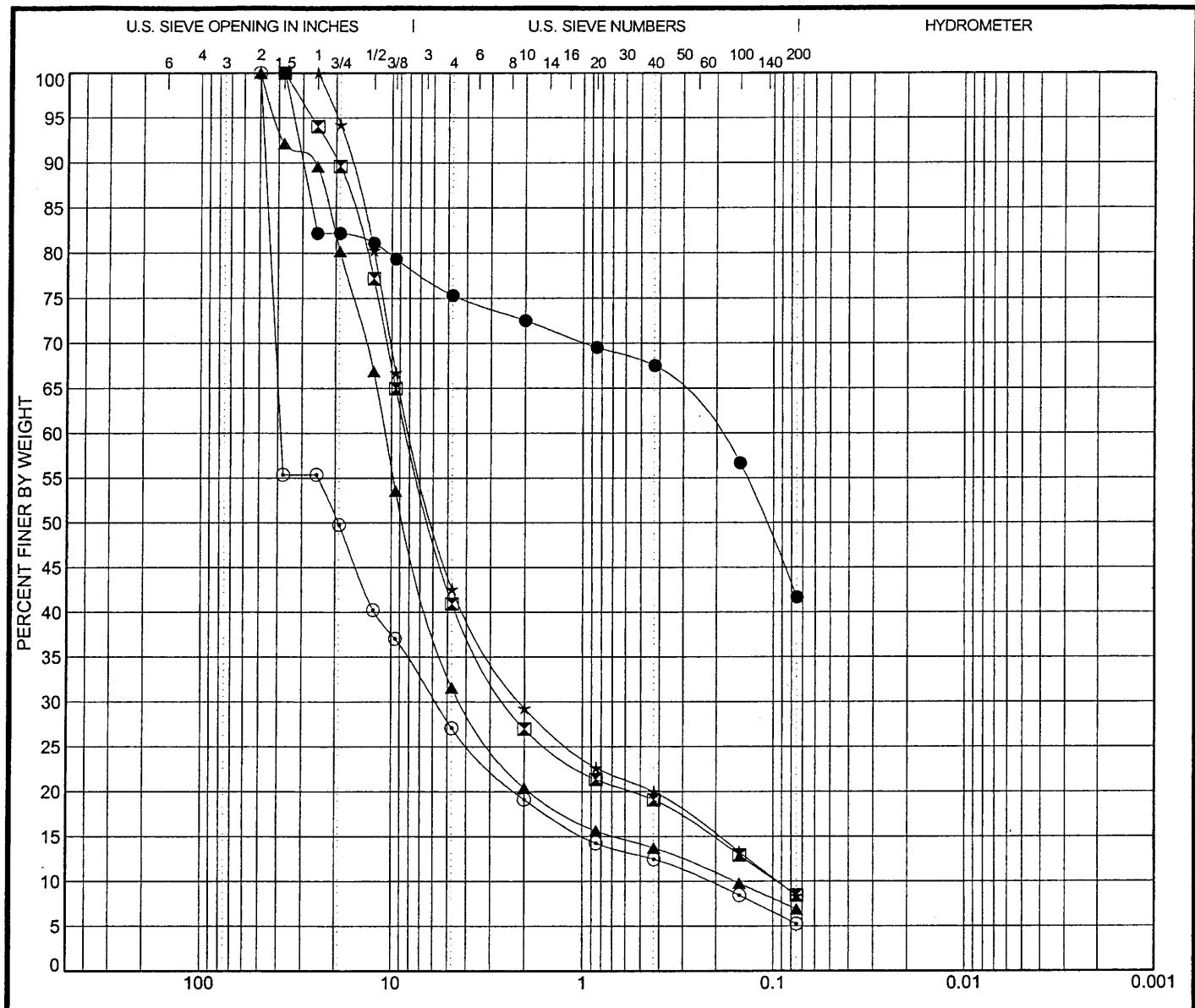
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-29 15.0'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						25	14	11	15.65	79.83
◻	B-29 20.0'	CLAYEY SAND (SC)						26	14	12		
▲	B-29 25.0'	CLAYEY SAND with GRAVEL (SC)						25	13	12		
★	B-29 30.0'	CLAYEY SAND (SC)						40	17	23		
◎	B-29 35.0'	CLAYEY GRAVEL with SAND (GC)						51	16	35		
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-29 15.0'	25	13.602	6.022	0.17	1.2	76.2	17.2		6.6		
◻	B-29 20.0'	25	0.136				12.5	6.5	57.4		36.1	
▲	B-29 25.0'	25	2.39	0.082			5.6	29.2	41.8		29.0	
★	B-29 30.0'	19	0.123				14.0	2.4	63.5		34.1	
◎	B-29 35.0'	25	5.77	0.112			9.4	43.0	32.2		24.8	



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COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

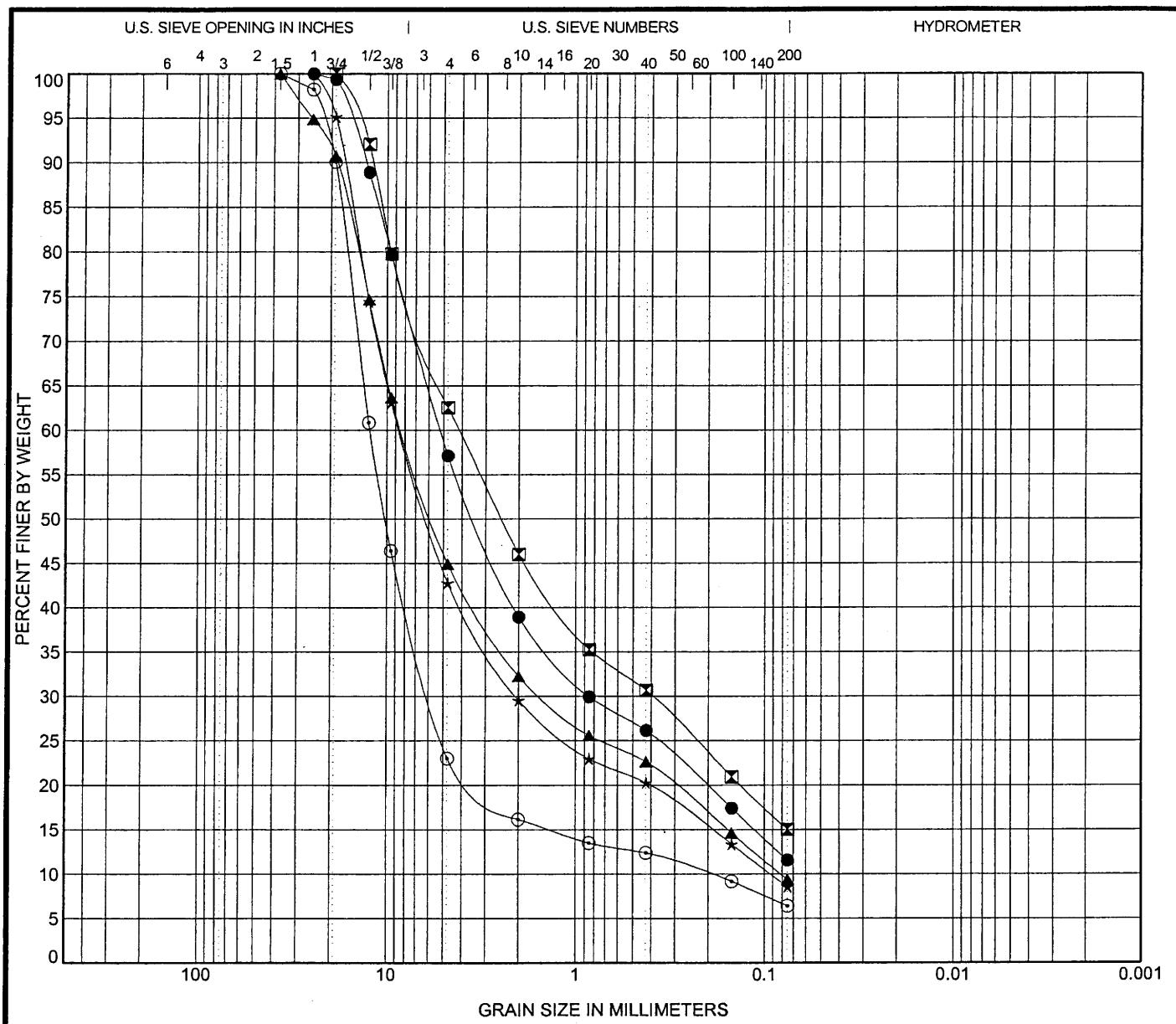
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-29 40.0'	CLAYEY SAND with GRAVEL (SC)						25	11	14		
☒	B-30 5.0'	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)						22	18	4	7.45	86.55
▲	B-30 10.0'	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						21	18	3	10.30	68.39
★	B-30 15.0'	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						19	18	1	5.96	83.15
○	B-30 20.0'	WELL-GRADED GRAVEL with CLAY and SAND (GW-GC)						38	23	15	3.93	172.62
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-29 40.0'	37.5	0.207			7.8	24.7	33.6		41.7		
☒	B-30 5.0'	37.5	8.236	2.416	0.095	1.3	59.1	32.5		8.5		
▲	B-30 10.0'	50	10.846	4.208	0.159	0.6	68.4	24.6		6.9		
★	B-30 15.0'	25	7.829	2.096	0.094	0.9	57.4	34.2		8.4		
○	B-30 20.0'	50	38.637	5.826	0.224	0.8	72.9	21.8		5.3		

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COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-31 5.0'	WELL-GRADED SAND with CLAY and GRAVEL (SW-SC)						29	16	13	2.27	83.43
▣	B-31 10.0'	CLAYEY SAND with GRAVEL (SC)						26	18	8		
▲	B-31 15.0'	WELL-GRADED GRAVEL with SILT and SAND (GW-GM)						18	17	1	3.33	102.30
★	B-31 20.0'	POORLY GRADED GRAVEL with SILT and SAND (GP-GM)						18	17	1	5.40	92.87
○	B-31 25.0'	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)						24	17	7	14.22	62.96
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-31 5.0'	25	5.189	0.856			1.3	42.9	45.6		11.6	
▣	B-31 10.0'	19	4.161	0.396			1.3	37.5	47.5		15.0	
▲	B-31 15.0'	37.5	8.299	1.497	0.081	1.4	55.1	35.5			9.4	
★	B-31 20.0'	25	8.549	2.062	0.092	1.3	57.2	34.2			8.6	
○	B-31 25.0'	37.5	12.299	5.845	0.195	0.7	77.0	16.6			6.4	

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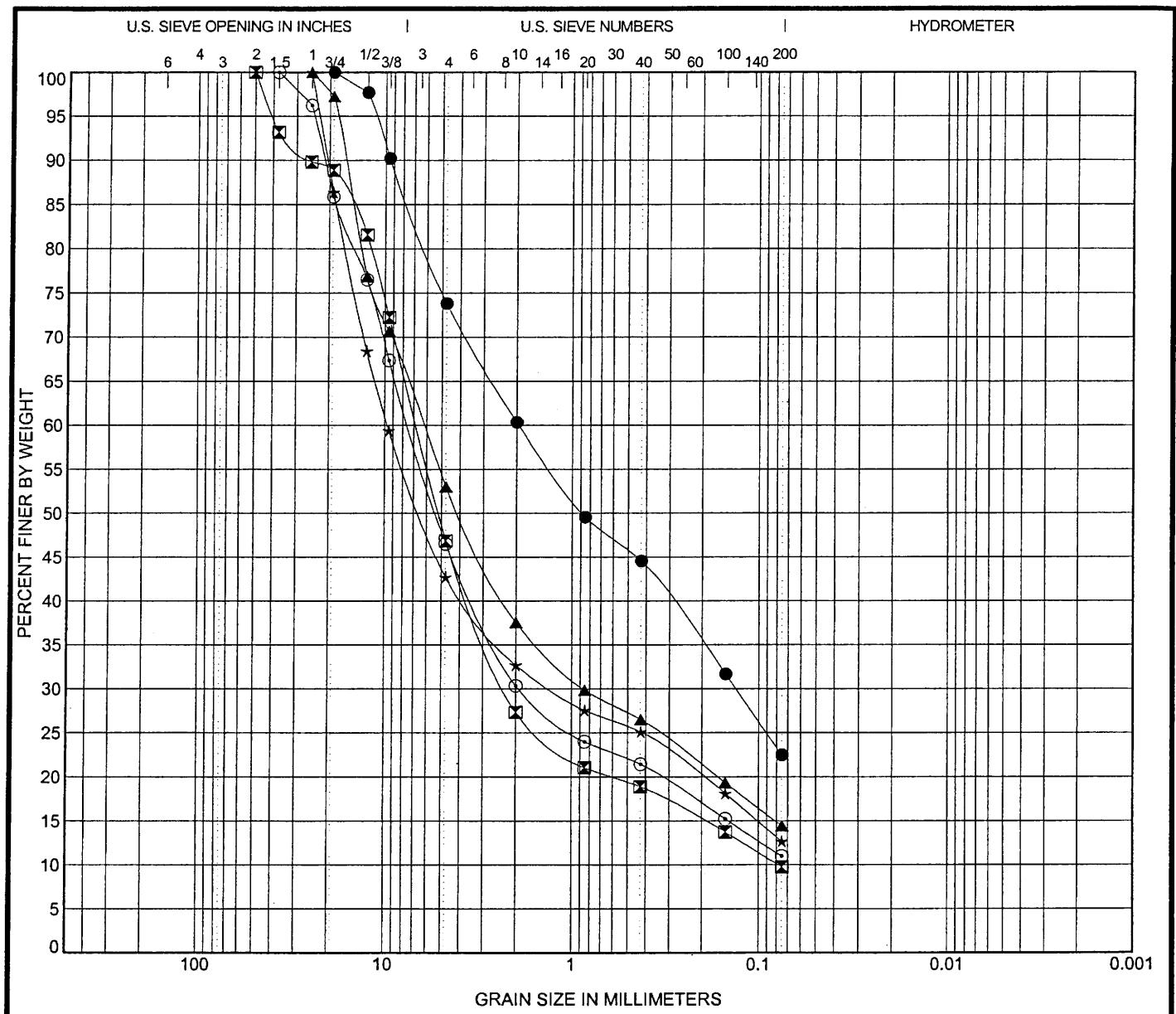
Project: US 95 Widening Project / Retaining-Sound Walls

Location: Las Vegas, Nevada

Project Number: 0324-01-4

Plate Number: 4i





COBBLES	GRAVEL		SAND			SILT OR CLAY			
	coarse	fine	coarse	medium	fine				

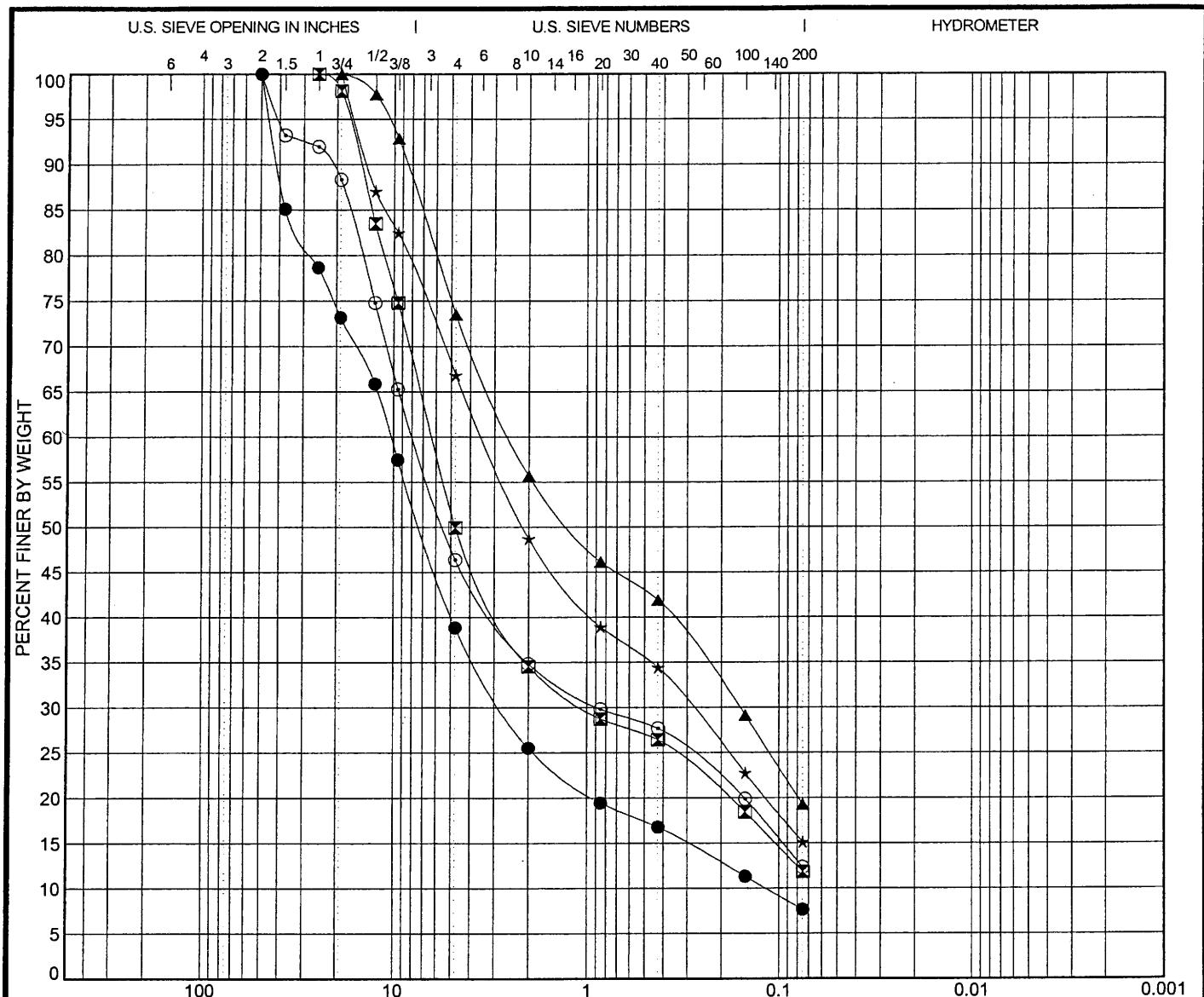
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-31 30.0'	CLAYEY SAND with GRAVEL (SC)						37	23	14		
☒	B-31 35.0'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						26	17	9	9.56	87.14
▲	B-32 5.5'	SILTY, CLAYEY GRAVEL with SAND (GC-GM)						21	15	6		
★	B-32 10.5'	CLAYEY GRAVEL with SAND (GC)						33	19	14		
○	B-32 15.5'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						31	17	14	7.70	116.74
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-31 30.0'	19	1.947	0.132		4.5	26.2	51.3		22.5		
☒	B-31 35.0'	50	6.802	2.253	0.078	2.0	53.2	37.1		9.8		
▲	B-32 5.5'	25	6.249	0.865		2.2	47.0	38.6		14.4		
★	B-32 10.5'	25	9.678	1.277		2.5	57.3	30.0		12.7		
○	B-32 15.5'	37.5	7.438	1.911		2.1	53.5	35.5		11.0		



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GRAIN SIZE DISTRIBUTION

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Plate Number: 4j



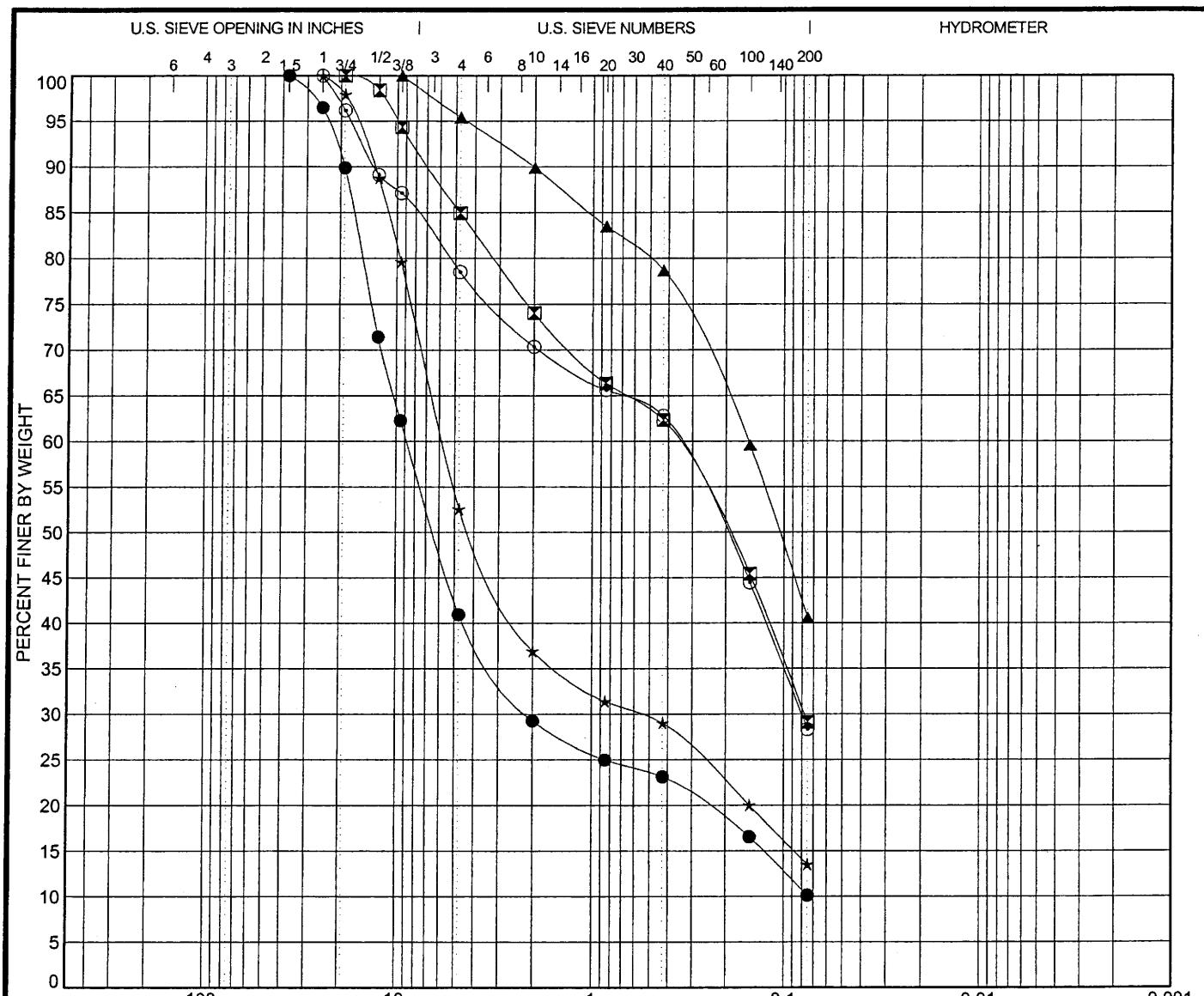
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Retaining-Sound Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-4
Plate Number: 4k



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

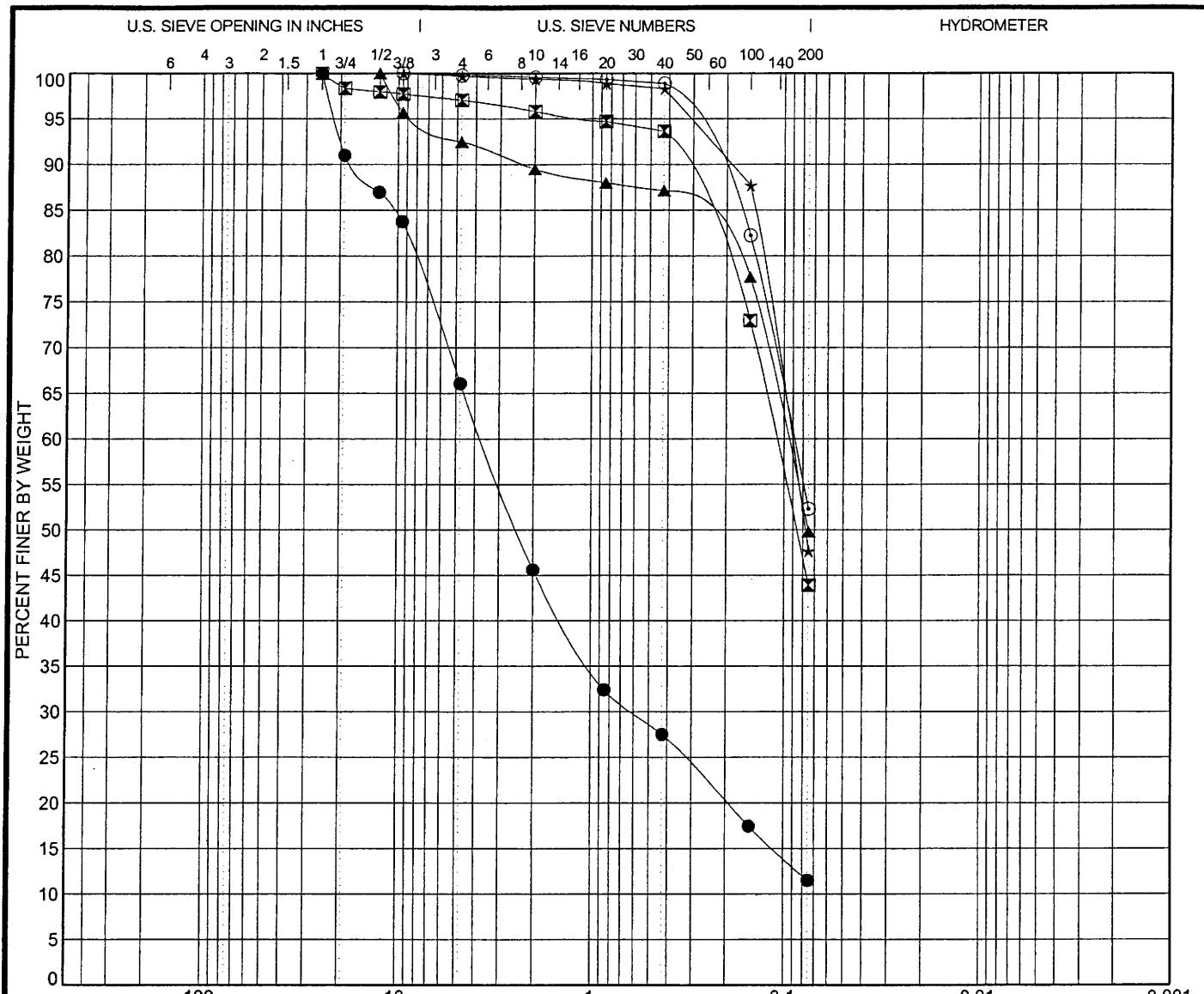
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-33 25.0'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						28	16	12	6.84	119.38
☒	B-33 30.0'	CLAYEY SAND with GRAVEL (SC)						48	19	29		
▲	B-33 35.0'	CLAYEY SAND (SC)						46	21	25		
★	B-34 5.5'	CLAYEY GRAVEL with SAND (GC)						28	18	10		
○	B-34 10.0'	CLAYEY SAND with GRAVEL (SC)						35	19	16		
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-33 25.0'	37.5	8.821	2.112		2.1	59.1	30.8		10.1		
☒	B-33 30.0'	19	0.369	0.078		7.0	15.1	55.8		29.1		
▲	B-33 35.0'	9.5	0.153			10.4	4.6	54.8		40.6		
★	B-34 5.5'	25	5.748	0.566		4.7	47.4	39.0		13.5		
○	B-34 10.0'	25	0.363	0.081		11.4	21.5	50.2		28.3		



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Retaining-Sound Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-4 Plate Number: 41



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-34 15.0'	WELL-GRADED SAND with SILT and GRAVEL (SW-SM)						NP	NP	NP	1.59	58.41
■	B-34 20.0'	CLAYEY SAND (SC)						32	16	16		
▲	B-34 25.0'	CLAYEY SAND (SC)						52	17	35		
*	B-34 30.0'	CLAYEY SAND (SC)						38	22	16		
○	B-34 35.0'	SANDY FAT CLAY (CH)						65	16	49		

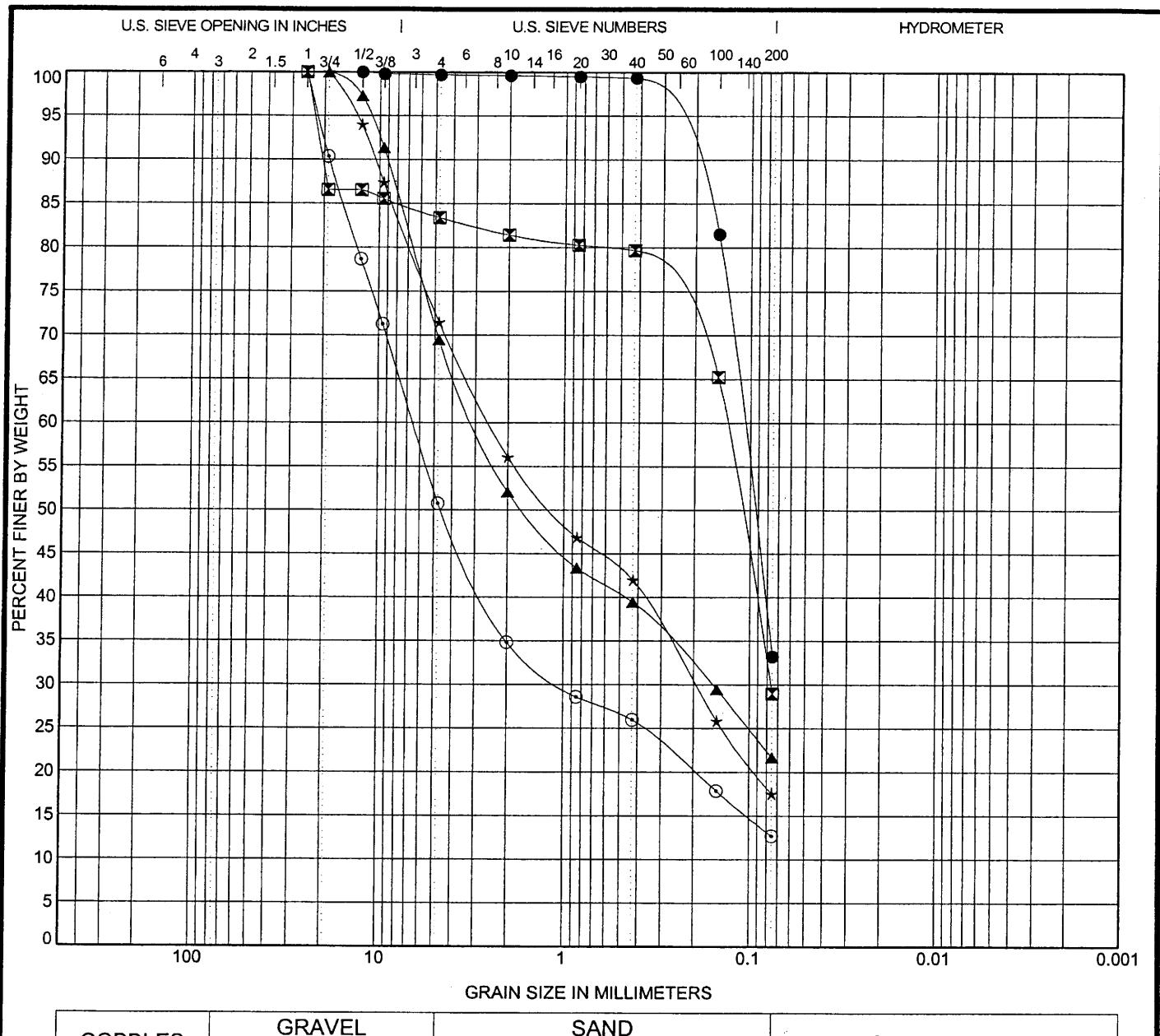
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-34 15.0'	25	3.675	0.606		3.6	33.9	54.6		11.5
■	B-34 20.0'	25	0.11			14.5	2.9	53.2		43.9
▲	B-34 25.0'	12.5	0.097			18.9	7.5	42.7		49.8
*	B-34 30.0'	9.5	0.093			15.5	0.3	52.0		47.6
○	B-34 35.0'	9.5	0.09			19.0	0.2	47.5		52.3



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Retaining-Sound Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-4
Plate Number: 4m



Specimen Identification	USCS Classification							LL	PL	PI	Cc	Cu
● B-34 40.0'	CLAYEY SAND (SC)							35	21	14		
☒ B-34 45.0'	CLAYEY SAND with GRAVEL (SC)							36	20	16		
▲ B-35 5.5'	CLAYEY SAND with GRAVEL (SC)							37	19	18		
★ B-35 10.0'	CLAYEY SAND with GRAVEL (SC)							29	16	13		
○ B-35 15.5'	CLAYEY GRAVEL with SAND (GC)							32	16	16		

Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-34 40.0'	12.5	0.11			15.6	0.3	66.5		33.2
☒ B-34 45.0'	25	0.136	0.077		13.0	16.6	54.4		29.0
▲ B-35 5.5'	19	2.966	0.159		5.0	30.5	47.8		21.7
★ B-35 10.0'	19	2.495	0.196		4.3	28.5	54.0		17.5
○ B-35 15.5'	25	6.495	1.035		2.9	49.3	38.0		12.7

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GRAIN SIZE DISTRIBUTION

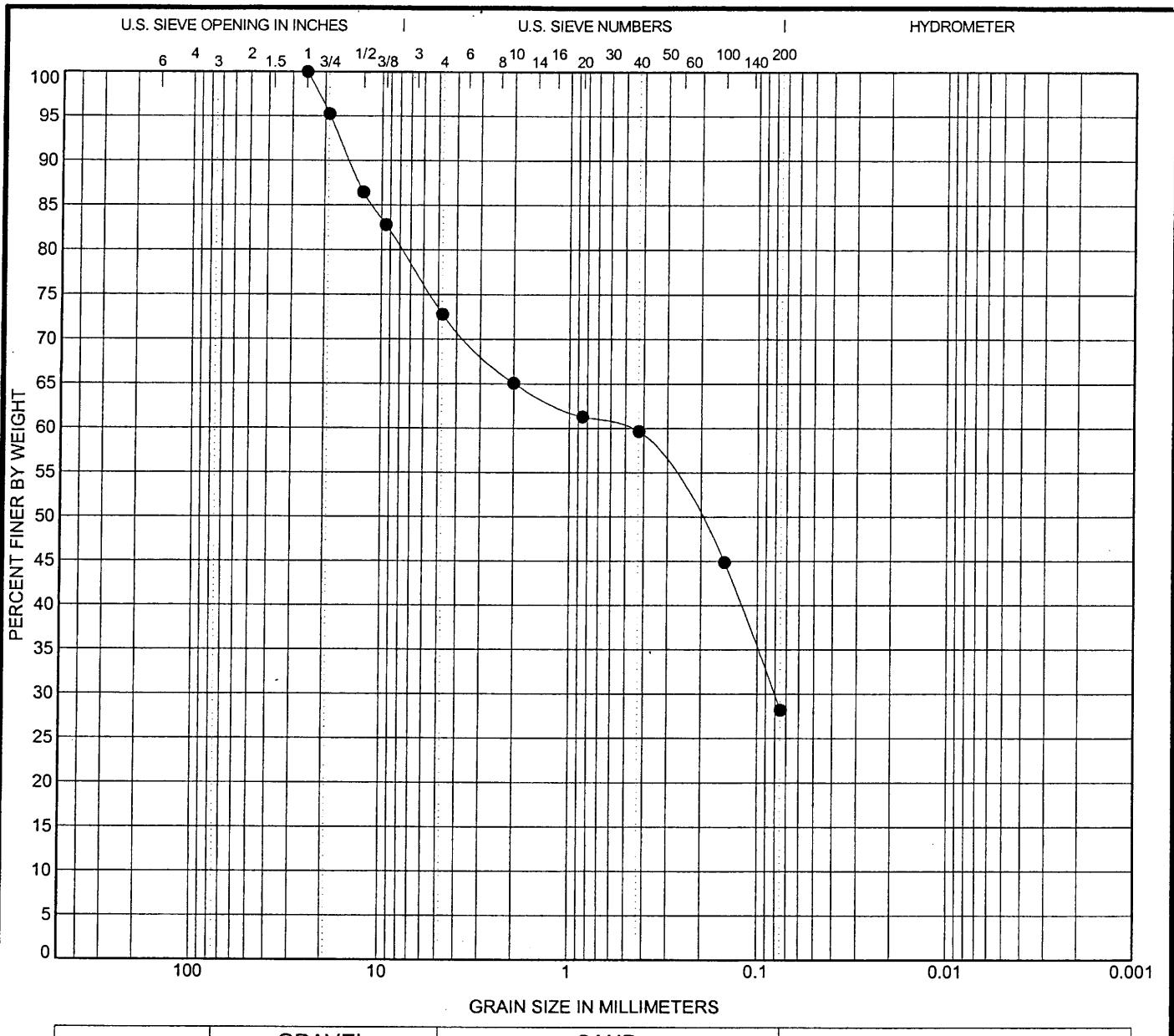
Project: US 95 Widening Project / Retaining-Sound Walls

Location: Las Vegas, Nevada

Project Number: 0324-01-4

Plate Number: 4n





COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
● B-35	20.0'	CLAYEY SAND with GRAVEL (SC)						30	14	16		

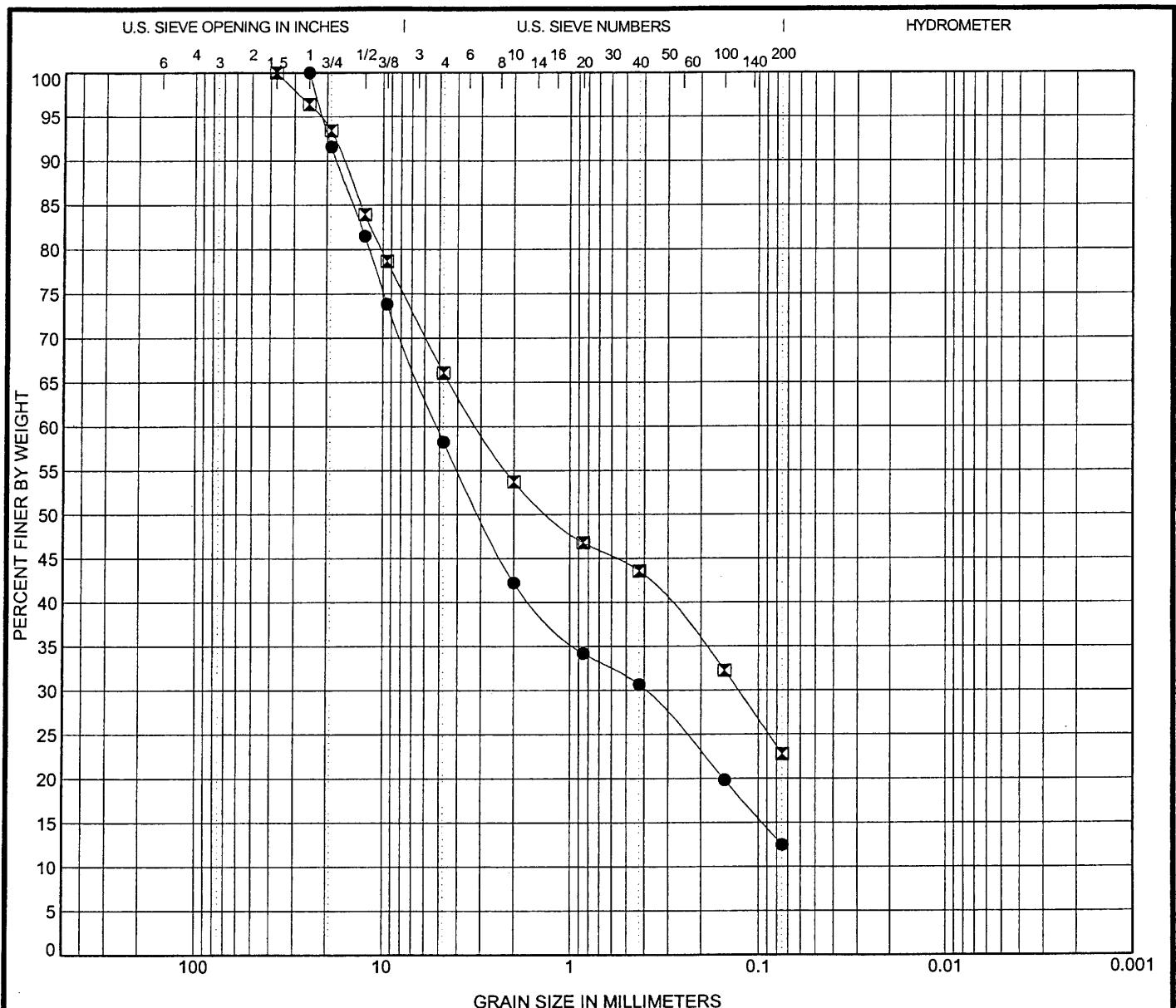
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-35	20.0'	25	0.491	0.081		9.0	27.2	44.6	28.2	



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Retaining-Sound Walls
Location: Las Vegas, Nevada
Project Number: 0324-01-4 Plate Number: 4o



Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-36 5.0'	CLAYEY SAND with GRAVEL (SC)						27	18	9	0.52	86.48
☒	B-37 4.0'	CLAYEY SAND with GRAVEL (SC)						26	15	11		

Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-36 5.0'	25	5.136	0.399		5.7	41.8	45.8		12.5
☒	B-37 4.0'	37.5	3.102	0.127		5.6	33.9	43.4		22.7



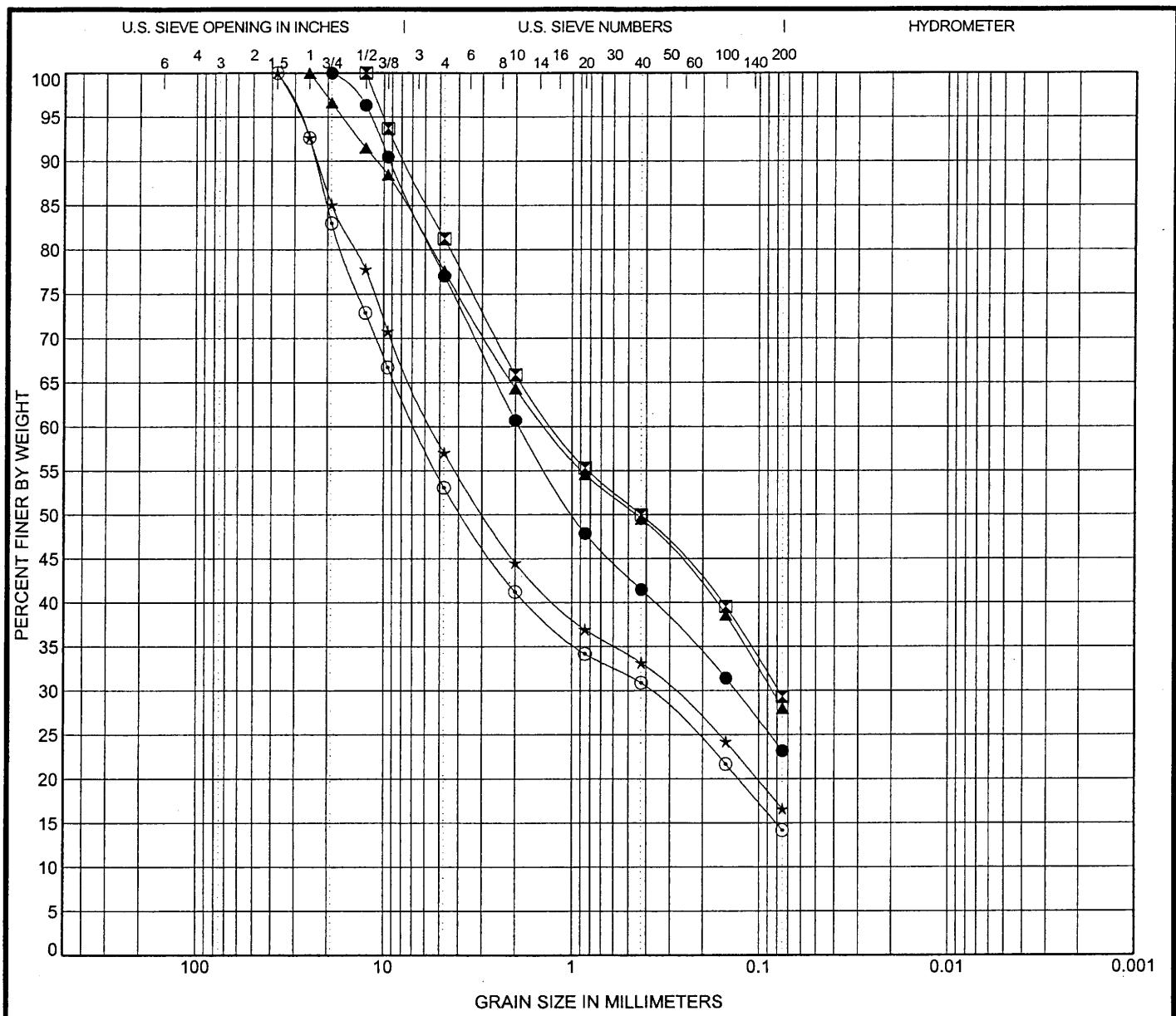
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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Rainbow Bridge

Location: Las Vegas, Nevada

Project Number: Plate Number:



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-40 2.5'	CLAYEY SAND with GRAVEL (SC)						37	17	20		
☒	B-40 5.0'	CLAYEY SAND with GRAVEL (SC)						41	18	23		
▲	B-40 7.5'	CLAYEY SAND with GRAVEL (SC)						41	18	23		
★	B-40 10.0'	CLAYEY GRAVEL with SAND (GC)						29	16	13		
○	B-40 12.5'	CLAYEY GRAVEL with SAND (GC)						26	17	9		

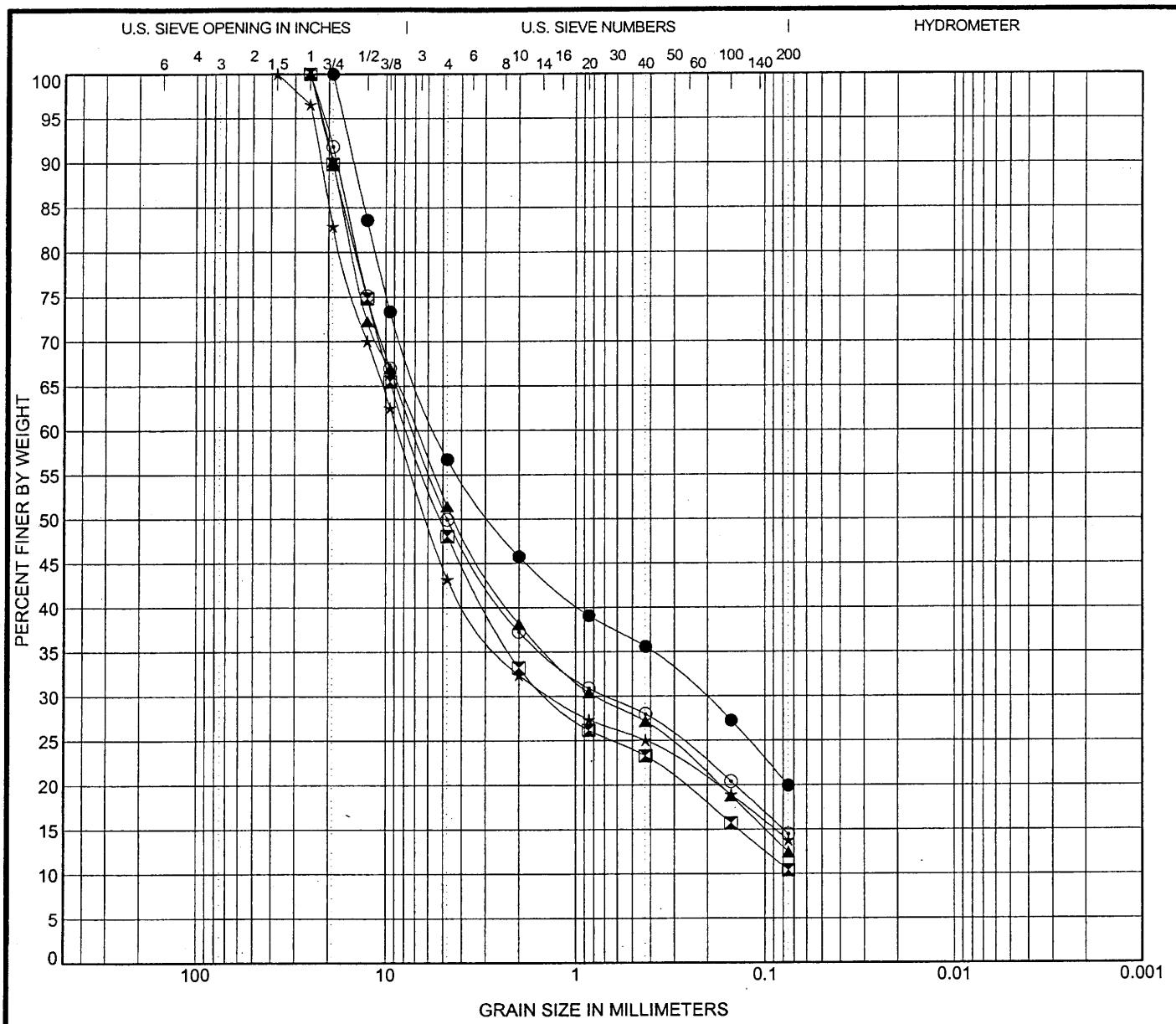
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-40 2.5'	19	1.908	0.133		5.0	23.0	53.9		23.2
☒	B-40 5.0'	12.5	1.243	0.079		7.4	18.8	52.0		29.3
▲	B-40 7.5'	25	1.368	0.086		7.6	22.4	49.6		28.0
★	B-40 10.0'	37.5	5.513	0.295		4.3	43.0	40.5		16.6
○	B-40 12.5'	37.5	6.754	0.385		2.4	46.9	38.9		14.2



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Washington Avenue Bridge
Location: Las Vegas, Nevada
Project Number: 0324-01-6 Plate Number: 4a



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Specimen Identification		USCS Classification					LL	PL	PI	Cc	Cu
●	B-40 17.5'	CLAYEY GRAVEL with SAND (GC)					30	12	18		
▣	B-40 20.0'	WELL-GRADED GRAVEL with SILTY CLAY and SAND (GW-GC)					22	17	5	3.37	107.28
▲	B-40 22.5'	SILTY, CLAYEY GRAVEL with SAND (GC-GM)					23	16	7	1.53	121.06
★	B-40 25.0'	CLAYEY GRAVEL with SAND (GC)					28	15	13		
○	B-40 27.5'	CLAYEY GRAVEL with SAND (GC)					25	15	10		

Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-40 17.5'	19	5.446	0.212		3.8	43.3	36.8		19.9
▣	B-40 20.0'	25	7.636	1.353		2.0	51.9	37.7		10.4
▲	B-40 22.5'	25	6.957	0.782		1.9	48.6	39.0		12.4
★	B-40 25.0'	37.5	8.675	1.331		2.3	56.8	29.4		13.8
○	B-40 27.5'	25	7.149	0.69		2.5	50.1	35.5		14.5

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GRAIN SIZE DISTRIBUTION

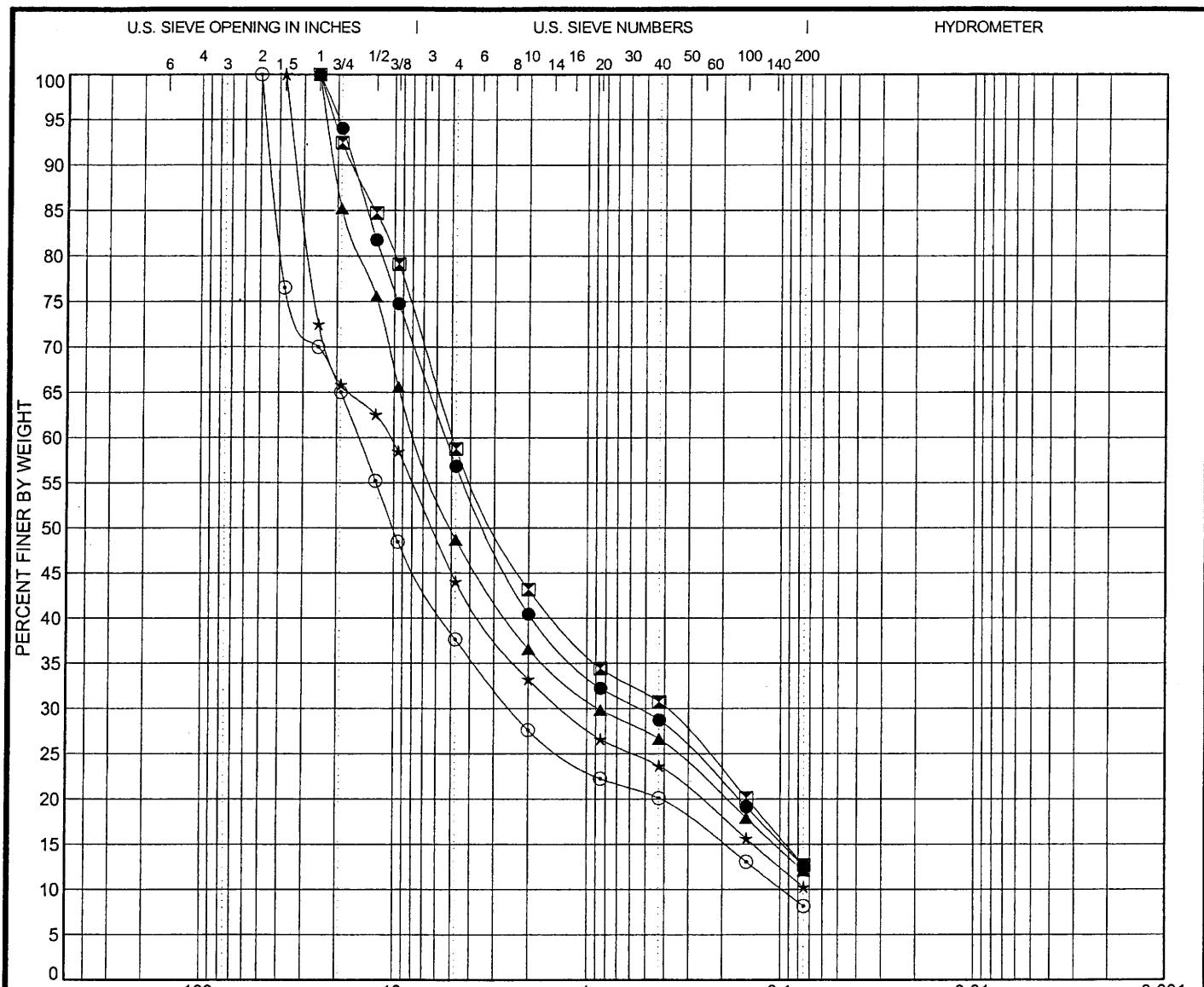
Project: US 95 Widening Project / Washington Avenue Bridge

Location: Las Vegas, Nevada

Project Number: 0324-01-6

Plate Number: 4b





COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

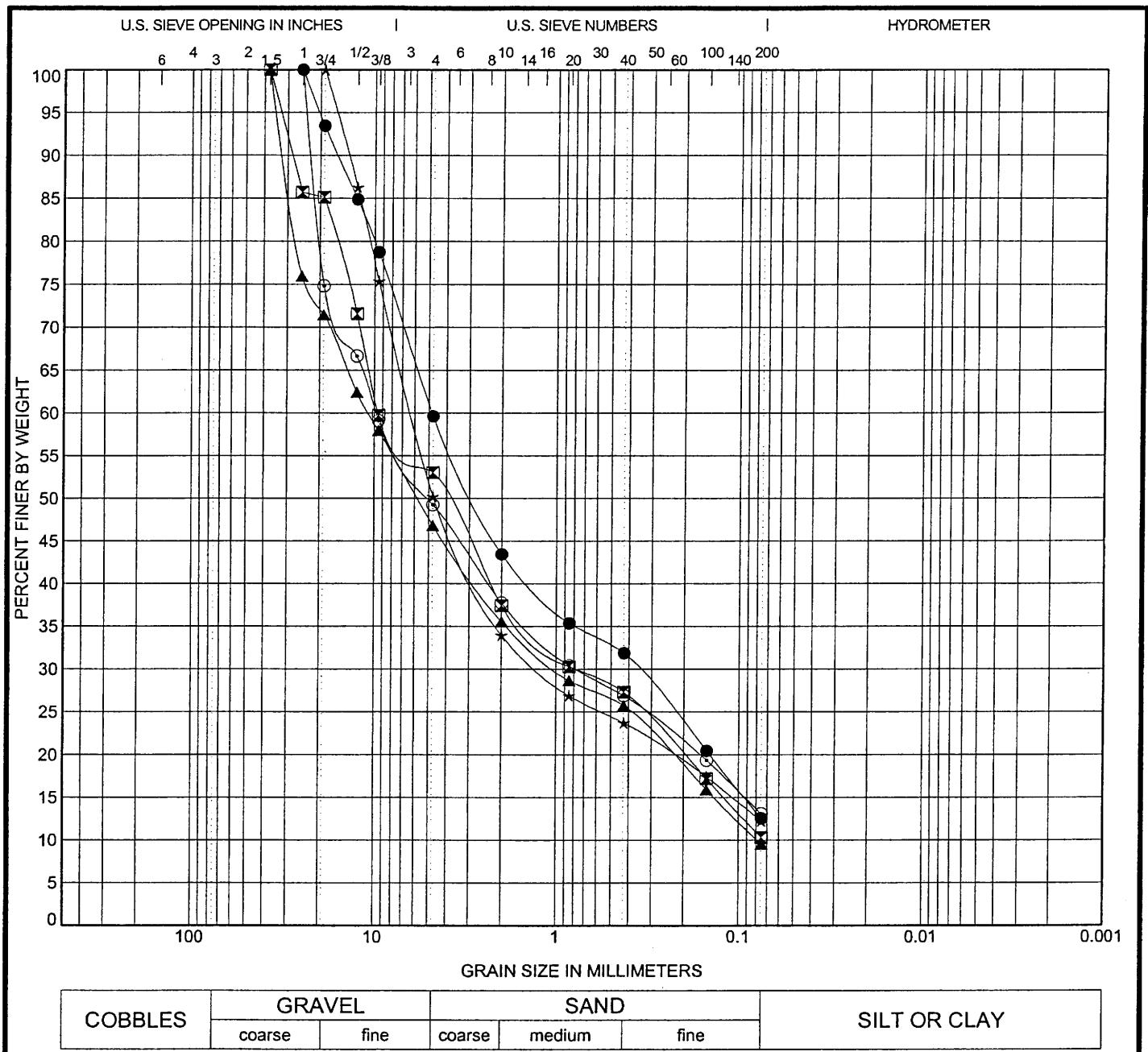
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-41 2.5'	CLAYEY SAND with GRAVEL (SC)						28	18	10		
◻	B-41 5.0'	SILTY, CLAYEY SAND with GRAVEL (SC-SM)						28	21	7		
▲	B-41 7.5'	CLAYEY GRAVEL with SAND (GC)						28	18	10	1.69	128.55
★	B-41 10.0'	WELL-GRADED GRAVEL with CLAY and SAND (GW-GC)						27	18	9	2.28	145.45
○	B-41 12.5'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						27	19	8	4.06	158.02
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-41 2.5'	25	5.367	0.547			3.8	43.2	44.2		12.6	
◻	B-41 5.0'	25	4.956	0.396			4.2	41.2	46.0		12.7	
▲	B-41 7.5'	25	7.553	0.867			3.6	51.3	36.6		12.1	
★	B-41 10.0'	37.5	10.529	1.318			3.2	55.9	33.8		10.3	
○	B-41 12.5'	50	15.334	2.458	0.097	3.3	62.4	29.5			8.2	



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Washington Avenue Bridge
Location: Las Vegas, Nevada
Project Number: 0324-01-6 Plate Number: 4c



US GRAIN SIZE2 0324016.GPJ US LAB.GDT 11/22/2002



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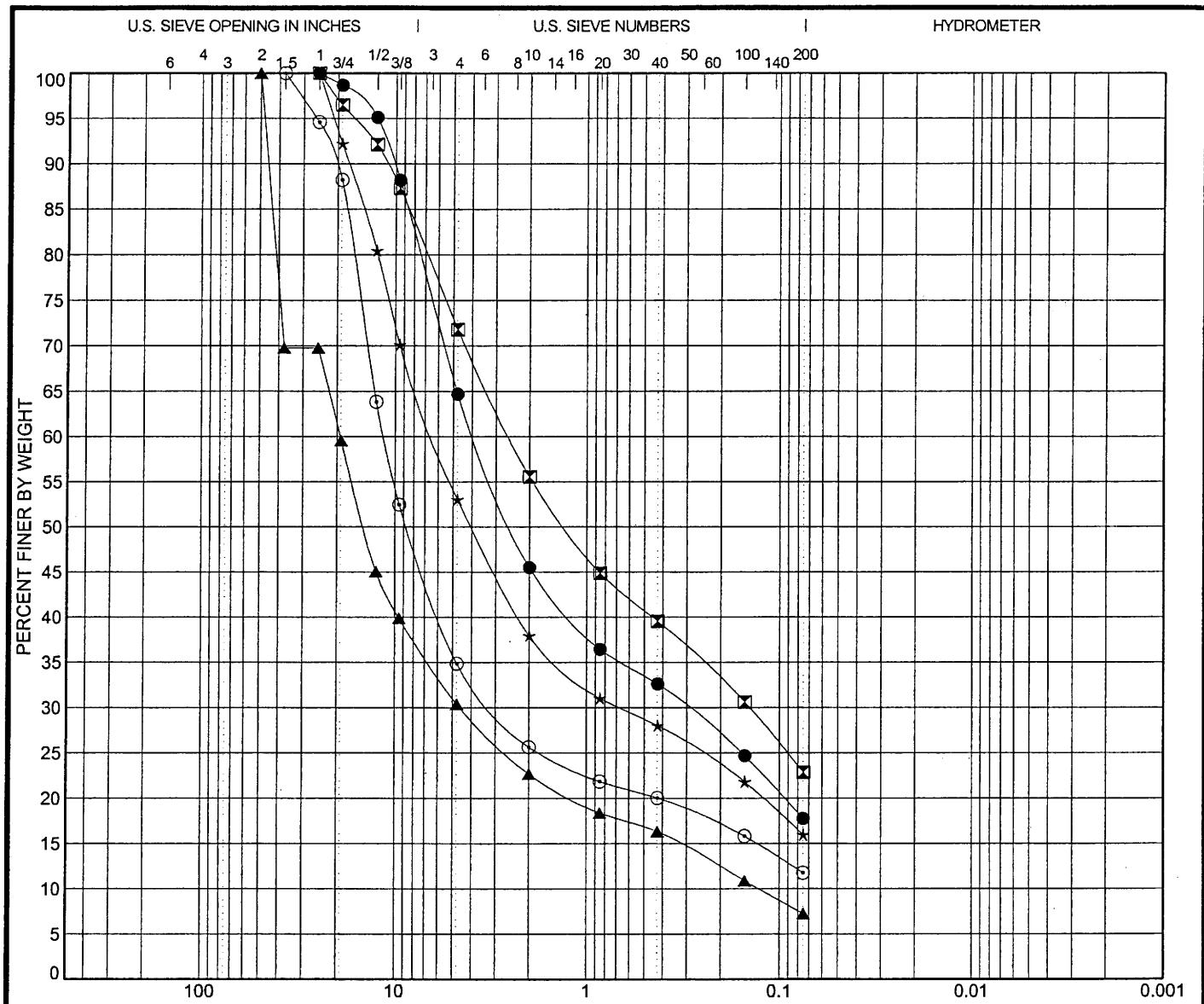
GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Washington Avenue Bridge

Location: Las Vegas, Nevada

Project Number: 0324-01-6

Plate Number: 4d



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

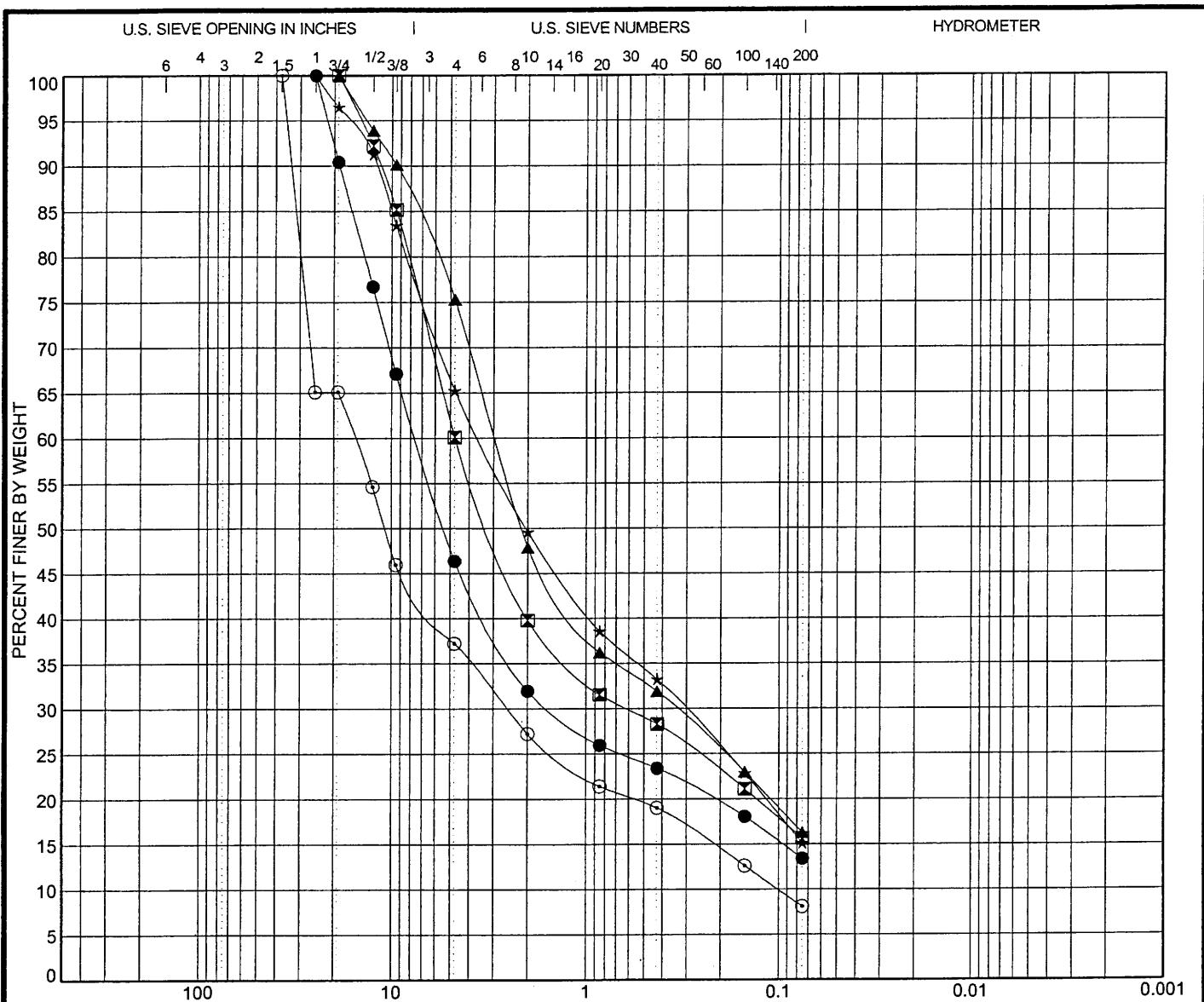
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-42 7.5'	CLAYEY SAND with GRAVEL (SC)						27	15	12		
◻	B-42 10.0'	CLAYEY SAND with GRAVEL (SC)						28	16	12		
▲	B-42 13.5'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						28	19	9	8.56	152.54
★	B-42 15.0'	CLAYEY GRAVEL with SAND (GC)						28	15	13		
○	B-42 17.5'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						27	15	12	14.38	205.74
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-42 7.5'	25	3.845	0.302			4.7	35.3	46.9		17.7	
◻	B-42 10.0'	25	2.536	0.142			5.8	28.2	48.9		22.8	
▲	B-42 13.5'	50	19.219	4.553	0.126	1.3	69.6	23.1			7.3	
★	B-42 15.0'	25	6.301	0.672			3.6	47.0	37.1		16.0	
○	B-42 17.5'	37.5	11.394	3.013			20.2	65.2	23.1		11.8	



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Washington Avenue Bridge
Location: Las Vegas, Nevada
Project Number: 0324-01-6 Plate Number: 4e



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Specimen Identification		USCS Classification					LL	PL	PI	Cc	Cu
●	B-42 20.0'	CLAYEY GRAVEL with SAND (GC)					25	15	10		
◻	B-42 25.0'	CLAYEY SAND with GRAVEL (SC)					24	14	10		
▲	B-42 27.5'	SILTY, CLAYEY SAND with GRAVEL (SC-SM)					23	16	7		
★	B-42 30.0'	CLAYEY SAND with GRAVEL (SC)					26	18	8		
○	B-43 2.5'	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)					25	18	7	4.17	154.40

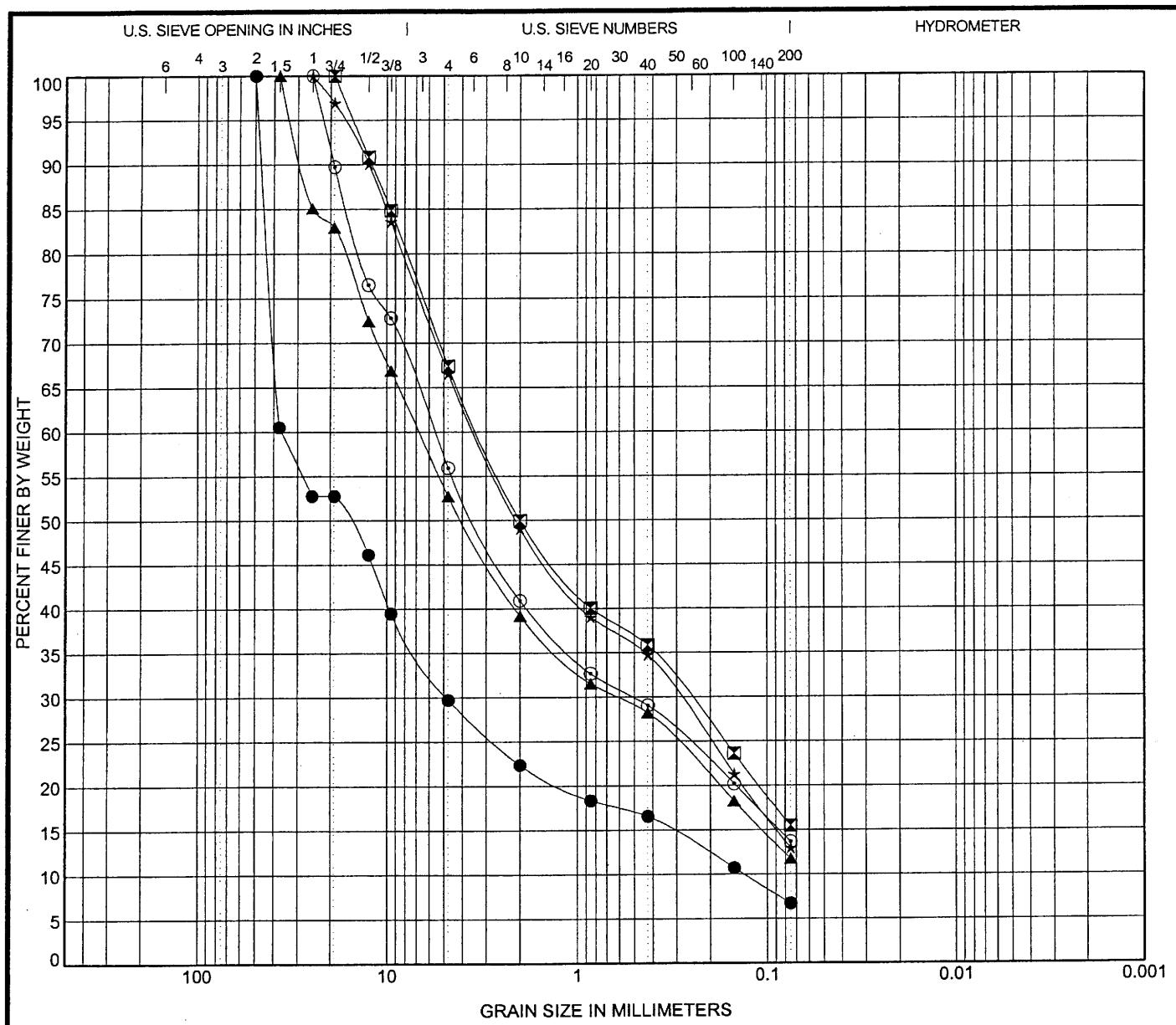
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
●	B-42 20.0'	25	7.492	1.515		2.6	53.6	33.0		13.4
◻	B-42 25.0'	19	4.736	0.616		2.5	39.9	44.4		15.6
▲	B-42 27.5'	19	2.933	0.341		2.6	24.7	59.0		16.3
★	B-42 30.0'	25	3.553	0.308		2.2	34.7	50.1		15.1
○	B-43 2.5'	37.5	15.5	2.546	0.1	2.7	62.8	29.1		8.1



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Washington Avenue Bridge
Location: Las Vegas, Nevada
Project Number: 0324-01-6 Plate Number: 4f



COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

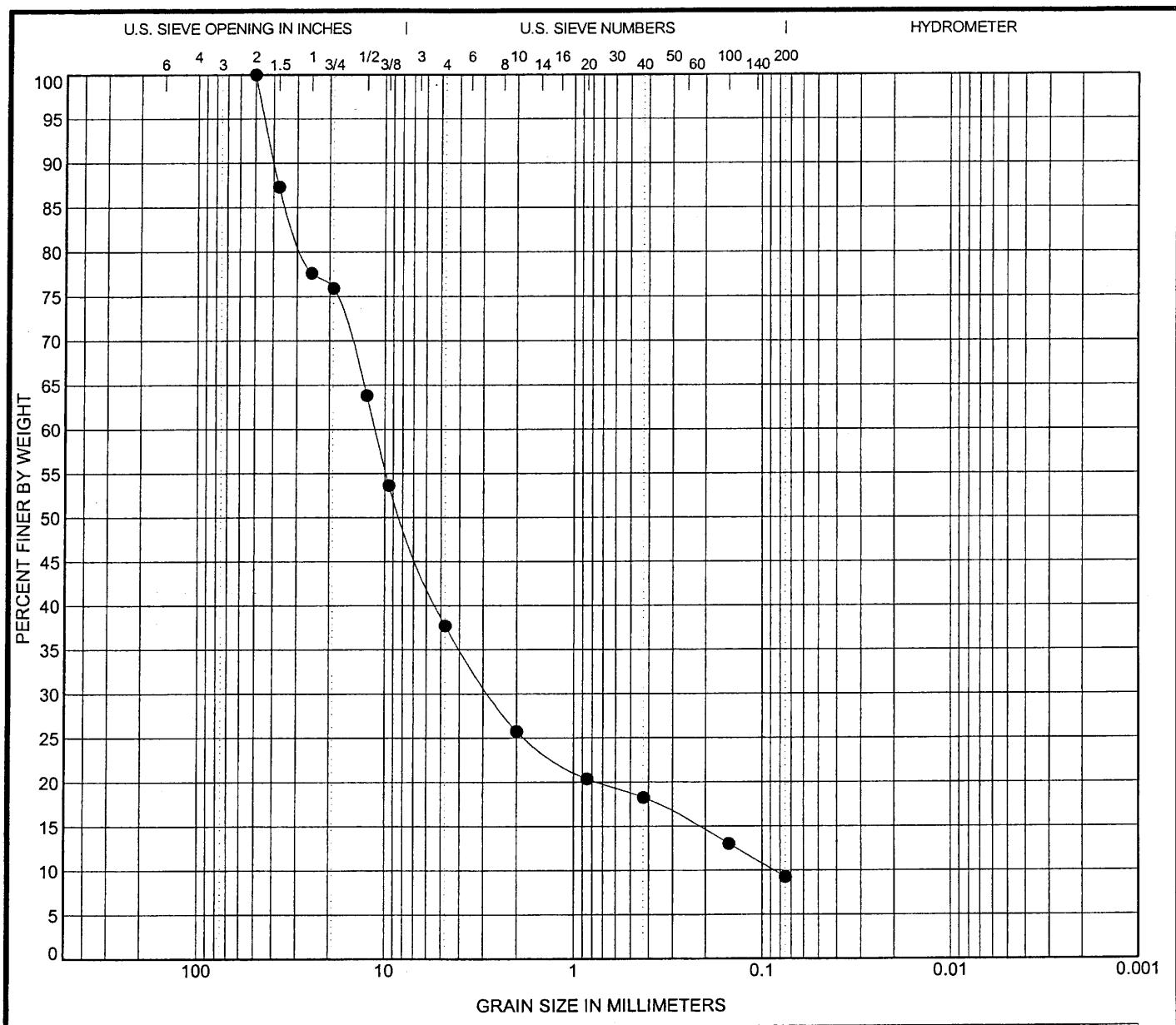
Specimen Identification		USCS Classification						LL	PL	PI	Cc	Cu
●	B-43 5.0'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						27	18	9	4.88	275.98
✗	B-43 7.5'	CLAYEY SAND with GRAVEL (SC)						28	18	10		
▲	B-43 10.0'	POORLY GRADED GRAVEL with SILTY CLAY and SAND (GP-GC)						25	18	7	0.91	109.03
★	B-43 12.5'	CLAYEY SAND with GRAVEL (SC)						27	19	8		
○	B-43 17.5'	CLAYEY GRAVEL with SAND (GC)						25	17	8		
Specimen Identification		D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay		
●	B-43 5.0'	50	36.484	4.85	0.132	2.5	70.3	23.0		6.7		
✗	B-43 7.5'	19	3.294	0.259		5.4	32.6	51.9		15.5		
▲	B-43 10.0'	37.5	6.783	0.62		4.8	47.3	41.0		11.8		
★	B-43 12.5'	25	3.437	0.294		6.3	33.5	53.6		13.0		
○	B-43 17.5'	25	5.617	0.512		3.5	44.1	42.3		13.7		

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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Washington Avenue Bridge
Location: Las Vegas, Nevada
Project Number: 0324-01-6
Plate Number: 4g





COBBLES	GRAVEL		SAND			SILT OR CLAY		
	coarse	fine	coarse	medium	fine			

Specimen Identification	USCS Classification						LL	PL	PI	Cc	Cu
● B-43 20.0'	POORLY GRADED GRAVEL with CLAY and SAND (GP-GC)						24	16	8	7.65	131.24

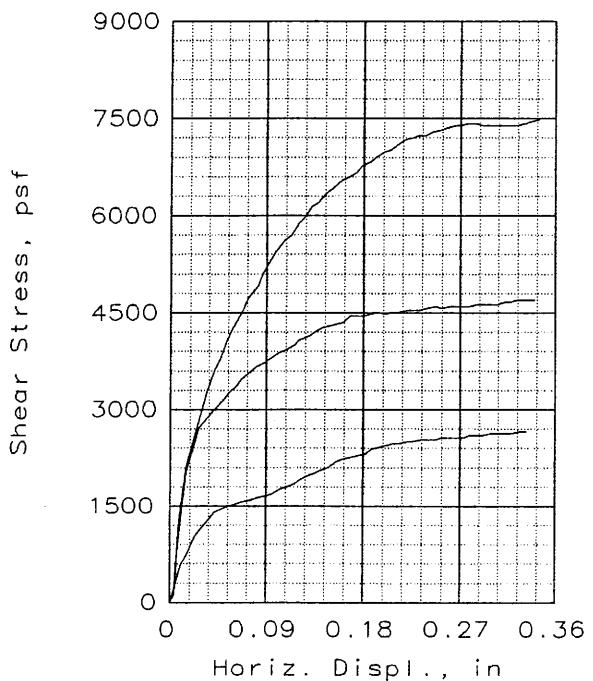
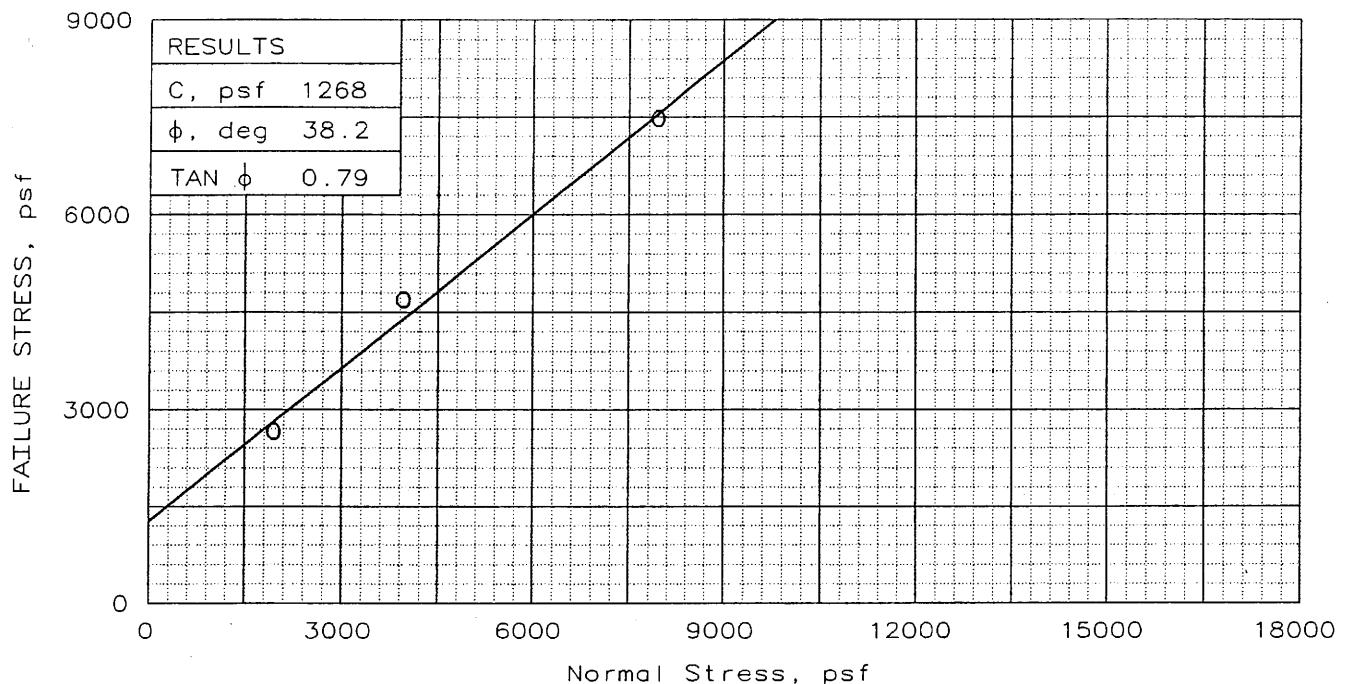
Specimen Identification	D100	D60	D30	D10	MC %	%Gravel	%Sand	%Silt	%Clay
● B-43 20.0'	50	11.275	2.722	0.086	2.8	62.3	28.4		9.3



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GRAIN SIZE DISTRIBUTION

Project: US 95 Widening Project / Washington Avenue Bridge
Location: Las Vegas, Nevada
Project Number: 0324-01-6 Plate Number: 4h

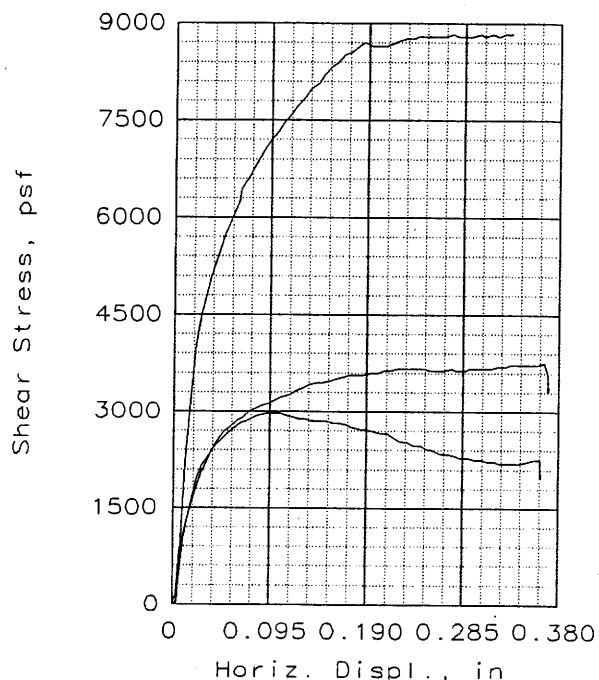
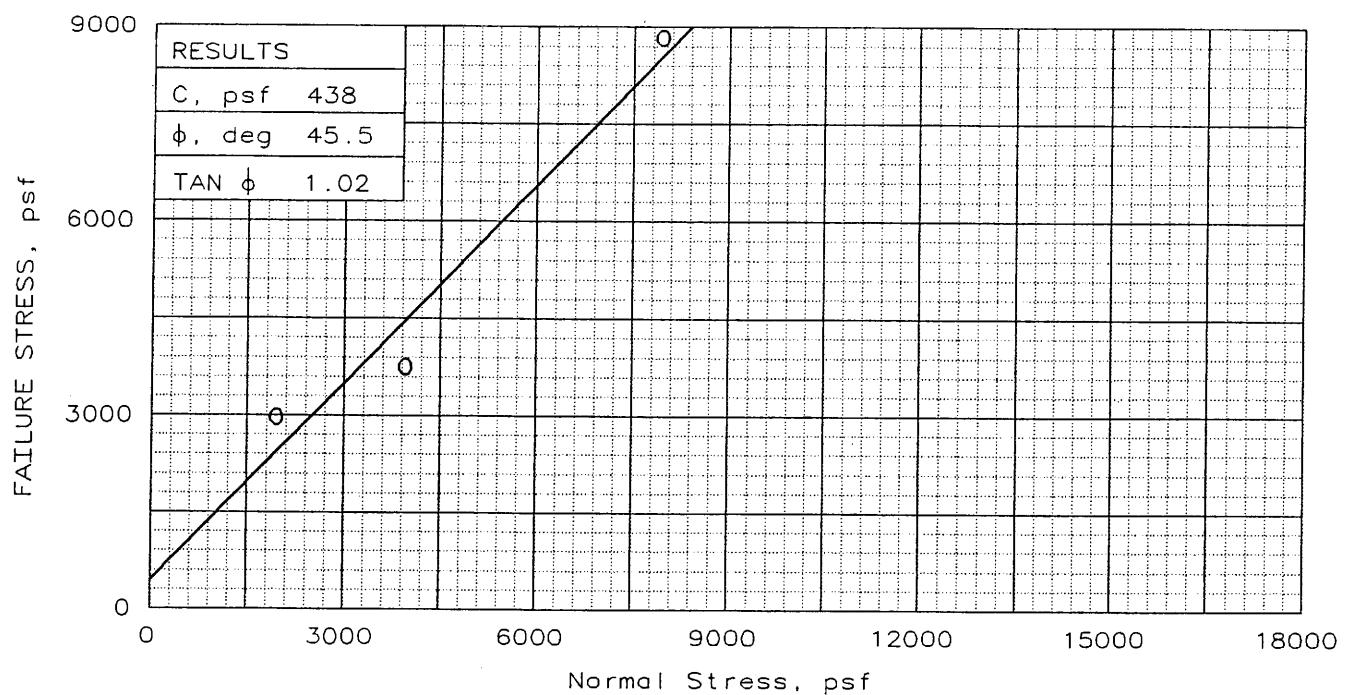


SAMPLE NO.:		1	2	3
INITIAL	WATER CONTENT, %	4.4	4.4	4.4
	DRY DENSITY,pcf	119.7	119.7	119.7
	SATURATION, %	32.0	32.0	32.0
	VOID RATIO	0.356	0.356	0.356
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	1.00	1.00	1.00
AT TEST	WATER CONTENT, %	7.1	6.5	4.7
	DRY DENSITY,pcf	125.5	122.3	122.3
	SATURATION, %	62.7	51.6	37.3
	VOID RATIO	0.293	0.327	0.327
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	0.95	0.98	0.98
NORMAL STRESS, psf		8000	2000	4000
FAILURE STRESS, psf		7482	2661	4696
DISPLACEMENT, in		0.34	0.33	0.32
ULTIMATE STRESS, psf				
DISPLACEMENT, in				
Strain rate, in/min		0.0400	0.0400	0.0400

SAMPLE TYPE: Remolded
 DESCRIPTION: Poorly Graded Grav
 el with Silty Clay and Sand
 LL= 22 PL= 6 PI= 16
 SPECIFIC GRAVITY= 2.6
 REMARKS:

CLIENT: PBS & J
 PROJECT: U.S. 95 Widening
 SAMPLE LOCATION: B-1, Sample 1B
 PROJ. NO.: 0324-01-1 DATE: 10/30/2001

DIRECT SHEAR TEST REPORT
 BLACK EAGLE CONSULTING, INC.

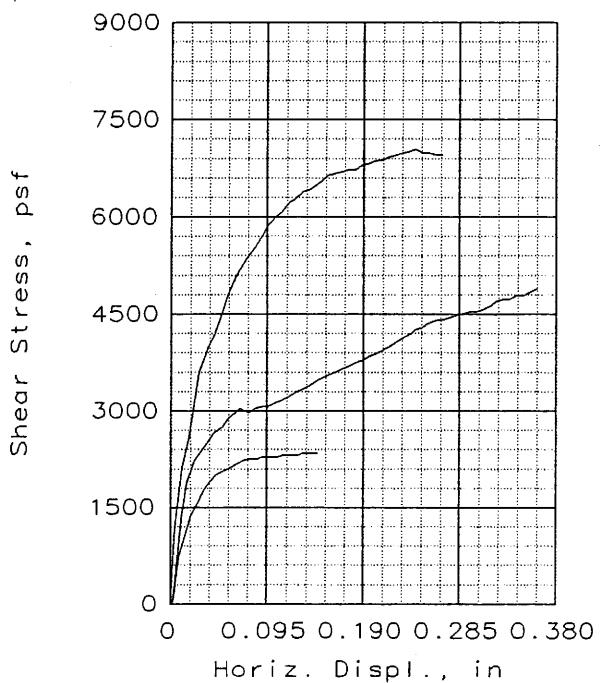
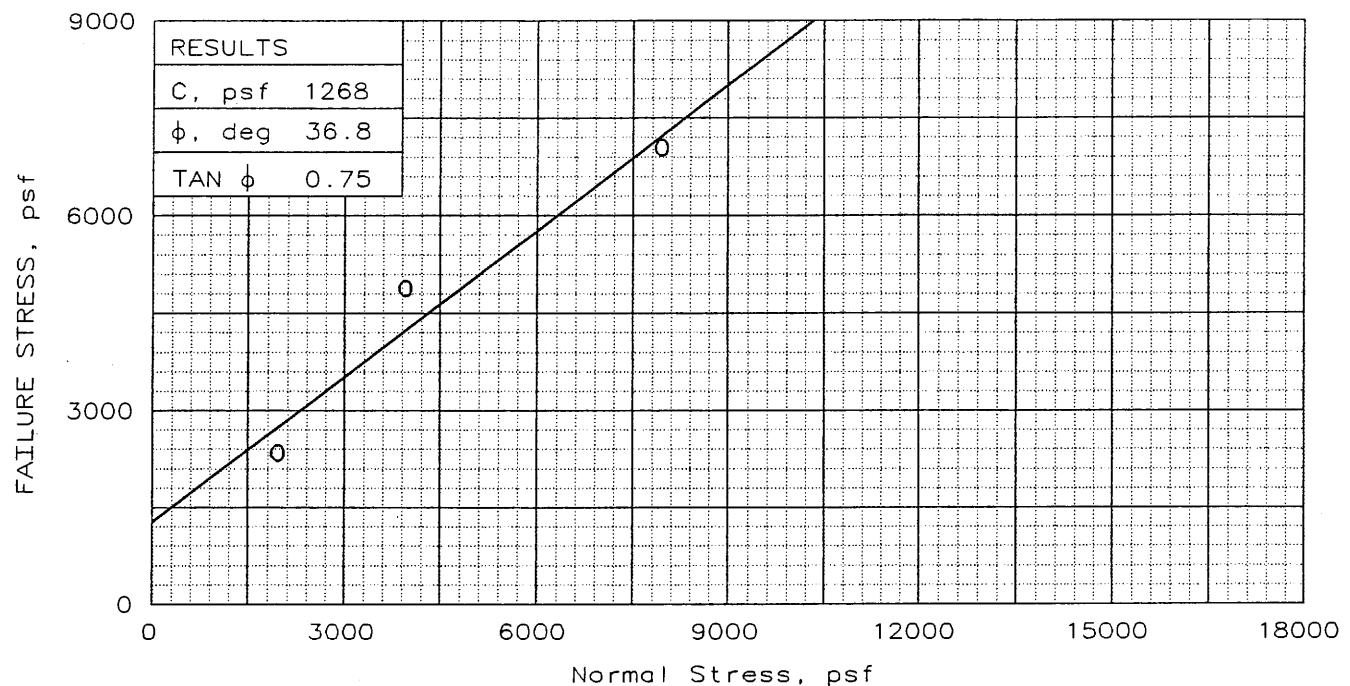


SAMPLE NO.:		1	2	3
INITIAL	WATER CONTENT, %	6.2	6.2	6.2
	DRY DENSITY, pcf	117.7	117.7	117.7
	SATURATION, %	42.7	42.7	42.7
	VOID RATIO	0.380	0.380	0.380
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	1.00	1.00	1.00
AT TEST	WATER CONTENT, %	6.2	6.0	8.7
	DRY DENSITY, pcf	122.4	120.2	120.8
	SATURATION, %	49.5	44.6	65.5
	VOID RATIO	0.326	0.351	0.344
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	0.96	0.98	0.97
NORMAL STRESS, psf		8000	2000	4000
FAILURE STRESS, psf		8829	2974	3757
DISPLACEMENT, in		0.27	0.09	0.37
ULTIMATE STRESS, psf				
DISPLACEMENT, in				
Strain rate, in/min		0.0400	0.0400	0.0400

SAMPLE TYPE: Remolded
 DESCRIPTION: Clayey Sand
 with Gravel
 LL= 32 PL= 18 PI= 14
 SPECIFIC GRAVITY= 2.6
 REMARKS:

CLIENT: PBS & J
 PROJECT: U.S. 95 Widening
 SAMPLE LOCATION: B-2, Sample 2G
 PROJ. NO.: 0324-01-1 DATE: 10/30/2001
 DIRECT SHEAR TEST REPORT

BLACK EAGLE CONSULTING, INC.



SAMPLE NO.:		1	2	3
INITIAL	WATER CONTENT, %	6.1	6.1	6.1
	DRY DENSITY, pcf	117.8	117.8	117.8
	SATURATION, %	41.8	41.8	41.8
	VOID RATIO	0.378	0.378	0.378
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	1.00	1.00	1.00
AT TEST	WATER CONTENT, %	6.9	6.2	8.3
	DRY DENSITY, pcf	122.9	121.1	121.3
	SATURATION, %	56.1	47.4	63.9
	VOID RATIO	0.321	0.340	0.338
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	0.96	0.97	0.97
NORMAL STRESS, psf		8000	2000	4000
FAILURE STRESS, psf		7044	2348	4884
DISPLACEMENT, in		0.24	0.13	0.36
ULTIMATE STRESS, psf				
DISPLACEMENT, in				
Strain rate, in/min		0.0400	0.0400	0.0400

SAMPLE TYPE: Remolded

DESCRIPTION: Silty, Clayey Sand
with Gravel

LL= 21 PL= 14 PI= 7

SPECIFIC GRAVITY= 2.6

REMARKS:

Fig. No.: _____

CLIENT: PBS & J

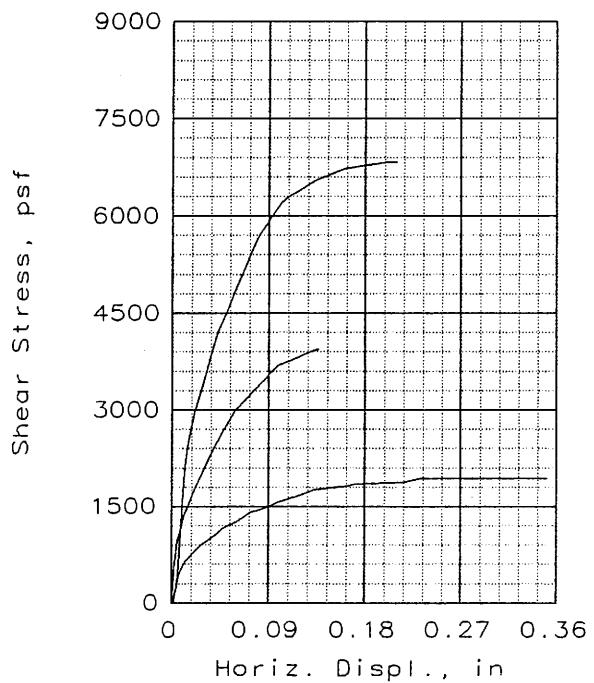
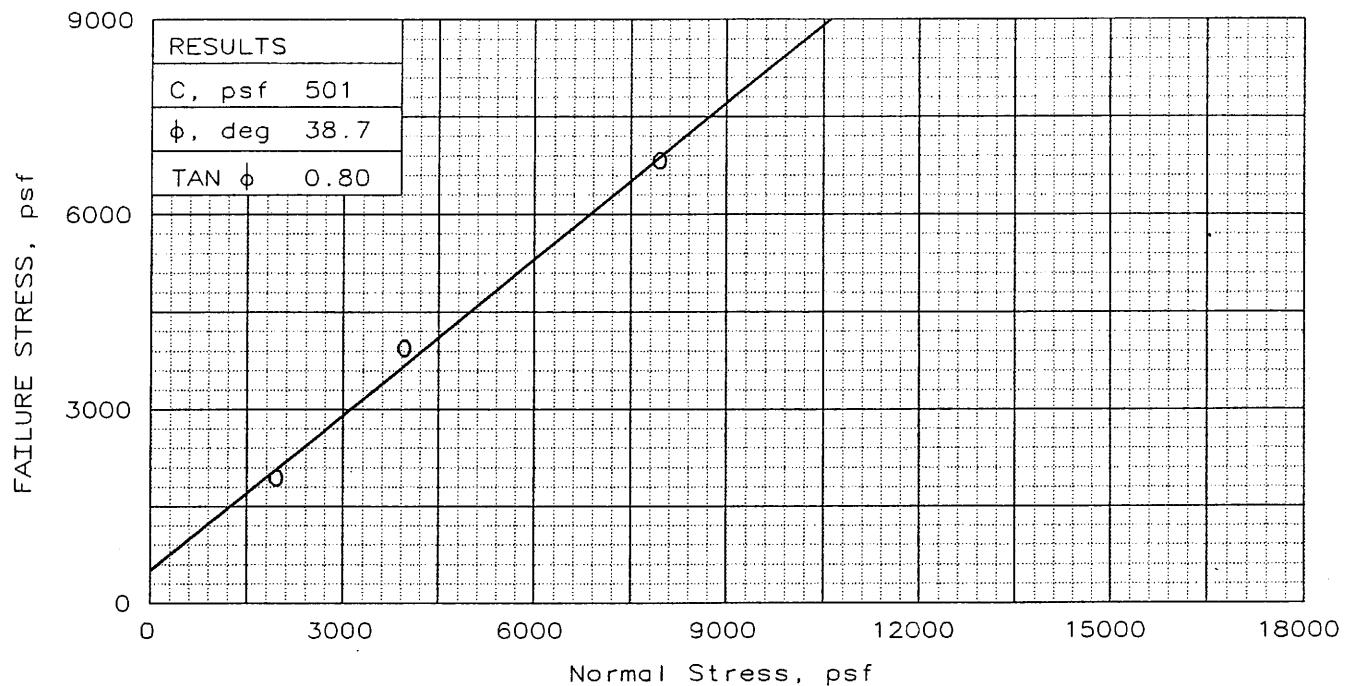
PROJECT: U.S. 95 Widening

SAMPLE LOCATION: B-3, Sample 3L

PROJ. NO.: 0324-01-1 DATE: 11/5/2001

DIRECT SHEAR TEST REPORT

BLACK EAGLE CONSULTING, INC.

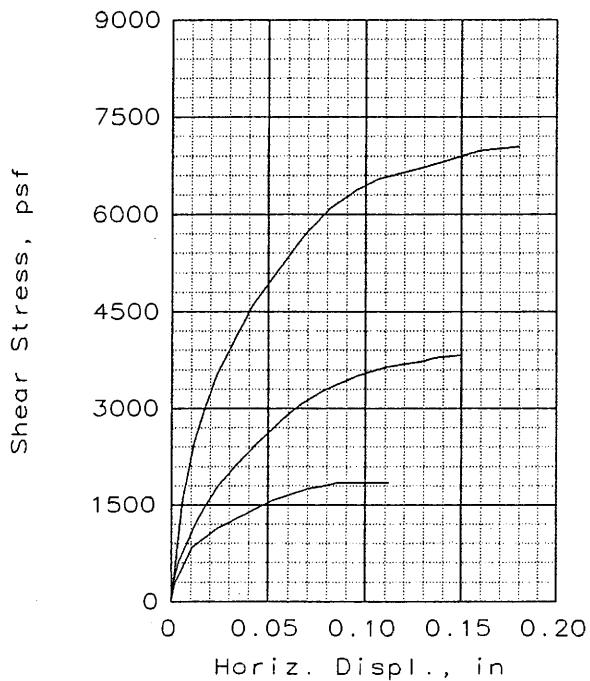
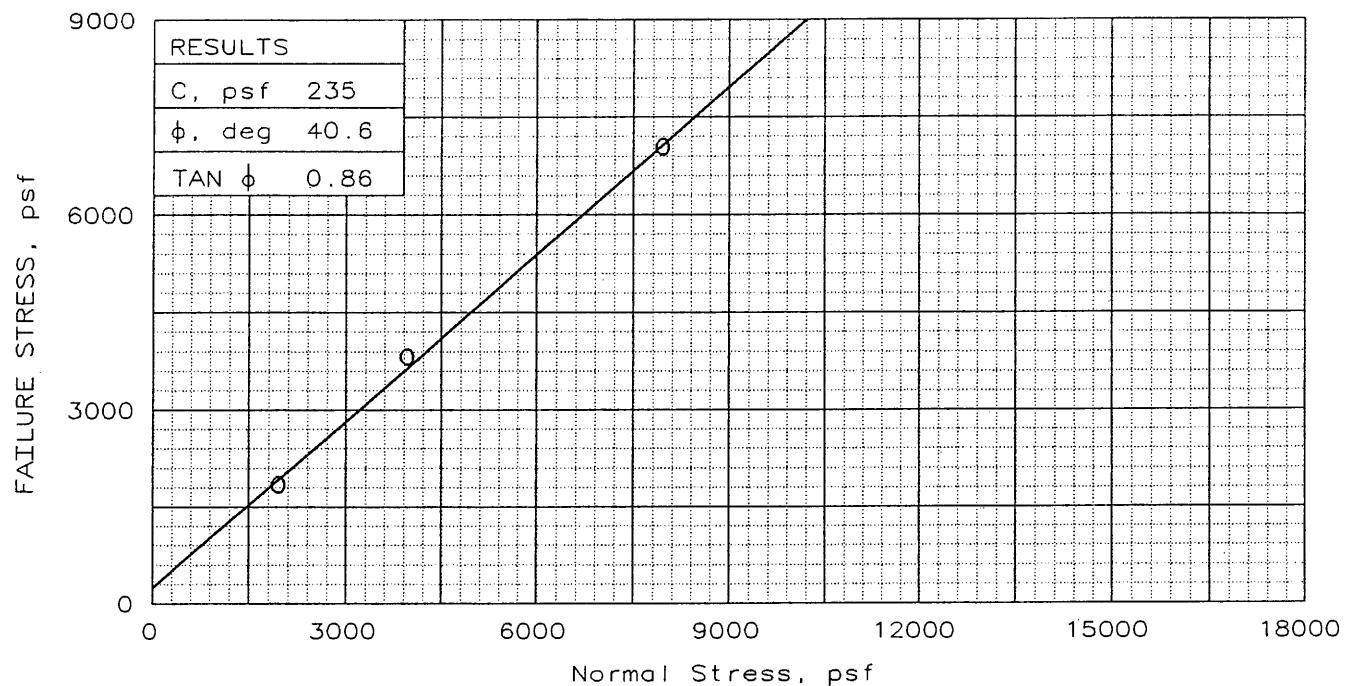


SAMPLE NO.:	1	2	3	
INITIAL	WATER CONTENT, %	3.1	3.1	3.1
	DRY DENSITY, pcf	114.5	114.5	114.5
	SATURATION, %	24.1	24.1	24.1
	VOID RATIO	0.309	0.309	0.309
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	1.00	1.00	1.00
AT TEST	WATER CONTENT, %	11.5	11.0	11.2
	DRY DENSITY, pcf	117.4	118.3	118.1
	SATURATION, %	99.5	99.2	100.1
	VOID RATIO	0.276	0.266	0.268
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	0.98	0.97	0.97
NORMAL STRESS, psf		2000	4000	8000
FAILURE STRESS, psf		1941	3945	6825
DISPLACEMENT, in		0.23	0.14	0.20
ULTIMATE STRESS, psf				
DISPLACEMENT, in				
Strain rate, in/min		0.0200	0.0200	0.0200

SAMPLE TYPE: Remolded
 DESCRIPTION: Poorly Graded
 Gravel with Silt and Sand
 LL= 20 PL= 17 PI= 3
 SPECIFIC GRAVITY= 2.4
 REMARKS:

Fig. No.: _____

CLIENT: PBS&J
 PROJECT: U.S. 95 / Rainbow Boulevard
 Bridge Reconstruction
 SAMPLE LOCATION: B-X, Sample B
 PROJ. NO.: 0324-01-2 DATE: 12/13/2001
 DIRECT SHEAR TEST REPORT
 BLACK EAGLE CONSULTING, INC.



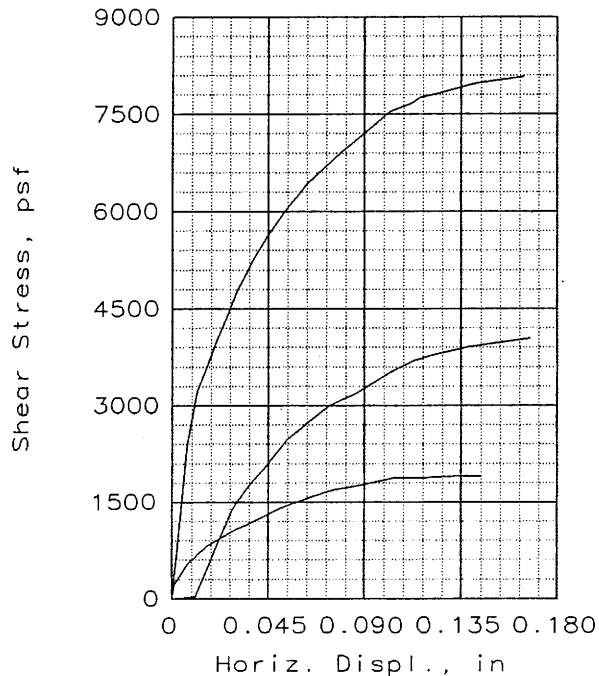
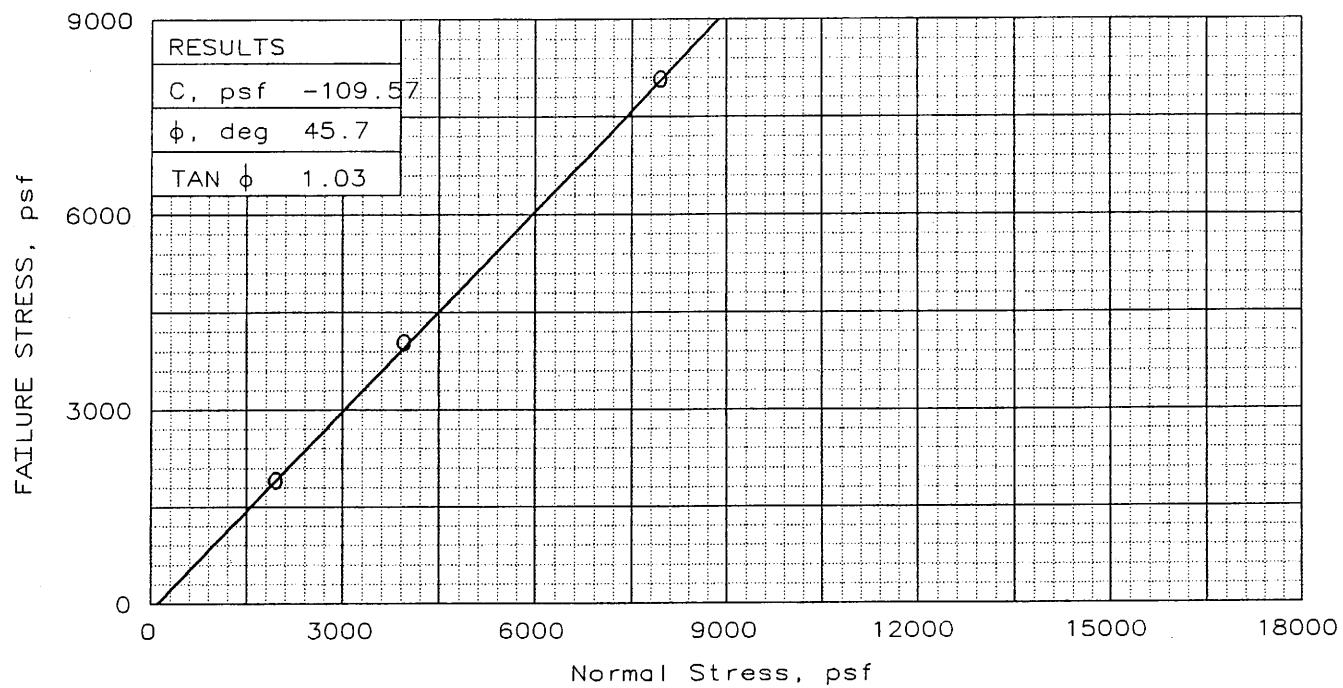
SAMPLE NO.:		1	2	3
INITIAL	WATER CONTENT, %	3.0	3.0	3.0
	DRY DENSITY,pcf	114.6	114.6	114.6
	SATURATION, %	20.7	20.7	20.7
	VOID RATIO	0.362	0.362	0.362
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	1.00	1.00	1.00
AT TEST	WATER CONTENT, %	13.6	13.1	12.7
	DRY DENSITY,pcf	116.5	117.5	118.4
	SATURATION, %	99.9	99.7	99.8
	VOID RATIO	0.340	0.328	0.318
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	0.98	0.98	0.97
NORMAL STRESS, psf		2000	4000	8000
FAILURE STRESS, psf		1847	3819	7044
DISPLACEMENT, in		0.09	0.15	0.18
ULTIMATE STRESS, psf				
DISPLACEMENT, in				
Strain rate, in/min		0.0200	0.0200	0.0200

SAMPLE TYPE: Remolded
 DESCRIPTION: Silty, Clayey Sand
 with Gravel
 LL= 27 PL= 20 PI= 7
 SPECIFIC GRAVITY= 2.5
 REMARKS:

Fig. No.: _____

CLIENT: PBS&J
 PROJECT: U.S. 95 / Rainbow Boulevard
 Bridge Reconstruction
 SAMPLE LOCATION: B-~~K~~, Sample A
 PROJ. NO.: 0324-01-2 DATE: 12/14/2001
 DIRECT SHEAR TEST REPORT

BLACK EAGLE CONSULTING, INC.



SAMPLE NO.:	1	2	3	
INITIAL	WATER CONTENT, %	2.2	2.2	2.2
	DRY DENSITY, pcf	115.5	115.5	115.5
	SATURATION, %	15.6	15.6	15.6
	VOID RATIO	0.351	0.351	0.351
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	1.00	1.00	1.00
AT TEST	WATER CONTENT, %	11.4	10.4	10.3
	DRY DENSITY, pcf	121.1	123.4	123.9
	SATURATION, %	98.9	98.5	98.9
	VOID RATIO	0.289	0.265	0.259
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	0.95	0.94	0.93
NORMAL STRESS, psf		2000	4000	8000
FAILURE STRESS, psf		1910	4039	8077
DISPLACEMENT, in		0.13	0.17	0.16
ULTIMATE STRESS, psf				
DISPLACEMENT, in				
Strain rate, in/min		0.0200	0.0200	0.0200

SAMPLE TYPE: Remolded
 DESCRIPTION: Well-Graded Sand
 with Silty Clay and Gravel
 LL= 21 PL= 16 PI= 5
 SPECIFIC GRAVITY= 2.5
 REMARKS:

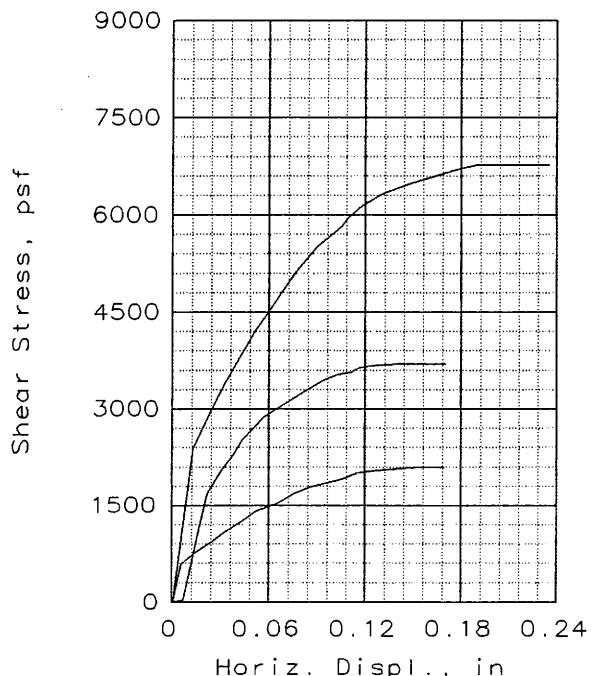
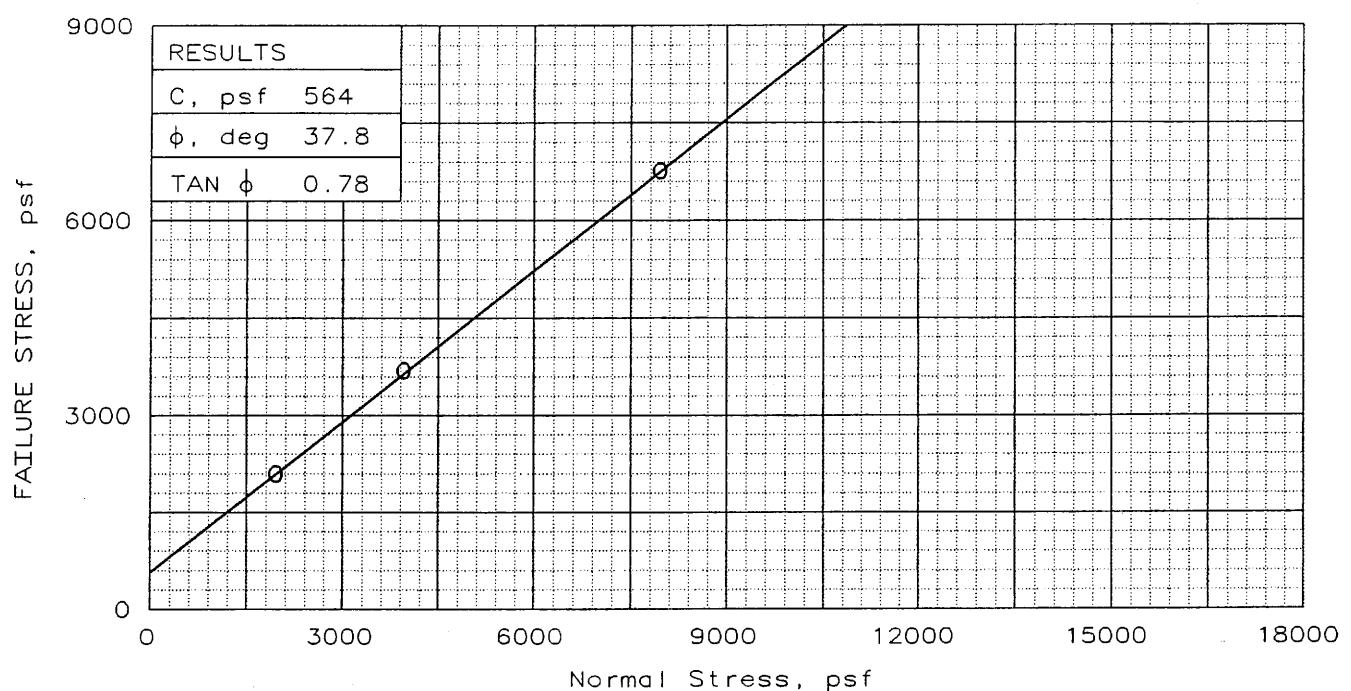
Fig. No.: _____

CLIENT: PBS&J
 PROJECT: U.S. 95 / Rainbow Boulevard
 Bridge Reconstruction
 SAMPLE LOCATION: B-X, Sample B

PROJ. NO.: 0324-01-2 DATE: 12/14/2001

DIRECT SHEAR TEST REPORT

BLACK EAGLE CONSULTING, INC.



SAMPLE NO.:		1	2	3
INITIAL	WATER CONTENT, %	1.2	1.2	1.2
	DRY DENSITY, pcf	116.6	116.6	116.6
	SATURATION, %	8.4	8.4	8.4
	VOID RATIO	0.365	0.365	0.365
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	1.00	1.00	1.00
AT TEST	WATER CONTENT, %	12.6	12.1	11.9
	DRY DENSITY, pcf	120.2	121.5	122.0
	SATURATION, %	99.3	99.7	99.7
	VOID RATIO	0.324	0.310	0.305
	DIAMETER, in	2.42	2.42	2.42
	HEIGHT, in	0.97	0.96	0.96
NORMAL STRESS, psf		2000	4000	8000
FAILURE STRESS, psf		2098	3694	6762
DISPLACEMENT, in		0.15	0.14	0.19
ULTIMATE STRESS, psf				
DISPLACEMENT, in				
Strain rate, in/min		0.0200	0.0200	0.0200

SAMPLE TYPE: Remolded
DESCRIPTION: Poorly Graded
Gravel with Silt and Sand

SPECIFIC GRAVITY = 2.55

REMARKS:

Fig. No.: _____

CLIENT: PBS&J

PROJECT: U.S. 95 / Rainbow Boulevard
Bridge Reconstruction

SAMPLE LOCATION: B-X Sample A

12

PROJ. NO.: 0324-01-2 DATE: 12/14/2001

DIRECT SHEAR TEST REPORT

BLACK EAGLE CONSULTING, INC.

APPENDIX III

CALCULATIONS

TABLE 3-4

Empirical values for ϕ , D_r , and unit weight of granular soils based on the SPT at about 6 m depth and normally consolidated [approximately, $\phi = 28^\circ + 15^\circ D_r (\pm 2^\circ)$]

Description	Very loose	Loose	Medium	Dense	Very dense
Relative density D_r	0	0.15	0.35	0.65	0.85
SPT N-value					
fine	1-2	3-6	7-15	16-30	?
medium	2-3	4-7	8-20	21-40	> 40
coarse	3-6	5-9	10-25	26-45	(> 45)
fine	26-28	28-30	30-34	33-38	
medium	27-28	30-32	32-36	36-42	(< 50)
coarse	28-30	30-34	33-40	(40-50)	
Unit weight γ kN/m ³	11-16*	14-18	17-20	17-22	20-23

Excavated soil or material dumped from a truck has a unit weight of 11 to 14 kN/m³ and must be quite dense to weigh much over 21 kN/m³. No existing soil has a $D_r = 0.00$ nor a value of 1.00. Common ranges are from 0.3 to 0.7.

The following are several SPT N -value correlations for angle of friction ϕ . The top two of Eq. (3-5) are from Shioi and Fukui (1982), who obtained them from the Japanese Railway Standards:

$$\begin{aligned}\phi &= \sqrt{18N'_{70} + 15} \\ \phi &= 0.36N_{70} + 27 \\ \phi &= 4.5N_{70} + 20 \text{ (in general)}\end{aligned}\quad (3-5)$$

The top equation of this set is for roads and bridges, and the second is for buildings (refer also to Table 3-4).

A relationship for N and D_r was proposed indirectly by Meyerhof (1957) as

$$\frac{N}{D_r^2} = A + B p'_o \quad (3-5a)$$

For this equation Skempton (1986), using a database of five different soils, found that A and B are site-dependent with a range in A of 15 to about 54 and in B from 0.306 to 0.204 (using the N'_{70} base). This spread is such that using average values for A and B is somewhat risky; however, using averages we obtain

$$\frac{N'_{70}}{D_r^2} = 32 + 0.288 p'_o \quad (3-5b)$$

with p'_o in kPa. For an average unit weight γ of 16 to 17 kN/m³ and a depth of about 6 m one obtains $N'_{70}/D_r^2 \approx 60$, which was also used as a guide in designating the N values for normally consolidated sands of Table 3-4. For overconsolidated sands ($OCR > 1$), Skempton (1986) suggested the following adjustment:

$$\frac{N'_{70}}{D_r^2} = A + BC_{OCR} p'_o \quad (3-5c)$$

BLACK EAGLE CONSULTING
Geotechnical and Construction Services

Project Name:US-95 Widening Proj. 5-A/B
Project Number: 0324-01-1

Date: 12/28/01
Page: 1 of 2
Calculated By:HEB
Checked By: SDB

CALCULATION OF STATIC BEARING CAPACITY

Location: Bridges R6, R7, and HOV Flyover Native Soils
also conservative for retaining walls

References

1. AASHTO, 1997: Standard Specifications for Highway Bridges, 16th edition, American Association of State Highway and Transportation Officials

Conversions

Checked By:SDB

$$\begin{aligned} \text{kN} &:= 1000 \cdot \text{N} & \text{kPa} &:= 1000 \cdot \text{Pa} & \text{kip} &:= 1000 \cdot \text{lbf} & \text{ksf} &:= 1000 \cdot \frac{\text{lbf}}{\text{ft}^2} & \text{psf} &:= \frac{\text{lbf}}{\text{ft}^2} & \text{pcf} &:= \frac{\text{lbf}}{\text{ft}^3} \\ \text{MPa} &:= 1000 \cdot \text{kPa} \end{aligned}$$

Assumptions

Checked By:SDB

1. Conditions are dry
2. Footings will be at least 1.4 meters wide
3. Native soils can be modeled as phi=40 degrees

Input Data

Checked By:SDB

Width of Footing:	$B := 4.6\text{ft}$	$B = 1.402\text{ m}$	Poissons Ratio	$\nu := 0.2$
Length of Footing	$L := 40\text{-ft}$		Youngs Mod	$E_s := 4200 \cdot \frac{\text{kip}}{\text{ft}^2}$
Depth of Embedment:	$D := 4\text{ft}$	$D = 1.219\text{ m}$	Rigidity shape Factor	$\beta_z := 1.41$
Unit Weight of Soil:	$\gamma := 130\text{pcf}$	$\gamma = 20.421 \frac{\text{kN}}{\text{m}^3}$		
Cohesion:	$c := 0\text{psf}$	$c = 0\text{ kPa}$		
Friction Angle:	$\phi := 40\text{deg}$			
Safety Factor:	$FS := 3$			

Calculate Bearing Capacity Factors:

$$N_q := e^{(\pi \cdot \tan(\phi))} \cdot \tan\left(45 \cdot \text{deg} + \frac{\phi}{2}\right)^2 \quad N_q = 64.195$$

$$N_c := (N_q - 1) \cdot \cot(\phi) \quad N_c = 75.313$$

$$N_\gamma := 2 \cdot (N_q + 1) \cdot \tan(\phi) \quad N_\gamma = 109.411$$

Calculate Overburden Pressure:

$$q := \gamma \cdot D \quad q = 520 \text{ psf} \quad q = 24.898 \text{ kPa}$$

Shape factors

Assume Worst Case -- a strip footing

Calculate Ultimate Bearing Capacity:

$$q_{ult} := (c \cdot N_c) + (0.5 \cdot \gamma \cdot B \cdot N_\gamma) + (q \cdot N_q) \quad q_{ult} = 6.61 \times 10^4 \text{ psf} \quad q_{ult} = 3.165 \text{ MPa}$$

Calculate Allowable Bearing Capacity:

$$q_{allow} := \frac{q_{ult}}{FS} \quad q_{allow} = 2.203 \times 10^4 \text{ psf} \quad q_{allow} = 1.055 \text{ MPa}$$

Settlement

$$q_0 := q_{\text{allow}}$$

$$S_c := \frac{q_0 \cdot (1 - v^2) \cdot \sqrt{B \cdot L}}{E_s \cdot \beta_z} \quad S_c = 14.766 \text{ mm}$$

BLACK EAGLE CONSULTING
Geotechnical and Construction Services

Project Name:US-95 Widening Proj. 5-A/B
Project Number: 0324-01-1

Date: 12/28/01
Page: 1 of 2
Calculated By:HEB
Checked By: SDB

CALCULATION OF STATIC BEARING CAPACITY

Location: Bridges R6, R7, and HOV Flyover (Fills) also
suitable as conservative for Retaining Walls

References

1. AASHTO, 1997: Standard Specifications for Highway Bridges, 16th edition, American Association of State Highway and Transportation Officials

Conversions

Checked By:SDB

$$\begin{aligned} \text{kN} &:= 1000 \cdot \text{N} & \text{kPa} &:= 1000 \cdot \text{Pa} & \text{kip} &:= 1000 \cdot \text{lbf} & \text{ksf} &:= 1000 \cdot \frac{\text{lbf}}{\text{ft}^2} & \text{psf} &:= \frac{\text{lbf}}{\text{ft}^2} & \text{pcf} &:= \frac{\text{lbf}}{\text{ft}^3} \\ & & & & & & & & & & \\ \text{MPa} &:= 1000 \cdot \text{kPa} & & & & & & & & & \end{aligned}$$

Assumptions

Checked By:SDB

1. Conditions are dry
2. Footings will be at least 1.0 meters wide
3. Embankment soils can be modeled as phi=32 degrees

Input Data

Checked By:SDB

Width of Footing:	$B := 1 \cdot \text{m}$	$B = 1 \text{ m}$	Poissons Ratio	$\nu := 0.2$
Length of Footing	$L := 40 \cdot \text{ft}$		Youngs Mod	$E_s := 4200 \cdot \frac{\text{kip}}{\text{ft}^2}$
Depth of Embedment:	$D := 2 \cdot \text{ft}$	$D = 0.61 \text{ m}$	Rigidity shape Factor	$\beta_z := 1.41$
Unit Weight of Soil:	$\gamma := 125 \text{pcf}$	$\gamma = 19.636 \frac{\text{kN}}{\text{m}^3}$		
Cohesion:	$c := 0 \text{ psf}$	$c = 0 \text{ kPa}$		
Friction Angle:	$\phi := 32 \text{deg}$			
Safety Factor:	$FS := 3$			

Calculate Bearing Capacity Factors:

$$N_q := e^{(\pi \cdot \tan(\phi))} \cdot \tan\left(45^\circ - \frac{\phi}{2}\right)^2 \quad N_q = 23.177$$

$$N_c := (N_q - 1) \cdot \cot(\phi) \quad N_c = 35.49$$

$$N_y := 2 \cdot (N_q + 1) \cdot \tan(\phi) \quad N_y = 30.215$$

Calculate Overburden Pressure:

$$q := \gamma \cdot D \quad q = 250 \text{ psf} \quad q = 11.97 \text{ kPa}$$

Shape factors Assume Worst Case -- a strip footing

Calculate Ultimate Bearing Capacity:

$$q_{ult} := (c \cdot N_c) + (0.5 \cdot \gamma \cdot B \cdot N_y) + (q \cdot N_q) \quad q_{ult} = 1.199 \times 10^4 \text{ psf} \quad q_{ult} = 574.074 \text{ kPa}$$

Calculate Allowable Bearing Capacity:

$$q_{allow} := \frac{q_{ult}}{FS} \quad q_{allow} = 3.997 \times 10^3 \text{ psf} \quad q_{allow} = 191.358 \text{ kPa}$$

Settlement

$$D = 0.61 \text{ m}$$

$$x := 190 \cdot \text{kPa} \quad x = 3.968 \frac{\text{kip}}{\text{ft}^2}$$

$$q_o := q_{allow}$$

$$S_c := \frac{[q_o \cdot (1 - v^2) \cdot \sqrt{B \cdot L}]}{E_s \cdot \beta_z} \quad S_c = 2.262 \text{ mm}$$

TABLE 1
Ultimate Friction Factors and Adhesion for Dissimilar Materials

Interface Materials	Friction factor, $\tan \delta$	Friction angle, δ degrees
Mass concrete on the following foundation materials:		
Clean sound rock.....	0.70	35
Clean gravel, gravel-sand mixtures, coarse sand...	<u>0.55 to 0.60</u>	<u>29 to 31</u>
Clean fine to medium sand, silty medium to coarse sand, silty or clayey gravel.....	<u>0.45 to 0.55</u>	<u>24 to 29</u>
Clean fine sand, silty or clayey fine to medium sand.....	0.35 to 0.45	19 to 24
Fine sandy silt, nonplastic silt.....	0.30 to 0.35	17 to 19
Very stiff and hard residual or preconsolidated clay.....	0.40 to 0.50	22 to 26
Medium stiff and stiff clay and silty clay.....	0.30 to 0.35	17 to 19
(Masonry on foundation materials has same friction factors.)		
Steel sheet piles against the following soils:		
Clean gravel, gravel-sand mixtures, well-graded rock fill with spalls.....	0.40	22
Clean sand, silty sand-gravel mixture, single size hard rock fill.....	0.30	17
Silty sand, gravel or sand mixed with silt or clay	0.25	14
Fine sandy silt, nonplastic silt.....	0.20	11
Formed concrete or concrete sheet piling against the following soils:		
Clean gravel, gravel-sand mixture, well-graded rock fill with spalls.....	0.40 to 0.50	22 to 26
Clean sand, silty sand-gravel mixture, single size hard rock fill.....	0.30 to 0.40	17 to 22
Silty sand, gravel or sand mixed with silt or clay	0.30	17
Fine sandy silt, nonplastic silt.....	0.25	14
Various structural materials:		
Masonry on masonry, igneous and metamorphic rocks:		
Dressed soft rock on dressed soft rock.....	0.70	35
Dressed hard rock on dressed soft rock.....	0.65	33
Dressed hard rock on dressed hard rock.....	0.55	29
Masonry on wood (cross grain).....	0.50	26
Steel on steel at sheet pile interlocks.....	0.30	17
Interface Materials (Cohesion)	Adhesion C_a (psf)	
Very soft cohesive soil (0 - 250 psf)	0 - 250	
Soft cohesive soil (250 - 500 psf)	250 - 500	
Medium stiff cohesive soil (500 - 1000 psf)	500 - 750	
Stiff cohesive soil (1000 - 2000 psf)	750 - 950	
Very stiff cohesive soil (2000 - 4000 psf)	950 - 1,300	

Project Name: US 95 Widening; Retaining Walls 2C/2D Cut 34 / level Backfill for Cantilever walls
 Project Number: 324-01-3 ($i = 0$ degrees)
 Calculated By: HEB Checked By: SDB

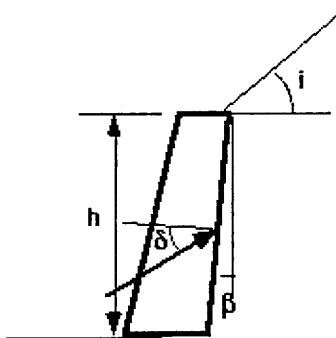
MONONOBE- OKABE ANALYSIS

Reference: Federal Highway Administration, 1998:
Geotechnical Earthquake Engineering,
 Publication No. FHWA HI-99-012.

$$k_h := .18 \quad K_h := 0.5 \cdot k_h \quad K_h = 0.09$$

(per AASHTO)

$$k_v := 0.0$$



For structural backfill: $\phi := 34 \cdot \text{deg}$

$\delta := 0$ (may approach 0 during earthquake;
 is conservative))

$\beta := 0 \cdot \text{deg}$ $i := 0 \text{deg}$

$$\theta := \text{atan} \left(\frac{k_h}{1 - k_v} \right) \quad \theta = 0.09$$

$$K_{ae} := \frac{\cos(\phi - \theta - \beta)^2}{\cos(\theta) \cdot \cos(\beta)^2 \cdot \cos(\delta + \beta + \theta) \cdot \left(1 + \sqrt{\frac{\sin(\phi + \delta) \cdot \sin(\phi - \theta - i)}{\cos(\delta + \beta + \theta) \cdot \cos(i - \beta)}} \right)^2}$$

$$K_{ae} = 0.334$$

$$K_a(\phi, i, \beta) \equiv \frac{\cos(\phi - \beta)^2}{(\cos(\beta)^2 \cdot \cos(i)) \cdot \left[\left(1 + \sqrt{\frac{\sin(\phi) \cdot \sin(\phi - i)}{\cos(\beta) \cdot \cos(i - \beta)}} \right)^2 \right]}$$

$$K_a := K_a(\phi, i, \beta)$$

$$K_a = 0.283$$

Project Name: US 95 Widening; Retaining Walls 2C/2D
Project Number: 324-01-3
Calculated By: KWK Checked By: SDB

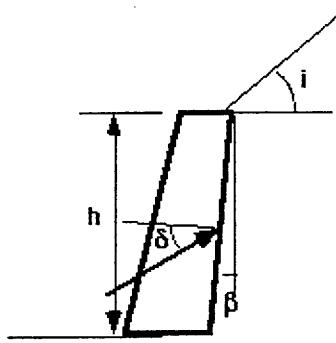
**Cut 34 / Sloping Backfill for Cantilever walls
($i = 26.6$ degrees)**

$$\text{atan}\left(\frac{i}{2}\right) = 26.6 \text{ deg}$$

MONONOBE-OKABE ANALYSIS

Reference: Federal Highway Administration, 1998:
Geotechnical Earthquake Engineering,
Publication No. FHWA HI-99-012.

$$k_h := .18 \quad K_h := 0.5 \cdot k_h \quad K_h = 0.09 \\ (\text{per AASHTO}) \\ k_v := 0.0$$



For structural backfill: $\phi := 34 \text{ deg}$

$\delta := 0$ (may approach 0 during earthquake;
is conservative))

$$\beta := 0 \cdot \text{deg} \quad i := 26.6 \text{ deg}$$

$$\theta := \text{atan}\left(\frac{K_h}{1 - k_v}\right) \quad \theta = 0.09$$

$$K_{ae} := \frac{\cos(\phi - \theta - \beta)^2}{\cos(\theta) \cdot \cos(\beta)^2 \cdot \cos(\delta + \beta + \theta) \cdot \left(1 + \sqrt{\frac{\sin(\phi + \delta) \cdot \sin(\phi - \theta - i)}{\cos(\delta + \beta + \theta) \cdot \cos(i - \beta)}}\right)^2}$$

$$K_{ae} = 0.577$$

Calculate K_a and K_p for static conditions (Assumes $\delta = 0$):

Sheet 2 of 2

$$K_a(\phi, i, \beta) \equiv \frac{\cos(\phi - \beta)^2}{\left(\cos(\beta)^2 \cdot \cos(\beta) \right) \cdot \left[\left(1 + \sqrt{\frac{\sin(\phi) \cdot \sin(\phi - i)}{\cos(\beta) \cdot \cos(i - \beta)}} \right)^2 \right]}$$

$$K_a := K_a(\phi, i, \beta)$$

$$K_a = 0.417$$

Project Name: US 95 Widening; Retaining Walls 2c 2d **Level Backfill (i = 0 degrees) MSE Walls**
Project Number: 324-01-3
Calculated By: heb Checked By:sdb

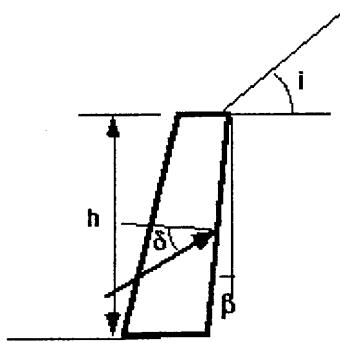
MONONOBE-OKABE ANALYSIS

Reference: Federal Highway Administration, 1998:
Geotechnical Earthquake Engineering,
Publication No. FHWA HI-99-012.

$$A := .18 \quad A_m := (1.45 - A) \cdot A$$

$$k_h := A_m \quad K_h := k_h \quad k_h = 0.229$$

$$k_v := 0$$



For structural backfill: $\phi := 34 \cdot \text{deg}$

$$\delta := 0$$

(may approach 0 during earthquake;))

$\beta := 0 \cdot \text{deg}$

j := 0deg

$$\theta := \text{atan} \left(\frac{k_h}{1 - k_v} \right) \quad \theta = 12.877 \text{ deg}$$

$$K_{ae} := \frac{\cos(\phi - \theta - \beta)^2}{\cos(\theta) \cdot \cos(\beta)^2 \cdot \cos(\delta + \beta + \theta) \cdot \left(1 + \sqrt{\frac{\sin(\phi + \delta) \cdot \sin(\phi - \theta - i)}{\cos(\delta + \beta + \theta) \cdot \cos(i - \beta)}} \right)^2}$$

$$K_{ge} = 0.433$$

Calculate K_a for static conditions (Assumes $\delta = 0$):

$$K_a(\phi, i, \beta) = \frac{\cos(\phi - \beta)^2}{(\cos(\beta)^2 \cdot \cos(\beta)) \left[\left(1 + \sqrt{\frac{\sin(\phi) \cdot \sin(\phi - i)}{\cos(\beta) \cdot \cos(i - \beta)}} \right)^2 \right]}$$

$$K_a := K_a(\phi, i, \beta)$$

$$K_a = 0.283$$

Project Name: US 95 Widening; Retaining Walls 2c 2d **Sloping Backfill ($i = 21.1$ degrees) MSE Walls**

Project Number: 324-01-3

Calculated By: heb Checked By:sdb

use 21.1degrees because slope fails to this

MONONOBE- OKABE ANALYSIS

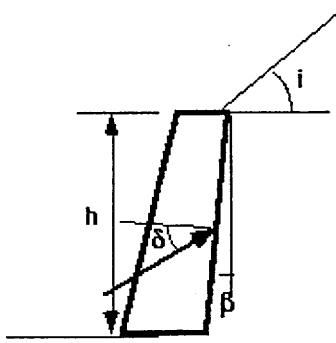
Reference: Federal Highway Administration, 1998:

Geotechnical Earthquake Engineering,
Publication No. FHWA HI-99-012.

$$A := .18 \quad A_m := (1.45 - A) \cdot A$$

$$k_h := A_m \quad K_h := k_h \quad K_h = 0.229$$

$$k_v := 0$$



For structural backfill: $\phi := 34 \text{ deg}$

$$\delta := 0$$

(may approach 0 during earthquake;))

$$\beta := 0 \text{ deg}$$

$$i := 21.1 \text{ deg}$$

$$\theta := \arctan\left(\frac{k_h}{1 - k_v}\right) \quad \theta = 12.877 \text{ deg}$$

$$K_{ae} := \frac{\cos(\phi - \theta - \beta)^2}{\cos(\theta) \cdot \cos(\beta)^2 \cdot \cos(\delta + \beta + \theta) \cdot \left(1 + \sqrt{\frac{\sin(\phi + \delta) \cdot \sin(\phi - \theta - i)}{\cos(\delta + \beta + \theta) \cdot \cos(i - \beta)}}\right)^2}$$

$$K_{ae} = 0.887$$

Calculate K_a for static conditions (Assumes $\delta = 0$):

$$K_a(\phi, i, \beta) = \frac{\cos(\phi - \beta)^2}{(\cos(\beta)^2 \cdot \cos(\beta)) \left[\left(1 + \sqrt{\frac{\sin(\phi) \cdot \sin(\phi - i)}{\cos(\beta) \cdot \cos(i - \beta)}} \right)^2 \right]}$$

$$K_a := K_a(\phi, i, \beta)$$

$$K_a = 0.368$$

Project Name: US 95 Widening 2C/2D

Tieback walls

Project Number: 324-01-3

($i = 21.6$ degrees)

Calculated By: HEB Checked By:

MONONOBE- OKABE ANALYSIS

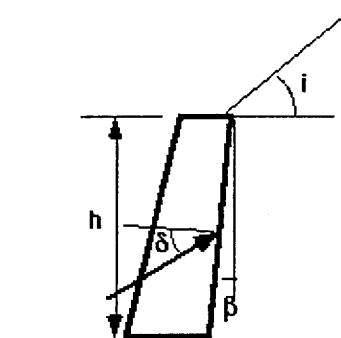
Reference: Federal Highway Administration, 1998:
Geotechnical Earthquake Engineering,
Publication No. FHWA HI-99-012.

ground acceleration from reports

$k_h = .18g$ for 10% probability in 50 years.

$K_h = 1.5k_h$ from AASHTO 5.7.4

$$k_h := .18 \quad K_h := 1.5 \cdot k_h$$



$$K_h = 0.27$$

$$k_v := 0.0$$

For structural backfill: $\phi := 34 \text{ deg}$

$\delta := 0$ (may approach 0 during earthquake; will use 0)

$\beta := 0 \text{ deg}$ $i := 18.5 \text{ deg}$ Slope fails to 18.5

$$\theta := \text{atan} \left(\frac{K_h}{1 - k_v} \right) \quad \theta = 0.264$$

$$K_{ae} := \frac{\cos(\phi - \theta - \beta)^2}{\cos(\theta) \cdot \cos(\beta)^2 \cdot \cos(\delta + \beta + \theta) \cdot \left(1 + \sqrt{\frac{\sin(\phi + \delta) \cdot \sin(\phi - \theta - i)}{\cos(\delta + \beta + \theta) \cdot \cos(i - \beta)}} \right)^2}$$

$$K_{ae} = 0.848$$

$i := 21.6 \cdot \text{deg}$

Sheet 2 of 2

$$K_a(\phi, i, \beta) = \frac{\cos(\phi - \beta)^2}{(\cos(\beta)^2 \cdot \cos(i)) \cdot \left[\left(1 + \sqrt{\frac{\sin(\phi) \cdot \sin(\phi - i)}{\cos(\beta) \cdot \cos(i - \beta)}} \right)^2 \right]}$$

$$K_a := K_a(\phi, i, \beta)$$

$$K_a = 0.372$$

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Sheet 1 of 2

Geotechnical and Construction Services

Date: 8/24/2002

Project Name: US 95 2c&2d **Lateral Earth Pressure: RW-6**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Lateral Pressure Calculations from FHWA-IF-99-015 - Static Conditions

For backfill:

$$\phi := 34 \cdot \text{deg} \quad \gamma := 125 \cdot \frac{\text{lbf}}{\text{ft}^3} \quad \text{kip} := 1000 \cdot \text{lbf}$$

$$K_a := .37$$

$$H_t := 5.447 \cdot m - 0.5 \cdot m \quad H_t = 16.23 \text{ ft}$$

$$p := 0.65 \cdot K_a \cdot \gamma \cdot H_t \quad \text{from page 51}$$

Location on Wall of Pressure Calculation

H_1 and H_n assumed

$$H_1 := \frac{H_t}{4} \quad \frac{2 \cdot H_1}{3} = 2.705 \text{ ft}$$

$$H_n := \frac{H_t}{4}$$

Apparent Earth Pressure Distribution:

$$H := \begin{pmatrix} 0 \\ 2 \cdot \frac{H_1}{3} \\ H_t - 2 \cdot \frac{H_n}{3} \\ H_t \end{pmatrix} \quad p_{\text{wall}} := \begin{pmatrix} 0 \\ p \\ p \\ 0 \end{pmatrix}$$

$$H = \begin{pmatrix} 0 \\ 2.705 \\ 13.525 \\ 16.23 \end{pmatrix} \text{ ft} \quad p_{\text{wall}} = \begin{pmatrix} 0 \\ 0.488 \\ 0.488 \\ 0 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Project Name: US 95 Widening 2c&2d Surcharge Load: RW-6 - Dead Load only

Project Number: 324-01-3

Calculated By: HEB Checked By:

Pressure Calculations from Surcharge Loads on Tie-Back Walls

$$\text{kip} := 1000 \cdot \text{lbf}$$

Strip Load Information

Horizontal dimension from top of wall to center of strip load:

$$d := 9.2 \text{ ft}$$

Width of strip load:

$$w := 10 \cdot \text{ft}$$

Load (kips/ft²):

$$q := 2.2 \cdot \frac{\text{kip}}{\text{ft}^2}$$

Location on Wall or Pressure Calculation

Vertical position on wall (measured from bottom of strip load):

$$H := \text{ft} \left\{ \begin{array}{l} 0.001 \\ 2 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 11 \\ 13.7 \end{array} \right.$$

Angles used in p_h calculation:

$$\alpha := \tan\left(\frac{d}{H}\right)$$

$$\alpha = \left\{ \begin{array}{l} 89.994 \\ 77.735 \\ 66.501 \\ 61.477 \\ 56.889 \\ 52.734 \\ 48.991 \\ 45.63 \\ 39.908 \\ 33.883 \end{array} \right. \text{deg}$$

$$\beta := 2 \left(\tan\left(\frac{d + \frac{w}{2}}{H}\right) - \alpha \right)$$

$$\beta = \left\{ \begin{array}{l} 4.386 \times 10^{-3} \\ 8.495 \\ 15.533 \\ 18.251 \\ 20.411 \\ 22.05 \\ 23.226 \\ 24.008 \\ 24.658 \\ 24.288 \end{array} \right. \text{deg}$$

Pressure at Specific Wall Height (kips/ft²):

$$P_h := \overrightarrow{\left[\left(\frac{2q}{\pi} \right) [\beta - (\sin(\beta))(\cos(2\alpha))] \right]}$$

$$H = \begin{pmatrix} 1 \times 10^{-3} \\ 2 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 11 \\ 13.7 \end{pmatrix} \text{ ft}$$

$$P_h = \begin{pmatrix} 2.144 \times 10^{-4} \\ 0.396 \\ 0.636 \\ 0.685 \\ 0.696 \\ 0.679 \\ 0.644 \\ 0.599 \\ 0.499 \\ 0.376 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-6 8/27/02

Dead Load Only

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height Meters
0	0.376	0	18.0	0.0
3	0.499	0.488	47.3	0.9
5	0.599	0.488	52.0	1.5
6	0.644	0.488	54.2	1.8
7	0.679	0.488	55.9	2.1
8	0.696	0.488	56.7	2.4
9	0.685	0.488	56.2	2.7
10	0.636	0.488	53.8	3.0
12	0.396	0.488	42.3	3.7
14	0	0.488	23.4	4.3
18	0	0	0.0	5.5

Project Name: US 95 Widening 2c&2d Surcharge Load: RW-6 - Dead Load + Live Load

Project Number: 324-01-3

Calculated By: HEB Checked By:

Pressure Calculations from Surcharge Loads on Tie-Back Walls

$$\text{kip} := 1000 \cdot \text{lbf}$$

Strip Load Information

Horizontal dimension from top of wall to center of strip load:

$$d := 9.2 \text{ ft}$$

Width of strip load:

$$w := 10 \cdot \text{ft}$$

Load (kips/ft²):

$$q := 2.6 \cdot \frac{\text{kip}}{\text{ft}^2}$$

Location on Wall of Pressure Calculation

Vertical position on wall (measured from bottom of strip load):

$$H := \text{ft} \cdot \begin{Bmatrix} 0.001 \\ 2 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 11 \\ 13.7 \end{Bmatrix}$$

Angles used in p_h calculation:

$$\alpha := \text{atan}\left(\frac{d}{H}\right)$$

$$\beta := 2 \left(\text{atan}\left(\frac{d + \frac{w}{2}}{H}\right) - \alpha \right)$$

$$\alpha = \begin{Bmatrix} 89.994 \\ 77.735 \\ 66.501 \\ 61.477 \\ 56.889 \\ 52.734 \\ 48.991 \\ 45.63 \\ 39.908 \\ 33.883 \end{Bmatrix} \text{deg}$$

$$\beta = \begin{Bmatrix} 4.386 \times 10^{-3} \\ 8.495 \\ 15.533 \\ 18.251 \\ 20.411 \\ 22.05 \\ 23.226 \\ 24.008 \\ 24.658 \\ 24.288 \end{Bmatrix} \text{deg}$$

Pressure at Specific Wall Height (kips/ft²):

$$P_h := \overrightarrow{\left[\left(\frac{2q}{\pi} \right) [\beta - (\sin(\beta))(\cos(2\alpha))] \right]}$$

$$H = \begin{pmatrix} 1 \times 10^{-3} \\ 2 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 11 \\ 13.7 \end{pmatrix} \text{ ft}$$

$$P_h = \begin{pmatrix} 2.534 \times 10^{-4} \\ 0.468 \\ 0.751 \\ 0.809 \\ 0.822 \\ 0.803 \\ 0.762 \\ 0.708 \\ 0.59 \\ 0.444 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-6 8/27/02**Dead Load + Live Load**

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height feet
0	0.444	0	21.3	0.0
3	0.59	0.488	51.6	0.9
5	0.712	0.488	57.5	1.5
6	0.762	0.488	59.9	1.8
7	0.803	0.488	61.8	2.1
8	0.82	0.488	62.6	2.4
9	0.809	0.488	62.1	2.7
10	0.751	0.488	59.3	3.0
12	0.468	0.488	45.8	3.7
14	0	0.488	23.4	4.3
18	0	0	0.0	5.5

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Geotechnical and Construction Services

Date: 8/24/2002

Project Name: US 95 2c&2d **Lateral Earth Pressure: RW-6**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Lateral Pressure Calculations from FHWA-IF-99-015 - Dynamic Conditions

For backfill:

$$\phi := 34 \cdot \text{deg} \quad \gamma := 125 \cdot \frac{\text{lbf}}{\text{ft}^3} \quad \text{kip} := 1000 \cdot \text{lbf}$$

$$K_{ae} := .848$$

$$H_t := 5.447 \cdot m - 0.5 \cdot m \quad H_t = 16.23 \text{ ft}$$

$$p := 0.65 \cdot K_{ae} \cdot \gamma \cdot H_t \quad \text{from page 51}$$

Location on Wall of Pressure Calculation

H_1 and H_n assumed

$$H_1 := \frac{H_t}{4} \quad \frac{2 \cdot H_1}{3} = 2.705 \text{ ft}$$

$$H_n := \frac{H_t}{4}$$

Apparent Earth Pressure Distribution:

$$H := \begin{pmatrix} 0 \\ \frac{2 \cdot H_1}{3} \\ H_t - 2 \cdot \frac{H_n}{3} \\ H_t \end{pmatrix} \quad p_{\text{wall}} := \begin{pmatrix} 0 \\ p \\ p \\ 0 \end{pmatrix}$$

$$H = \begin{pmatrix} 0 \\ 2.705 \\ 13.525 \\ 16.23 \end{pmatrix} \text{ ft} \quad p_{\text{wall}} = \begin{pmatrix} 0 \\ 1.118 \\ 1.118 \\ 0 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-6 8/27/02

Dead Load + Sies

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height meters
0	0.376	0	18.0	0.0
3	0.499	1.118	77.6	0.9
5	0.599	1.118	82.4	1.5
6	0.644	1.118	84.6	1.8
7	0.679	1.118	86.2	2.1
8	0.696	1.118	87.1	2.4
9	0.685	1.118	86.5	2.7
10	0.636	1.118	84.2	3.0
12	0.396	1.118	72.7	3.7
14	0	1.118	53.7	4.3
18	0	0	0.0	5.5

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Sheet 1 of 1

Geotechnical and Construction Services

Date: 8/24/2002

Project Name: US 95 2c&2d **Lateral Earth Pressure: RW-7**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Lateral Pressure Calculations from FHWA-IF-99-015 - Static Conditions

For backfill:

$$\phi := 34 \cdot \text{deg} \quad \gamma := 125 \cdot \frac{\text{lbf}}{\text{ft}^3} \quad \text{kip} := 1000 \cdot \text{lbf}$$

$$K_a := .37$$

$$H_t := 5.638 \cdot m - 0.52 \cdot m$$

$$H_t = 16.791 \text{ ft}$$

$$p := 0.65 \cdot K_a \cdot \gamma \cdot H_t \quad \text{from page 51}$$

Location on Wall of Pressure Calculation

$$\begin{aligned} H_1 \text{ and } H_n \text{ assumed} \quad H_1 &:= \frac{H_t}{4} & \frac{2 \cdot H_1}{3} &= 2.799 \text{ ft} \\ H_n &:= \frac{H_t}{4} & H &:= \begin{pmatrix} 0 \\ 2 \cdot \frac{H_1}{3} \\ H_t - 2 \cdot \frac{H_n}{3} \\ H_t \end{pmatrix} & p_{\text{wall}} &:= \begin{pmatrix} 0 \\ p \\ p \\ 0 \end{pmatrix} \\ \text{Apparent Earth Pressure Distribution:} \quad & & & & & \\ H &= \begin{pmatrix} 0 \\ 2.799 \\ 13.993 \\ 16.791 \end{pmatrix} \text{ ft} & p_{\text{wall}} &= \begin{pmatrix} 0 \\ 0.505 \\ 0.505 \\ 0 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2} \end{aligned}$$

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Geotechnical and Construction Services

Date: 8/24 /2002

Project Name: US 95 Widening 2c&2d **Surcharge Load: RW-7 - Dead Load only**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Pressure Calculations from Surcharge Loads on Tie-Back Walls

$$\text{kip} := 1000 \cdot \text{lbf}$$

Strip Load Information

Horizontal dimension from top of wall to center of strip load:

$$d := 12.5 \text{ ft}$$

Width of strip load:

$$w := 10 \cdot \text{ft}$$

Load (kips/ft²):

$$q := 2.3 \cdot \frac{\text{kip}}{\text{ft}^2}$$

Location on Wall for Pressure Calculation

Vertical position on wall (measured from bottom of strip load):

$$H := \text{ft} \cdot \begin{Bmatrix} 0.001 \\ 2 \\ 4 \\ 6 \\ 8 \\ 10 \\ 12 \\ 14 \\ 16 \\ 17.1 \end{Bmatrix}$$

Angles used in p_h calculation:

$$\alpha := \text{atan}\left(\frac{d}{H}\right)$$
$$\beta := 2 \left(\text{atan}\left(\frac{d + \frac{w}{2}}{H}\right) - \alpha \right)$$
$$\alpha = \begin{Bmatrix} 89.995 \\ 80.91 \\ 72.255 \\ 64.359 \\ 57.381 \\ 51.34 \\ 46.169 \\ 41.76 \\ 37.999 \\ 36.167 \end{Bmatrix} \text{deg}$$

$$\beta = \begin{Bmatrix} 2.619 \times 10^{-3} \\ 5.141 \\ 9.739 \\ 13.433 \\ 16.104 \\ 17.83 \\ 18.784 \\ 19.16 \\ 19.13 \\ 18.992 \end{Bmatrix} \text{deg}$$

Pressure at Specific Wall Height (kips/ft²):

$$P_h := \overrightarrow{\left[\left(\frac{2q}{\pi} \right) [\beta - (\sin(\beta))(\cos(2\alpha))] \right]}$$

$$H = \begin{pmatrix} 1 \times 10^{-3} \\ 2 \\ 4 \\ 6 \\ 8 \\ 10 \\ 12 \\ 14 \\ 16 \\ 17.1 \end{pmatrix} \text{ ft}$$

$$P_h = \begin{pmatrix} 1.339 \times 10^{-4} \\ 0.256 \\ 0.451 \\ 0.556 \\ 0.582 \\ 0.554 \\ 0.499 \\ 0.435 \\ 0.373 \\ 0.341 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-7 8/27/02

Dead Load Only

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height meters
0	0.341	0	16.3	0.0
2	0.373	0.505	42.0	0.6
4	0.435	0.505	45.0	1.2
6	0.499	0.505	48.1	1.8
8	0.554	0.505	50.7	2.4
10	0.582	0.505	52.0	3.0
12	0.556	0.505	50.8	3.7
14	0.451	0.505	45.8	4.3
16	0.256	0.505	36.4	4.9
17.6	0	0	0.0	5.4
18	0	0	0.0	5.5

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Geotechnical and Construction Services

Date: 8/24 /2002

Project Name: US 95 Widening 2c&2d Surcharge Load: RW-7 - Dead Load + Live Load

Project Number: 324-01-3

Calculated By: HEB Checked By:

Pressure Calculations from Surcharge Loads on Tie-Back Walls

$$\text{kip} := 1000 \cdot \text{lbf}$$

Strip Load Information

Horizontal dimension from top of wall to center of strip load:

$$d := 12.5 \text{ ft}$$

Width of strip load:

$$w := 10 \cdot \text{ft}$$

Load (kips/ft²):

$$q := 2.6 \cdot \frac{\text{kip}}{\text{ft}^2}$$

Location on Wall for Pressure Calculation

Vertical position on wall (measured from bottom of strip load):

$$H := \text{ft} \cdot \begin{Bmatrix} 0.001 \\ 2 \\ 4 \\ 6 \\ 8 \\ 10 \\ 12 \\ 14 \\ 16 \\ 17.1 \end{Bmatrix}$$

Angles used in p_h calculation:

$$\alpha := \text{atan} \left(\frac{d}{H} \right)$$
$$\alpha = \begin{Bmatrix} 89.995 \\ 80.91 \\ 72.255 \\ 64.359 \\ 57.381 \\ 51.34 \\ 46.169 \\ 41.76 \\ 37.999 \\ 36.167 \end{Bmatrix} \text{deg}$$
$$\beta := 2 \cdot \text{atan} \left(\frac{d + \frac{w}{2}}{H} \right) - \alpha$$
$$\beta = \begin{Bmatrix} 2.619 \times 10^{-3} \\ 5.141 \\ 9.739 \\ 13.433 \\ 16.104 \\ 17.83 \\ 18.784 \\ 19.16 \\ 19.13 \\ 18.992 \end{Bmatrix} \text{deg}$$

Pressure at Specific Wall Height (kips/ft²):

$$P_h := \overrightarrow{\left[\left(\frac{2q}{\pi} \right) [\beta - (\sin(\beta))(\cos(2\alpha))] \right]}$$

$$H = \begin{pmatrix} 1 \times 10^{-3} \\ 2 \\ 4 \\ 6 \\ 8 \\ 10 \\ 12 \\ 14 \\ 16 \\ 17.1 \end{pmatrix} \text{ ft}$$

$$P_h = \begin{pmatrix} 1.513 \times 10^{-4} \\ 0.289 \\ 0.509 \\ 0.629 \\ 0.658 \\ 0.626 \\ 0.564 \\ 0.492 \\ 0.421 \\ 0.385 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-7 8/27/02

Dead Load + Live Load

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height meters
0	0.385	0	18.4	0.0
2	0.421	0.505	44.3	0.6
4	0.492	0.505	47.7	1.2
6	0.564	0.505	51.2	1.8
8	0.626	0.505	54.2	2.4
10	0.658	0.505	55.7	3.0
12	0.629	0.505	54.3	3.7
14	0.509	0.505	48.6	4.3
16	0.289	0.505	38.0	4.9
17.6	0	0	0.0	5.4
18	0	0	0.0	5.5

BLACK EAGLE CONSULTING

Sheet 1 of 2

Geotechnical and Construction Services

Date: 8/24/2002

Project Name: US 95 2c&2d **Lateral Earth Pressure: RW-7**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Lateral Pressure Calculations from FHWA-IF-99-015 - Dynamic Conditions

For backfill:

$$\phi := 34 \cdot \text{deg} \quad \gamma := 125 \cdot \frac{\text{lbf}}{\text{ft}^3} \quad \text{kip} := 1000 \cdot \text{lbf}$$

$$K_{ae} := .848$$

$$H_t := 5.638 \cdot m - 0.52 \cdot m$$

$$H_t = 16.791 \text{ ft}$$

$$p := 0.65 \cdot K_{ae} \cdot \gamma \cdot H_t \quad \text{from page 51}$$

Location on Wall of Pressure Calculation

H_1 and H_n assumed

$$H_1 := \frac{H_t}{4} \quad \frac{2 \cdot H_1}{3} = 2.799 \text{ ft}$$

$$H_n := \frac{H_t}{4}$$

Apparent Earth Pressure Distribution:

$$H := \begin{pmatrix} 0 \\ 2 \cdot \frac{H_1}{3} \\ H_t - 2 \cdot \frac{H_n}{3} \\ H_t \end{pmatrix} \quad p_{\text{wall}} := \begin{pmatrix} 0 \\ p \\ p \\ 0 \end{pmatrix}$$

$$H = \begin{pmatrix} 0 \\ 2.799 \\ 13.993 \\ 16.791 \end{pmatrix} \text{ ft} \quad p_{\text{wall}} = \begin{pmatrix} 0 \\ 1.157 \\ 1.157 \\ 0 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-7 8/27/02

Dead Load + Seismic Load

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height meters
0	0.341	0	16.3	0.0
2	0.373	1.157	73.3	0.6
4	0.435	1.157	76.2	1.2
6	0.499	1.157	79.3	1.8
8	0.554	1.157	81.9	2.4
10	0.582	1.157	83.3	3.0
12	0.556	1.157	82.0	3.7
14	0.451	1.157	77.0	4.3
16	0.256	1.157	67.7	4.9
17.6	0	0	0.0	5.4
18	0	0	0.0	5.5

BLACK EAGLE CONSULTING

Sheet 1 of 1

Geotechnical and Construction Services

Date: 8/24/2002

Project Name: US 95 2c&2d **Lateral Earth Pressure: RW-19**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Lateral Pressure Calculations from FHWA-IF-99-015 - Static Conditions

For backfill:

$$\phi := 34 \cdot \text{deg} \quad \gamma := 125 \cdot \frac{\text{lbf}}{\text{ft}^3} \quad \text{kip} := 1000 \cdot \text{lbf}$$

$$K_a := .37$$

$$H_t := 5.366 \cdot m - 0.5 \cdot m$$

$$H_t = 15.965 \text{ ft}$$

$$p := 0.65 \cdot K_a \cdot \gamma \cdot H_t \quad \text{from page 51}$$

Location on Wall of Pressure Calculation

H_1 and H_n assumed

$$H_1 := \frac{H_t}{4} \quad \frac{2 \cdot H_1}{3} = 2.661 \text{ ft}$$

$$H_n := \frac{H_t}{4}$$

Apparent Earth Pressure Distribution:

$$H := \begin{pmatrix} 0 \\ \frac{H_1}{3} \\ H_t - 2 \cdot \frac{H_n}{3} \\ H_t \end{pmatrix} \quad p_{\text{wall}} := \begin{pmatrix} 0 \\ p \\ p \\ 0 \end{pmatrix}$$

$$H = \begin{pmatrix} 0 \\ 2.661 \\ 13.304 \\ 15.965 \end{pmatrix} \text{ ft} \quad p_{\text{wall}} = \begin{pmatrix} 0 \\ 0.48 \\ 0.48 \\ 0 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Project Name: US 95 Widening 2c&2d **Surcharge Load: RW-19 - Dead Load only**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Pressure Calculations from Surcharge Loads on Tie-Back Walls

$$\text{kip} := 1000 \cdot \text{lbf}$$

Strip Load Information

Horizontal dimension from top of wall to center of strip load:

$$d := 8.1 \cdot \text{ft}$$

Width of strip load:

$$w := 6.0 \cdot \text{ft}$$

Load (kips/ft²):

$$q := 3.1 \cdot \frac{\text{kip}}{\text{ft}^2}$$

Location on Wall of Pressure Calculation

Vertical position on wall (measured from bottom of strip load):

$$H := \text{ft} \cdot \begin{pmatrix} 0.001 \\ 2 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 10 \\ 12 \\ 14 \end{pmatrix}$$

Angles used in p_h calculation:

$$\alpha := \tan\left(\frac{d}{H}\right)$$

$$\beta := 2 \left(\tan\left(\frac{d + \frac{w}{2}}{H}\right) - \alpha \right)$$

$$\alpha = \begin{pmatrix} 89.993 \\ 76.13 \\ 63.719 \\ 58.314 \\ 53.471 \\ 49.167 \\ 45.356 \\ 39.007 \\ 34.019 \\ 30.052 \end{pmatrix} \text{deg}$$

$$\beta = \begin{pmatrix} 3.824 \times 10^{-3} \\ 7.311 \\ 12.929 \\ 14.874 \\ 16.272 \\ 17.193 \\ 17.726 \\ 17.954 \\ 17.499 \\ 16.714 \end{pmatrix} \text{deg}$$

Pressure at Specific Wall Height (kips/ft²):

$$P_h := \overrightarrow{\left[\left(\frac{2q}{\pi} \right) [\beta - (\sin(\beta))(\cos(2\alpha))] \right]}$$

$$H = \begin{pmatrix} 1 \times 10^{-3} \\ 2 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 10 \\ 12 \\ 14 \end{pmatrix} \text{ ft}$$

$$P_h = \begin{pmatrix} 2.634 \times 10^{-4} \\ 0.474 \\ 0.714 \\ 0.739 \\ 0.722 \\ 0.677 \\ 0.618 \\ 0.492 \\ 0.381 \\ 0.293 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-19 8/27/02

Dead Load Only

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height meters
0	0.293	0	14.0	0.0
2	0.381	0.48	41.2	0.6
4	0.492	0.48	46.5	1.2
6	0.618	0.48	52.6	1.8
7	0.677	0.48	55.4	2.1
8	0.722	0.48	57.6	2.4
9	0.739	0.48	58.4	2.7
10	0.714	0.48	57.2	3.0
12	0.474	0.48	45.7	3.7
14	0	0.48	23.0	4.3
17.6	0	0	0.0	5.4

Project Name: US 95 Widening 2c&2d Surcharge Load: RW-19 - Dead Load + Live Load
 Project Number: 324-01-3
 Calculated By: HEB Checked By:

Pressure Calculations from Surcharge Loads on Tie-Back Walls

$$\text{kip} := 1000 \cdot \text{lbf}$$

Strip Load Information

Horizontal dimension from top of wall to center of strip load:

$$d := 8.1 \cdot \text{ft}$$

Width of strip load:

$$w := 6.0 \cdot \text{ft}$$

Load (kips/ft²):

$$q := 3.9 \cdot \frac{\text{kip}}{\text{ft}^2}$$

Location on Wall of Pressure Calculation

Vertical position on wall (measured from bottom of strip load):

$$H := \text{ft} \cdot \begin{pmatrix} 0.001 \\ 2 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 10 \\ 12 \\ 14 \end{pmatrix}$$

Angles used in p_h calculation:

$$\alpha := \text{atan} \left(\frac{d}{H} \right)$$

$$\beta := 2 \cdot \text{atan} \left(\frac{d + \frac{w}{2}}{H} \right) - \alpha$$

$$\alpha = \begin{pmatrix} 89.993 \\ 76.13 \\ 63.719 \\ 58.314 \\ 53.471 \\ 49.167 \\ 45.356 \\ 39.007 \\ 34.019 \\ 30.052 \end{pmatrix} \text{deg}$$

$$\beta = \begin{pmatrix} 3.824 \times 10^{-3} \\ 7.311 \\ 12.929 \\ 14.874 \\ 16.272 \\ 17.193 \\ 17.726 \\ 17.954 \\ 17.499 \\ 16.714 \end{pmatrix} \text{deg}$$

Pressure at Specific Wall Height (kips/ft²):

$$P_h := \overline{\left[\left(\frac{2q}{\pi} \right) [\beta - (\sin(\beta))(\cos(2\alpha))] \right]}$$

$$H = \begin{pmatrix} 1 \times 10^{-3} \\ 2 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 10 \\ 12 \\ 14 \end{pmatrix} \text{ ft}$$

$$P_h = \begin{pmatrix} 3.314 \times 10^{-4} \\ 0.596 \\ 0.898 \\ 0.93 \\ 0.908 \\ 0.851 \\ 0.778 \\ 0.619 \\ 0.479 \\ 0.368 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-19 8/27/02

Dead Load + Live Load

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height meters
0	0.368	0	17.6	0.0
2	0.479	0.48	45.9	0.6
4	0.619	0.48	52.6	1.2
6	0.778	0.48	60.2	1.8
7	0.851	0.48	63.7	2.1
8	0.908	0.48	66.5	2.4
9	0.93	0.48	67.5	2.7
10	0.898	0.48	66.0	3.0
12	0.596	0.48	51.5	3.7
14	0	0.48	23.0	4.3
17.6	0	0	0.0	5.4

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Sheet 1 of 2

Geotechnical and Construction Services

Date: 8/24/2002

Project Name: US 95 2c&2d **Lateral Earth Pressure: RW-19**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Lateral Pressure Calculations from FHWA-IF-99-015 - Dynamic Conditions

For backfill:

$$\phi := 34 \cdot \text{deg} \quad \gamma := 125 \cdot \frac{\text{lbf}}{\text{ft}^3} \quad \text{kip} := 1000 \cdot \text{lbf}$$

$$K_a := .848$$

$$H_t := 5.366 \cdot m - 0.5 \cdot m$$

$$H_t = 15.965 \text{ ft}$$

$$p := 0.65 \cdot K_a \cdot \gamma \cdot H_t \quad \text{from page 51}$$

Location on Wall of Pressure Calculation

$$H_1 \text{ and } H_n \text{ assumed} \quad H_1 := \frac{H_t}{4} \quad \frac{2 \cdot H_1}{3} = 2.661 \text{ ft}$$

Apparent Earth Pressure Distribution:

$$H_n := \frac{H_t}{4} \quad H := \begin{pmatrix} 0 \\ \frac{H_1}{3} \\ H_t - 2 \cdot \frac{H_n}{3} \\ H_t \end{pmatrix} \quad p_{\text{wall}} := \begin{pmatrix} 0 \\ p \\ p \\ 0 \end{pmatrix}$$

$$H = \begin{pmatrix} 0 \\ 2.661 \\ 13.304 \\ 15.965 \end{pmatrix} \text{ ft} \quad p_{\text{wall}} = \begin{pmatrix} 0 \\ 1.1 \\ 1.1 \\ 0 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Ret Wall RW-19 8/27/02

Dead Load + Seismic

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height meters
0	0.293	0	14.0	0.0
2	0.381	1.1	70.9	0.6
4	0.492	1.1	76.2	1.2
6	0.618	1.1	82.3	1.8
7	0.677	1.1	85.1	2.1
8	0.722	1.1	87.2	2.4
9	0.739	1.1	88.1	2.7
10	0.714	1.1	86.9	3.0
12	0.474	1.1	75.4	3.7
14	0	1.1	52.7	4.3
17.6	0	0	0.0	5.4

Project Name: US 95 Widening 2C/2D

Tieback walls RW-16

Project Number: 324-01-3

($i = 26.6$ degrees)

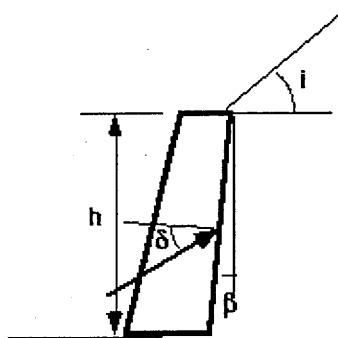
Calculated By: HEB Checked By:

MONONOBE- OKABE ANALYSIS

Reference: Federal Highway Administration, 1998:
Geotechnical Earthquake Engineering,
Publication No. FHWA HI-99-012.

ground acceleration from reports
 $k_h = .18g$ for 10% probability in 50 years.
 $K_h = 1.5k_h$ from AASHTO 5.7.4

$$k_h := .18 \quad K_h := 1.5 \cdot k_h$$



$$K_h = 0.27$$

$$k_v := 0.0$$

For native soil: $\phi := 40 \cdot \text{deg}$

$\delta := 0$ (may approach 0 during earthquake; will use 0)

$\beta := 0 \cdot \text{deg}$ $i := 22.6 \cdot \text{deg}$ Slope fails to 22.6

$$\theta := \text{atan} \left(\frac{K_h}{1 - k_v} \right) \quad \theta = 0.264$$

$$K_{ae} := \frac{\cos(\phi - \theta - \beta)^2}{\cos(\theta) \cdot \cos(\beta)^2 \cdot \cos(\delta + \beta + \theta) \cdot \left(1 + \sqrt{\frac{\sin(\phi + \delta) \cdot \sin(\phi - \theta - i)}{\cos(\delta + \beta + \theta) \cdot \cos(i - \beta)}} \right)^2}$$

$$K_{ae} = 0.645$$

$i := 26.6 \cdot \text{deg}$

Sheet 2 of 2

$$K_a(\phi, i, \beta) = \frac{\cos(\phi - \beta)^2}{(\cos(\beta)^2 \cdot \cos(\beta)) \cdot \left[\left(1 + \sqrt{\frac{\sin(\phi) \cdot \sin(\phi - i)}{\cos(\beta) \cdot \cos(i - \beta)}} \right)^2 \right]}$$

$$K_a := K_a(\phi, i, \beta)$$

$$K_a = 0.296$$

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Sheet 1 of 1

Geotechnical and Construction Services

Date: 3/26/2002

Project Name: US 95 Widening; Retaining Walls 2C/2D

Lateral Earth Pressure: RW-16

Project Number: 324-01-3

Calculated By: HEB Checked By:

Lateral Pressure Calculations from FHWA-IF-99-015 - Static Conditions

For native soils

$$\phi := 40 \cdot \text{deg} \quad \gamma := 130 \cdot \frac{\text{lbf}}{\text{ft}^3} \quad \text{kip} := 1000 \cdot \text{lbf}$$

$$K_a := .29$$

$$H_t := 18 \cdot \text{ft}$$

$$p := 0.65 \cdot K_a \cdot \gamma \cdot H_t \quad \text{from page 51}$$

Location on Wall of Pressure Calculation

Top of wall

$$H_1 := 2.13 \cdot \text{ft}$$

Apparent Earth Pressure Distribution:

$$H_n := 2.44 \cdot \text{ft}$$
$$H := \begin{pmatrix} 0 \\ 2 \cdot \frac{H_1}{3} \\ H_t - 2 \cdot \frac{H_n}{3} \\ H_t \end{pmatrix} \quad p_{\text{wall}} := \begin{pmatrix} 0 \\ p \\ p \\ 0 \end{pmatrix}$$
$$H = \begin{pmatrix} 0 \\ 1.42 \\ 16.373 \\ 18 \end{pmatrix} \text{ft} \quad p_{\text{wall}} = \begin{pmatrix} 0 \\ 0.441 \\ 0.441 \\ 0 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

BLACK EAGLE CONSULTING

Sheet 1 of 1

Geotechnical and Construction Services

Date: 3/26/2002

Project Name: US 95 Widening; Retaining Walls 2c **Lateral Earth Pressure: RW-16**

Project Number: 324-01-3

Calculated By: HEB Checked By:

Lateral Pressure Calculations from FHWA-IF-99-015 - Dynamic Conditions

For native soils

$$\phi := 40 \cdot \text{deg} \quad \gamma := 130 \cdot \frac{\text{lbf}}{\text{ft}^3} \quad \text{kip} := 1000 \cdot \text{lbf}$$

$$K_{ae} := .65$$

$$H_t := 18 \cdot \text{ft}$$

$$p := 0.65 \cdot K_{ae} \cdot \gamma \cdot H_t \quad \text{from page 51}$$

Location on Wall of Pressure Calculation

Top of wall

$$H_1 := 2.13 \cdot \text{ft}$$

Apparent Earth Pressure Distribution:

$$H_n := 2.44 \cdot \text{ft}$$
$$H := \begin{pmatrix} 0 \\ 2 \cdot \frac{H_1}{3} \\ H_t - 2 \cdot \frac{H_n}{3} \\ H_t \end{pmatrix} \quad p_{wall} := \begin{pmatrix} 0 \\ p \\ p \\ 0 \end{pmatrix}$$

$$H = \begin{pmatrix} 0 \\ 1.42 \\ 16.373 \\ 18 \end{pmatrix} \text{ft} \quad p_{wall} = \begin{pmatrix} 0 \\ 0.989 \\ 0.989 \\ 0 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

Project Name: US 95 Widening; Retaining Walls 2c **Surcharge Load: RW-16**
 Project Number: 324-01-3 **Dead Load**
 Calculated By: HEB Checked By:

Pressure Calculations from Surcharge Loads on Tie-Back Walls

$$\text{kip} := 1000 \cdot \text{lbf}$$

Strip Load Information

Horizontal dimension from top of wall to center of strip load:

$$d := 14 \cdot \text{ft}$$

Width of strip load:

$$w := 6.5 \cdot \text{ft}$$

Load (kips/ft²):

$$q := 2.4 \cdot \frac{\text{kip}}{\text{ft}^2}$$

Location on Wall of Pressure Calculation

Vertical position on wall (measured from top of wall):

$$H := \text{ft} \cdot \begin{Bmatrix} 0.001 \\ 2 \\ 4 \\ 6 \\ 8 \\ 10 \\ 12 \\ 14 \\ 16 \\ 18 \end{Bmatrix}$$

Angles used in p_h calculation:

$$\alpha := \tan\left(\frac{d}{H}\right)$$

$$\beta := 2 \left(\tan\left(\frac{d + \frac{w}{2}}{H}\right) - \alpha \right)$$

$$\alpha = \begin{Bmatrix} 89.996 \\ 81.87 \\ 74.055 \\ 66.801 \\ 60.255 \\ 54.462 \\ 49.399 \\ 45 \\ 41.186 \\ 37.875 \end{Bmatrix} \text{deg}$$

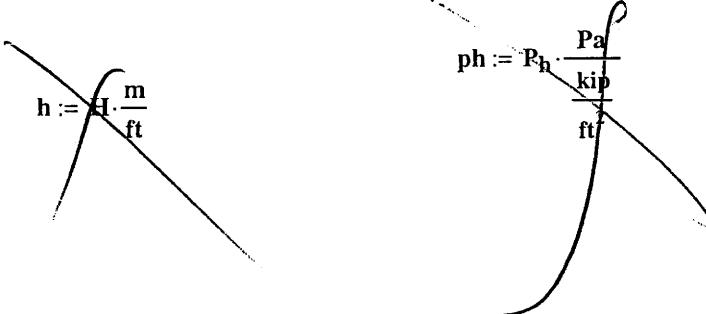
$$\beta = \begin{Bmatrix} 1.542 \times 10^{-3} \\ 3.033 \\ 5.78 \\ 8.039 \\ 9.729 \\ 10.873 \\ 11.554 \\ 11.875 \\ 11.934 \\ 11.812 \end{Bmatrix} \text{deg}$$

Pressure at Specific Wall Height (kips/ft²):

$$P_h := \overline{\left[\left(\frac{2q}{\pi} \right) \beta - (\sin(\beta))(\cos(2\alpha)) \right]}$$

$$H = \begin{pmatrix} 1 \times 10^{-3} \\ 2 \\ 4 \\ 6 \\ 8 \\ 10 \\ 12 \\ 14 \\ 16 \\ 18 \end{pmatrix} \text{ ft}$$

$$P_h = \begin{pmatrix} 8.225 \times 10^{-5} \\ 0.159 \\ 0.285 \\ 0.362 \\ 0.391 \\ 0.383 \\ 0.355 \\ 0.317 \\ 0.276 \\ 0.238 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$



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Sheet 1 of 2

Geotechnical and Construction Services

Date: 3/11/2002

Project Name: US 95 Widening; Retaining Walls 2c

Surcharge Load: RW-16

Project Number: 324-01-3

Dead+Live Load

Calculated By: HEB Checked By:

Pressure Calculations from Surcharge Loads on Tie-Back Walls

$$\text{kip} := 1000 \cdot \text{lbf}$$

Strip Load Information

Horizontal dimension from top of wall to center of strip load:

$$d := 14 \cdot \text{ft}$$

Width of strip load:

$$w := 6.5 \cdot \text{ft}$$

Load (kips/ft²):

$$q := 3.1 \cdot \frac{\text{kip}}{\text{ft}^2}$$

Location on Wall of Pressure Calculation

Vertical position on wall (measured from top of wall):

$$H := \text{ft} \cdot \begin{Bmatrix} 0.001 \\ 2 \\ 4 \\ 6 \\ 8 \\ 10 \\ 12 \\ 14 \\ 16 \\ 18 \end{Bmatrix}$$

Angles used in p_h calculation:

$$\alpha := \text{atan}\left(\frac{d}{H}\right)$$
$$\beta := 2 \left(\text{atan}\left(\frac{d + \frac{w}{2}}{H}\right) - \alpha \right)$$
$$\alpha = \begin{Bmatrix} 89.996 \\ 81.87 \\ 74.055 \\ 66.801 \\ 60.255 \\ 54.462 \\ 49.399 \\ 45 \\ 41.186 \\ 37.875 \end{Bmatrix} \text{deg}$$
$$\beta = \begin{Bmatrix} 1.542 \times 10^{-3} \\ 3.033 \\ 5.78 \\ 8.039 \\ 9.729 \\ 10.873 \\ 11.554 \\ 11.875 \\ 11.934 \\ 11.812 \end{Bmatrix} \text{deg}$$

Pressure at Specific Wall Height (kips/ft²):

$$P_h := \overline{\left[\left(\frac{2q}{\pi} \right) [\beta - (\sin(\beta))(\cos(2\alpha))] \right]}$$

$$H = \begin{pmatrix} 1 \times 10^{-3} \\ 2 \\ 4 \\ 6 \\ 8 \\ 10 \\ 12 \\ 14 \\ 16 \\ 18 \end{pmatrix} \text{ ft}$$

$$P_h = \begin{pmatrix} 1.062 \times 10^{-4} \\ 0.205 \\ 0.368 \\ 0.467 \\ 0.504 \\ 0.495 \\ 0.458 \\ 0.409 \\ 0.357 \\ 0.307 \end{pmatrix} \frac{\text{kip}}{\text{ft}^2}$$

$$h := H \frac{\text{m}}{\text{ft}}$$

$$ph := P_h \frac{\text{Pa}}{\frac{\text{kip}}{\text{ft}^2}}$$

Ret Wall RW-16 3/26/02 REVISION

Dead Load Only

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height Meters	
0	0.238	0	11.4	0.0	
2	0.276	0.441	34.3	0.6	
4	0.317	0.441	36.3	1.2	
6	0.355	0.441	38.1	1.8	
8	0.383	0.441	39.5	2.4	
10	0.391	0.441	39.8	3.0	
12	0.362	0.441	38.4	3.7	
14	0.285	0.441	34.8	4.3	
16	0.159	0.441	28.7	4.9	
18	0	0	0.0	5.5	

Dead Load + Live Load

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height Meters
0	0.238	0	0	0	0.307	0	0	0.0
2	0.276	0.441	34.3	2	0.357	0.441	38.2	0.6
4	0.317	0.441	36.3	4	0.409	0.441	40.7	1.2
6	0.355	0.441	38.1	6	0.458	0.441	43.0	1.8
8	0.383	0.441	39.5	8	0.495	0.441	44.8	2.4
10	0.391	0.441	39.8	10	0.504	0.441	45.2	3.0
12	0.362	0.441	38.4	12	0.467	0.441	43.5	3.7
14	0.285	0.441	34.8	14	0.368	0.441	38.7	4.3
16	0.159	0.441	28.7	16	0.205	0.441	30.9	4.9
18	0	0	0.0	18	0	0.0	0.0	5.5

Dead and Seismic Load

Wall Height feet	Sur Press kip/sq.ft.	Lat Press kip/sq.ft.	Total Press kPa	Wall Height Meters
0	0.238	0	11.4	0.0
2	0.276	0.989	60.6	0.6
4	0.317	0.989	62.5	1.2
6	0.355	0.989	64.4	1.8
8	0.383	0.989	65.7	2.4
10	0.391	0.989	66.1	3.0
12	0.362	0.989	64.7	3.7
14	0.285	0.989	61.0	4.3
16	0.159	0.989	55.0	4.9
18	0	0	0.0	5.5